Appendix L. Noise Technical Report

Noise Technical Report

Fanita Ranch Project

May 2020

Prepared for:



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Prepared by:



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Acronyms and Abbreviations

ADT Caltrans CEQA CFR CNEL dB dBA FTA HVAC in/sec Ldn Leq Lmax Lmin MCAS NSLU PDMWD PPV RCNM RV SR-	average daily traffic California Department of Transportation California Environmental Quality Code of Federal Regulations community noise equivalent level decibels A-weighted decibels Federal Transit Administration heating, ventilation, and air conditioning inches per second day-night noise level equivalent energy level maximum noise level minimum noise level Marine Corps Air Station noise-sensitive land use Padre Dam Municipal Water District peak particle velocity Roadway Construction Noise Model recreational vehicle State Route
10,	
211	
UTV	utility task vehicle
VdB	vibration decibels

Section 1 Summary

This report assesses potential noise and vibration impacts associated with implementation of the Fanita Ranch Project (proposed project). This report examines the impacts of the proposed project and proposes mitigation measures where necessary and feasible to address significant noise impacts.

The noise and vibration analysis concluded that implementation of the proposed project would have the potential to result in five significant impacts: (1) nighttime nuisance noise from potential use of Special Use area, (2) excessive noise levels as a result of permanent increases in ambient noise levels, (3) exposure of new noise-sensitive land use (NSLU) to noise levels in excess of land use compatibility standards, (4) excessive noise levels during construction, and (5) groundborne vibration impacts during roadway construction. These impacts are summarized in Table 1. Mitigation Measure NOI-1 would reduce nuisance noise from the Special Use area to a less than significant level. Mitigation Measure NOI-2 would reduce impacts from traffic noise levels to certain receptors to less than significant but would not fully mitigate impacts to any entire segment due to infeasibility. Mitigation Measure NOI-3 would reduce operational impacts related to on-site noise compatibility to a less than significant level. Mitigation Measures NOI-4 and NOI-5 would reduce temporary ambient noise levels increases from construction vehicle trips to a less than significant level. Mitigation Measures NOI-6 and NOI-7 would reduce impacts related to construction equipment noise levels to a less than significant level. Mitigation Measures NOI-8 and NOI-9 would reduce groundborne vibration impacts to a less than significant level. Impacts related to aircraft operations would be less than significant without mitigation. Table 2 provides a crosswalk for mitigation measure numbering between the Fanita Ranch Draft Revised Environmental Impact Report, Section 4.13, Noise, and this Noise Technical Report.

	-							
Threshold	Impact	Significance Before Mitigation	Mitigation	Significance After Mitigation				
Project Impacts								
Exceedance of Noise Standards	The proposed project would have the potential to generate substantial temporary noise during construction and permanent increases in ambient noise levels during operation.	Potentially significant	Special Use Area Noise Measures (NOI-1), Noise Barrier Installation (NOI-2), On-Site Ambient Noise Exposure (NOI-3), Construction Access Road Speed Limitations (NOI-4), Vendor Trip Route Limitations (NOI-5), Roadway Construction Notification (NOI-6), Nighttime Noise Sound Management Plan (NOI-7)	Significant and unavoidable (permanent increase in traffic noise levels); less than significant (construction and project operation)				
Excessive Groundborne Vibration or Noise	Construction activities including blasting may result in substantial temporary increase in groundborne vibration and/or noise levels.	Potentially significant	Roadway Construction Notification (NOI-6), Nighttime Noise Sound Management Plan (NOI-7), Vibration Best Management Practices (NOI-8), Construction Vibration Notification (NOI-9)	Less than significant				
Aircraft Noise	The proposed project would not expose people residing or working on the project site to excessive noise levels resulting from aircraft noise.	Less than significant	No mitigation required	Less than significant				
		Cumulativ	ve Impacts					
Exceedance of Noise Levels	A cumulatively considerable impact as a result of cumulative growth through Year 2035 would occur on a total of seven roadway segments.	Potentially significant	Noise Barrier Installation (NOI-2)	Cumulatively considerable and unavoidable				
Excessive Groundborne Vibration	A significant cumulative vibration impact would not occur.	Less than significant	No mitigation required	Not cumulatively considerable				
Aircraft Noise	A cumulative impact related to aircraft noise would not occur.	Less than significant	No mitigation required	Not cumulatively considerable				

Table 1. Summary of Impacts

Noise Technical Report	Environmental Impact Report Section 4.12, Noise
NOI-1: Special Use Area Noise Measures	NOI-5
NOI-2: Noise Barrier Installation	NOI-6
NOI-3: On-Site Ambient Noise Exposure	NOI-7
NOI-4: Construction Access Road Speed Limitations	NOI-1
NOI-5: Vendor Trip Route Limitations	NOI-2
NOI-6: Roadway Construction Notification	NOI-3
NOI-7: Nighttime Noise Sound Management Plan	NOI-4
NOI-8: Vibration Best Management Practices	NOI-8
NOI-9: Construction Vibration Notification	NOI-9

Table 2. Noise Mitigation Measure Equivalency Table

Section 2 **Project Description**

The main components of the proposed project are summarized below.

2.1 Project Location and Regional Context

The project site consists of approximately 2,638 acres in the northern portion of the City of Santee (City) in eastern County of San Diego (County). The City is located approximately 18 miles east of downtown San Diego and the Pacific Ocean (see Figure 1, Regional Location). The project site is north of State Route (SR-) 52 and west of SR-67 (see Figure 2, Project Site). Access to the project site would be provided by the northerly extension of Fanita Parkway and Cuyamaca Street and the extension of Magnolia Avenue to Cuyamaca Street. The project site is bordered by Marine Corps Air Station (MCAS) Miramar and Padre Dam Municipal Water District (PDMWD) facilities and Santee Lakes Recreation Preserve to the west; open space/recreational areas, including Goodan Ranch/Sycamore Canyon County Preserve, to the north and west; existing City residential neighborhoods to the south; and Eucalyptus Hills, an existing residential community in the County's jurisdiction, to the east.

2.2 Fanita Ranch Project

The proposed project proposes to develop a master planned community consisting of up to 2,949 residences under the preferred land use plan with school, or 3,008 units under the land use plan without school, up to 80,000 square feet of commercial uses, a school site, parks, open space, and agricultural uses (see Figure 3, Conceptual Land Use Plan, and Appendix A, Site Utilization Plan Statistical Summary). The proposed project would implement a Specific Plan that preserves approximately 63 percent of the project site as a permanent Habitat Preserve (approximately 1,650.4 acres). Development would be clustered within three villages: Fanita Commons, Orchard Village, and Vineyard Village. Each village would be defined by its unique design theme, location, physical characteristics, and mix of housing types and land uses. In addition to the villages, the Specific Plan would include a 31.9-acre Special Use area located in the southwest portion of the project site. The proposed project would provide approximately 78 acres of public and private parks distributed throughout the three villages, including a 31.2-acre Community Park, 30.4 acres of Neighborhood Parks, and approximately 16.4 acres of Mini-Parks and paseos. The Farm would be approximately 27.3 acres, with an additional 10.9 acres of agricultural land uses throughout the site. Approximately 256 acres of open space, outside of the Habitat Preserve, would include manufactured open space slopes, fuel modification areas, trails, water quality/hydromodification basins, pump stations, and water tanks.

Each village/development area and key project components are summarized below.

2.2.1 Fanita Commons

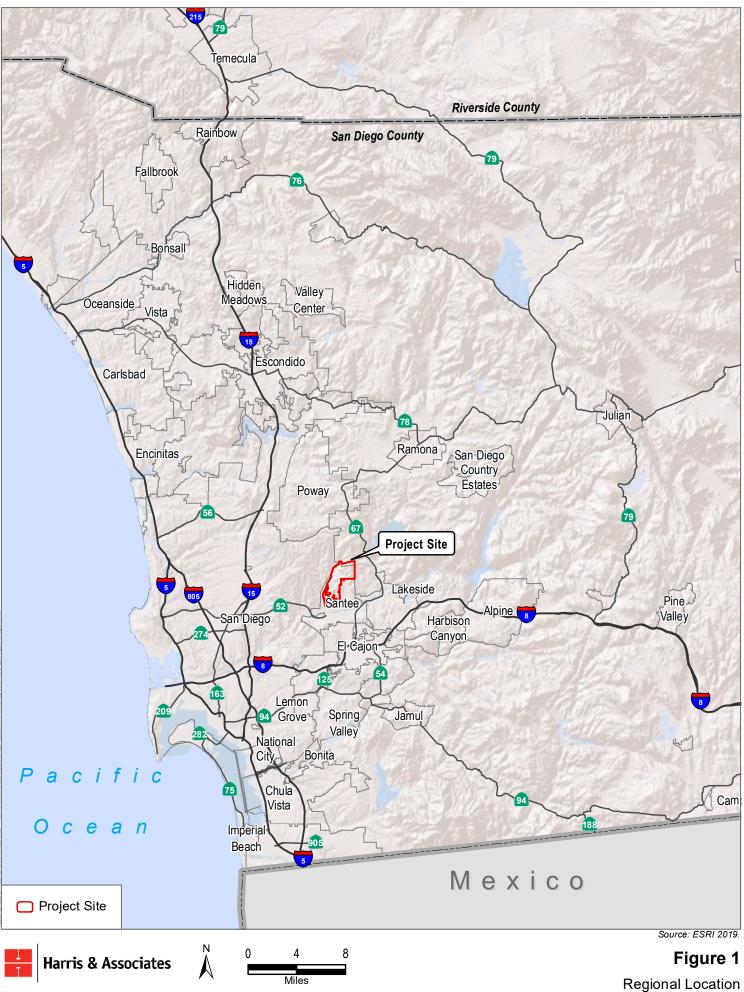
Fanita Commons would be in the northwest portion of the project site and is planned as the primary activity center for the proposed project. Fanita Commons would include a mixed-use Village Center, an Active Adult neighborhood, a K–8 school site, a Community Park, a working farm, and two preserved natural drainages with an adjoining Linear Park. With the Farm as its focal point, orchards, vineyards, fields, and a barn for community events would define this village. The mixed-use Village Center would allow for up to 40,000 square feet of commercial uses and residential, recreation, and civic uses, including a site for a new City fire station. A 15-acre school site, the underlying Medium Density Residential land use designation would be implemented. In that case, the maximum total number of units permitted in the Specific Plan would increase by 59 units for a total of 3,008 units. Fanita Commons would include a total of 768 residential units, including 445 Active Adult residences and 323 residences within the mixed-use Village Center.

2.2.2 Orchard Village

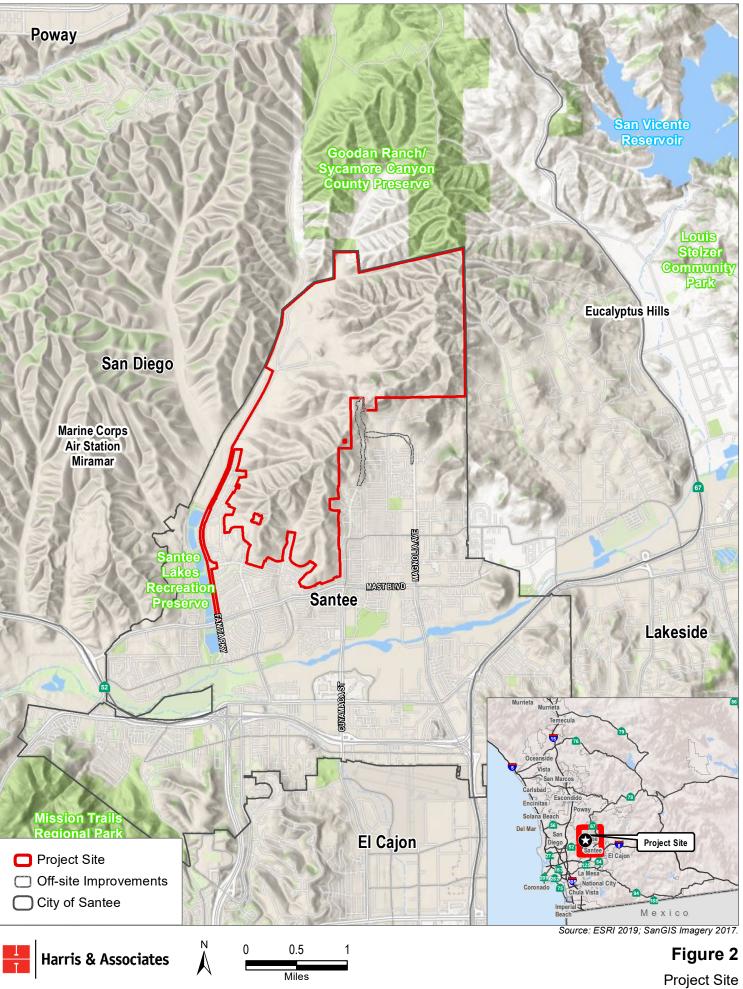
Orchard Village would be located south of Fanita Commons and consists of residential land uses, Neighborhood and Mini-Parks, and a centrally located mixed-use Village Center. Orchard Village would provide a total of 855 residential units, including 454 Low Density Residential) residences, 368 Medium Density Residential residences and 33 residences within the mixed-use Village Center. Open space and a linear riparian area geographically and topographically would separate Orchard Village from Fanita Commons. Roadways, trails, and a pedestrian bridge would connect Orchard Village to Fanita Commons. A neighborhood-serving Village Center would include up to 10,000 square feet of retail, office, and commercial uses. Orchard Village would also include Neighborhood Parks and Mini-Parks.

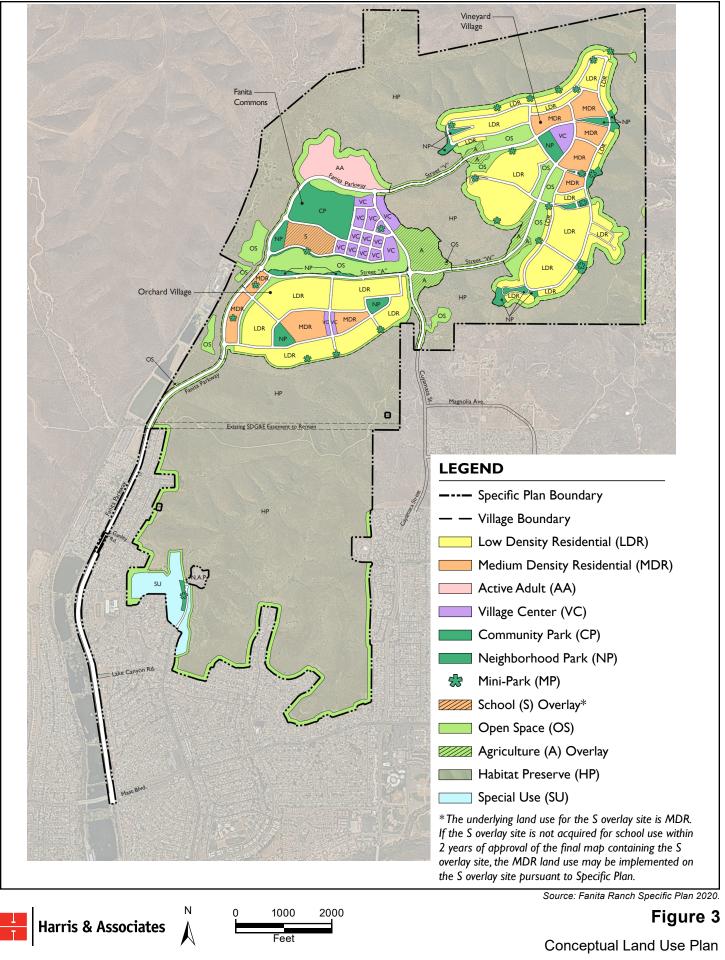
2.2.3 Vineyard Village

Vineyard Village would be located in the northeastern portion of the project site. Vineyard Village would be separated from the other two villages by an open space/wildlife corridor within the Habitat Preserve. Two local streets would connect Vineyard Village to Fanita Commons and Orchard Village. Vineyard Village would provide a total of 1,326 residential units including 749 Low Density Residential residences, 498 Medium Density Residential residences, and 79 residences within the mixed-use Village Center. The neighborhood-serving Village Center would include up to 10,000 square feet of retail and office uses. Vineyard Village would also feature agricultural land planned for vineyards, as well as Neighborhood Parks and Mini-Parks.



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2.2.4 Habitat Preserve

The Habitat Preserve would be composed of approximately 1,650.4 acres of permanently preserved open space. The biological areas within the Habitat Preserve would be conserved and managed in perpetuity and protected through permanently funded management plans and funding mechanisms. Permitted uses within the Habitat Preserve would include water quality features, water reservoirs and pump stations, utilities and utility access roads, trails, and revegetated slopes. Restoration and management of the Habitat Preserve would be conducted as prescribed by the Natural Community Conservation Plan design guidelines and standards and City's 2018 Draft Multiple Species Conservation Program Subarea Plan.

2.2.5 Farm

The Farm would be the community focal point for the proposed project. The approximately 27.3acre Farm would be located along the eastern edge of Fanita Commons, near the center of the proposed project. An event barn featuring iconic agrarian architecture would set the theme for the community and provide a venue for special events and farming operations. The working Farm is planned to include terraced vegetable fields, pasture lands, limited housing for employees, raised gardens, and small-scale animal husbandry. A community-supported agriculture program is planned for the Farm. Food grown on the Farm may be distributed to local schools, restaurants, and other institutional facilities, such as the congregate care and assisted living facilities.

2.2.6 Special Use Area

The Special Use area would be composed of approximately 31.9 acres in the southwestern corner of the project site east of Fanita Parkway and west of an existing PDMWD Carlton Hills water reservoir. Permitted uses for the Special Use area would include water quality basins, the extension of Carlton Hills Boulevard, a solar farm, recreational vehicle (RV) and boat storage, or aboveground agriculture. Access to the Special Use area would be provided by Carlton Hills Boulevard. A Mini-Park would be along the eastern perimeter of the Special Use area and provide trail staging and parking areas for trail users on the project site.

2.2.7 Parks, Trails, and Recreational Facilities

The proposed project would include a coordinated system of parks and non-motorized use trails that connect to the three villages, regional trails, and surrounding open space areas, including the Habitat Preserve. Approximately 78 acres of public and private parks would be distributed throughout the three villages. The Community Park, located in Fanita Commons, would provide for both active and passive recreation opportunities. Neighborhood Parks are planned in key locations to provide recreational opportunities within walking distance of all residences. Mini-Parks would provide trailheads, overlooks, and passive recreational opportunities. A series of trails and paths would connect the Farm to the villages in the proposed project.

2.2.8 Mobility (On Site)

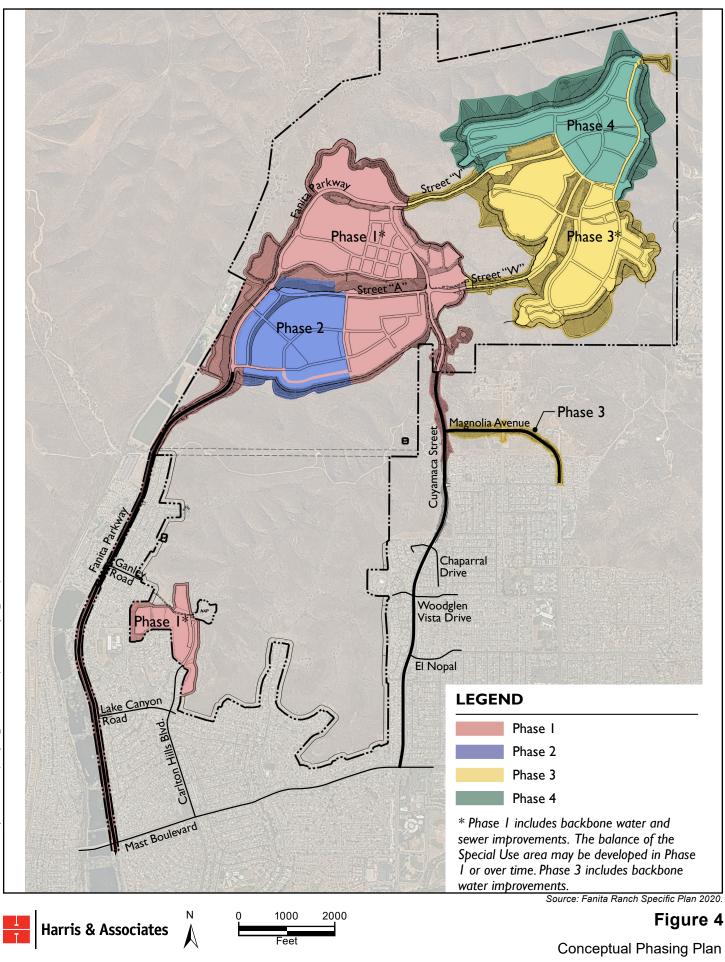
The Fanita Ranch Specific Plan would establish an on-site roadway network and street cross sections designed as a system of complete streets that support motorists, pedestrians, bicyclists, and transit users. On-site streets would generally be two lanes and include traffic calming measures such as gateways, roundabouts, narrowed travel lanes, on-street bike facilities and parking, a chicane, raised crosswalks, and intersection pop-outs. On-site streets that cross open space areas would be designed to minimize impacts to sensitive habitat and to accommodate wildlife crossings.

2.2.9 Mobility Improvements

Mobility improvements would include the extension of three roadways identified in the Santee General Plan Mobility Element: (1) the extension of Fanita Parkway from Ganley Road through the project site, (2) the extension of Cuyamaca Street from north of Chaparral Drive through the project site, and (3) the extension of Magnolia Avenue from its current northern limit to Cuyamaca Street. Additionally, the proposed project proposes to widen Fanita Parkway between Mast Boulevard and Lake Canyon Road and modify Cuyamaca Street from Mast Boulevard to Chaparral Drive to consist of a four-lane divided street with two travel lanes in each direction, bicycle lanes, and sidewalks.

2.2.10 Development Phasing

The proposed project would be developed in four phases over a 10- to 15-year period, as shown on Figure 4, Conceptual Phasing Plan. Phases would overlap or vary depending on market conditions and may be broken down into smaller subphases. Construction is anticipated to begin in 2021. The Special Use area would not be tied to development phasing and may be developed anytime during project buildout; however, water infrastructure in the Special Use area would be constructed during Phase 1.



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Section 3 Existing Conditions

3.1 Noise Basics

3.1.1 Quantification of Noise

The California Department of Transportation (Caltrans) defines noise as sound that is loud, unpleasant, unexpected, or undesired. Further, for the purposes of noise analysis, noise only exists if a source, path, and receiver are present. Sound pressure waves must be produced by a source and transmitted through a medium, such as air. The sound must be perceived by, registered by, or affect a receptor, such as an ear or noise monitoring device (Caltrans 2013a).

Sound pressure levels are quantified using a logarithmic ratio of actual sound pressures to a reference pressure squared, called bels. A bel is typically divided into tenths, or decibels (dB). Sound pressure alone is not a reliable indicator of loudness because frequency (or pitch) also affects how receptors respond to the sound. To account for the pitch of sounds and the corresponding sensitivity of human hearing to them, the raw sound pressure level is adjusted with a frequency-dependent A-weighting scale that is stated in units of decibels (dBA) (Caltrans 2013a). Typical A-weighted noise levels are listed in Table 3.

Common Outdoor Activities	Noise Level (dBA)	Common Indoor Activities	
	<u> </u>	Rock band	
Jet flyover at 1,000 feet			
	— 100 —		
Gas lawn mower at 3 feet			
	<u> </u>		
Diesel truck at 50 feet at 50 miles per hour		Food blender at 3 feet	
	<u> </u>	Garbage disposal at 3 feet	
Noisy urban area, daytime			
Gas lawn mower, 100 feet	<u> </u>	Vacuum cleaner at 10 feet	
Commercial area		Normal speech at 3 feet	
Heavy traffic at 300 feet	<u> </u>		
		Large business office	
Quiet urban daytime	— 50 —	Dishwasher next room	
Quiet urban nighttime	<u> </u>	Theater, large conference room (background)	
Quiet suburban nighttime			
	— 30 —	Library	
Quiet rural nighttime		Bedroom at night	

Table 3. Typical A-Weighted Noise Levels

Common Outdoor Activities	Noise Level (dBA)	Common Indoor Activities	
	<u> </u>		
		Broadcast/recording studio	
	<u> </u>		
Lowest threshold of human hearing	— 0 —	Lowest threshold of human hearing	

Table 3. Typical A-Weighted Noise Levels

Source: Caltrans 2013a.

Note: dBA = A-weighted decibel

A receptor's response to a given noise may vary depending on the sound level, duration of exposure, character of the noise sources, the time of day during which the noise is experienced, and the activity affected by the noise. Activities most affected by noise include rest, relaxation, recreation, study, and communications. In consideration of these factors, different measures of noise exposure have been developed to quantify the extent of the effects from a variety of noise levels. For example, some measures consider the 24-hour noise environment of a location by using a weighted average that penalizes noise levels during normal relaxation and sleep hours. Other measures consider an average noise level over a period of time that includes ambient noise and a steady-state noise source for a given period of time within the averaging period (Caltrans 2013a). The indices for measuring community noise levels that are used in this report are defined below:

Lmax, the maximum noise level, is the highest instantaneous noise level during a specified time period.

Lmin, the minimum noise level, is the lowest instantaneous noise level during a specified time period.

Leq, the equivalent energy level, provides an average acoustical or sound energy content of noise, measured during a prescribed period, such as 1 minute, 15 minutes, 1 hour, or 8 hours. The sound level may not be constant over the measured time period, but the average decibel sound level, given as dBA Leq, contains an equal amount of energy as the fluctuating sound level.

Ldn, the day-night noise level, is a 24-hour Leq, except that the nighttime hours (10:00 p.m. to 7:00 a.m.) are assessed a 10 dBA penalty. This penalty attempts to account for the fact that nighttime noise levels are potentially more disturbing than equal daytime noise levels. The community noise equivalent level (CNEL) is similar to Ldn, except an additional +5 dBA weighting is applied to all sound occurring between 7:00 p.m. and 10:00 p.m. The City uses Ldn to measure noise in the City; therefore, Ldn is used in this analysis (City of Santee 2003). Ldn and CNEL are typically within 1 dBA of each other and, for most intents and purposes, are interchangeable.

The decibel level of a sound decreases (or attenuates) as the distance from the source of that sound increases. For a single point source, such as a piece of mechanical equipment, the sound level normally decreases by about 6 dBA for each doubling of distance from the source. Sound that originates from a linear, or "line" source such as vehicular traffic, attenuates by approximately 3 dBA per doubling of distance. Other contributing factors that affect sound reception include ground absorption, topography that provides a natural barrier, meteorological conditions, or the presence of human-made obstacles such as buildings and sound barriers (Caltrans 2013a). Noise from roadways in environments with major ground effects may yield attenuation rates as high as 4.5 dBA for each doubling of distance due to vegetation and loose soils that would reduce noise levels by either absorbing or scattering the sound (WSDOT 2019).

3.1.2 Noise Effects

Reaction to a given sound varies depending on acoustical characteristics of the source and the environment of the receptor. The A-scale deemphasizes low-frequency sounds because humans are more sensitive to high-frequency sounds that are more likely to cause hearing damage. People tend to compare an intruding noise to existing background noise levels. If a new noise is considerably louder or noticeable above existing levels, it is generally considered objectionable. The activity that the receptor is engaged in also affects response. For example, the same noise source, such as constant freeway traffic, may be more objectionable to people sleeping than to workers in a factory. A 3 dBA change is the smallest increment that is perceptible by most receivers, and a 5 dBA change in community noise level is clearly noticeable. Generally, 1 to 2 dBA changes are not detectable, except under controlled laboratory conditions. A sound that is 10 dBA greater than the reference sound is typically perceived as twice as loud (Caltrans 2013a).

3.2 Environmental Vibration Basics

Vibration is defined as dynamic excitation of an elastic system, such as the ground or a structure, which results in oscillatory movement of the system (Caltrans 2013b). Typical human-made causes of earthborne vibration include trains and construction activities such as blasting, pile-driving, and operation of heavy earthmoving equipment (FTA 2018). The resulting waves transmitted through solid material are referred to as structureborne or groundborne vibration. Vibration energy spreads out as it travels through the ground, causing the vibration amplitude to decrease with distance away from the source. The vibration levels inside a building depend on the vibration energy that reaches the foundation and the characteristics of the structure that affect propagation of the vibration through it. A heavier building will typically experience lower vibration levels. The most common impact associated with vibration is annoyance resulting from the effects of vibration, such as building movement, rattling of windows, shaking of items on shelves or walls, and rumbling sounds. In more extreme cases, building damage may occur. Because the effects of vibration elicit a greater response than the vibration itself, vibration is typically only perceptible to people inside buildings (FTA 2018).

Vibration levels are typically expressed in terms of the peak particle velocity (PPV) and root mean square amplitude, both in inches per second (in/sec). PPV is most appropriate for evaluating building damage potential. Caltrans estimates that continuous vibration levels of less than 0.08 PPV and single-event vibration levels of less than 0.12 PPV do not result in damage to even the most fragile historic buildings (Caltrans 2013b). The Federal Transit Administration (FTA) has identified a maximum PPV of 0.2 in/sec for fragile buildings and 0.12 in/sec for extremely fragile historic buildings (FTA 2018).

PPV does not account for human response to vibration. The root mean square amplitude is used to represent average vibration amplitude, which accounts for the time it takes for the human body to respond to vibration signals. The root mean square amplitude is also given in decibel notation, referenced as vibration decibels (VdB), which serves to compress the range of numbers required to describe vibration relative to human response (FTA 2018). The general human response to different groundborne vibration velocity levels is described in Table 4.

Vibration	Noise Level			
Velocity Level	Low Mid Frequency Frequency		Human Reaction	
65 VdB	25 dBA	40 dBA	Approximate threshold of perception for many people. Mid-frequency sound may disturb sleep.	
75 VdB	35 dBA	50 dBA	Approximate dividing line between barely perceptible and distinctly perceptible. Many people find that transportation-related vibration at this level is annoying. Mid-frequency noise disturbs sleep and is considered annoying in more quiet areas.	
85 VdB	45 dBA	60 dBA	Vibration acceptable only if there are an infrequent number of events per day. Low-frequency noise disturbs sleep and mid-frequency noise can be annoying to daytime NSLUs, such as schools.	

Table 4. Human Response to Different Levels of Groundborne Vibration

Source: FTA 2018.

Note: dBA = A-weighted decibel; NSLU = noise-sensitive land use; VdB = vibration decibel

The rumbling sound caused by the vibration of room surfaces is called groundborne noise. Like airborne noise, groundborne noise is measured in dBA. The sound level accompanying vibration is generally 25 to 40 dBA lower than the vibration velocity level in VdB, as shown in Table 4. Due to its low-frequency components, groundborne noise sounds louder than broadband noise with the same noise level (FTA 2018). Typical human response to groundborne noise levels are shown in Table 4. The background vibration velocity level in residential areas is usually around 50 VdB, which is below the 65 VdB threshold of human perception (FTA 2018). The same human reaction corresponds to a given vibration velocity level and its resulting noise level; therefore, for simplicity, this analysis refers only to a source's VdB to describe potential human response to groundborne vibration and noise.

3.3 Regulatory Framework

3.3.1 Federal

3.3.1.1 Federal Aviation Administration Standards

Enforced by the Federal Aviation Administration, Code of Federal Regulations, Title 14, Part 150, prescribes the procedures, standards, and methods governing the development, submission, and review of airport noise exposure maps and airport noise compatibility programs, including the process for evaluating and approving or disapproving those programs. Title 14 also identifies those land uses which are normally compatible with various levels of exposure to noise by individuals. The Federal Aviation Administration considers residential land uses to be compatible with exterior noise levels at or less than 65 dBA Ldn.

3.3.1.2 Federal Transit Administration Standards

Although the FTA standards are intended for federally funded mass transit projects, the impact assessment procedures and criteria included in the FTA Transit Noise and Vibration Impact Assessment Manual (September 2018) are routinely used for projects proposed by local jurisdictions. The manual includes criteria for assessing the impacts of groundborne vibration, presented in Table 5.

	Impact Levels (VdB)			
Land Use Category	Frequent Events ¹	Occasional Events ²	Infrequent Events ³	
Category 1: Buildings where vibration would interfere with interior operations	65	65	65	
Category 2: Residences and buildings where people normally sleep	72	75	80	
Category 3: Institutional land uses with primarily daytime uses	75	78	83	

 Table 5. FTA Groundborne Vibration Impact Criteria

Source: FTA 2018.

Notes: VdB = vibration decibel

Vibration levels are measured in or near the vibration-sensitive use.

¹ "Frequent Events" are defined as more than 70 vibration events of the same source per day.

² "Occasional Events" are defined as between 30 and 70 vibration events of the same source per day.

³ "Infrequent Events" are defined as fewer than 30 vibration events of the same source per day.

3.3.1.3 Noise Control Act

The Noise Control Act of 1972 identified uncontrolled noise as a danger to health and welfare, particularly for people in urban areas. Responsibility for noise control remains primarily a state and local issue; however, the Noise Control Act established a means for effective coordination of federal research and noise control activities (USEPA 2019). The act included a directive that the U.S. Environmental Protection Agency develop and publish information on noise levels to protect public health and welfare with an adequate margin of safety. In 1974, the U.S. Environmental

Protection Agency published the document "Information on Levels of Environmental Noise Requisite to Protect Public Health and Welfare with an Adequate Margin of Safety." The document identifies an interior noise level of 45 dBA Ldn in indoor residential areas to be adequate to protect indoor activity from interference and annoyance. An exterior noise level of 55 dBA Ldn was identified as the maximum noise level to avoid interference and annoyance in residential areas and other areas in which quiet is a basis for use. A maximum 24-hour average outdoor noise level of 70 dBA Leq is recommended to prevent hearing loss (USEPA 1974).

3.3.2 State

3.3.2.1 California Noise Control Act of 1973

Sections 46000 through 46080 of the California Health and Safety Code, known as the California Noise Control Act of 1973, find that excessive noise is a serious hazard to the public health and welfare and that exposure to certain levels of noise can result in physiological, psychological, and economic damage. The California Noise Control Act declares that the State of California has a responsibility to protect the health and welfare of its citizens by the control, prevention, and abatement of noise. It is the policy of the state to provide an environment for all Californians free from noise that jeopardizes their health or welfare. Section 46050.1 of the act mandates development guidelines for the preparation and content of General Plan Noise Elements.

3.3.3 Local

3.3.3.1 Santee General Plan

The Noise Element of the Santee General Plan contains goals and policies to control and abate environmental noise and to protect the citizens of Santee from excessive exposure to noise. The Santee General Plan establishes an exterior ambient noise standard of 65 dBA Ldn for NSLUs. This criterion is applied at the rear yard areas of single-family residences and ground floor common areas and private patio areas for multi-family residences. For other NSLUs, such as libraries, schools, or hospitals, noise-sensitive areas shall be those areas that serve a significant function for the use that could be adversely affected by noise. For example, for schools, it is applied to outdoor teaching or discussion areas (does not include playgrounds or other active outdoor areas).

Table 6 presents the Noise Element guidelines for determining acceptable and unacceptable community noise exposure limits for various land use categories. Normally acceptable noise levels are defined as satisfactory, based on the assumption that any buildings involved are of normal conventional construction, without any special noise insulation requirements. Conditionally acceptable noise levels indicate that new construction or development should be undertaken only after a detailed analysis of the noise reduction requirements is made and needed noise insulation features have been included in the design. Conventional construction with closed windows and fresh air supply systems or air conditioning will normally suffice. The Santee General Plan states

that these compatibility guidelines are not prohibitive but should be used as a guide and a resource.¹ Additionally, the Santee General Plan Noise Element contains the following objectives and policies that are applicable to new development in the City:

- **Objective 1.0:** Control noise from sources adjacent to residential, institutional and other noise-sensitive receptors.
 - **Policy 1.1:** The City shall support a coordinated program to protect and improve the acoustical environment of the City including development review for new public and private development and code compliance for existing development.
 - **Policy 1.2:** The City shall utilize noise studies and noise contour maps when evaluating development proposals during the discretionary review process.
 - **Policy 1.4:** The City shall promote alternative sound attenuation measures rather than traditional wall barrier wherever feasible; these may include glass or polycarbonate walls, berms, landscaping, and the siting of noise-sensitive uses on a parcel away from the roadway or other noise source.
 - **Policy 1.5:** The City shall review future projects with particular scrutiny regarding the reduction of unnecessary noise near noise-sensitive areas such as hospitals, schools, parks, etc.
- **Objective 2.0:** Ensure that future developments will be constructed to minimize interior and exterior noise levels.
 - **Policy 2.1:** The City shall adhere to planning guidelines and building codes which include noise control for the exterior and interior living space of all new residential developments within noise impacted areas.
 - Policy 2.2: The City should require new development to mitigate noise impacts to existing uses resulting from new development when: (1) such development adds traffic to existing City streets that necessitates the widening of the street; and (2) the additional traffic generated by new development causes the noise standard or significance thresholds to be exceeded.
 - Policy 2.3: The City should not require new development to mitigate noise impacts to existing uses when new development only adds traffic already anticipated by the City's General Plan to an existing street, but does not necessitate widening of that street.

¹ See page 7-14 of the Santee General Plan Noise Element in Section 8.1, Local Regulations.

Table 0. Santee General Flan Land Ose Compatibility Guidennes (Lun)				
Land Use Category	Normally Acceptable	Conditionally Acceptable	Normally Unacceptable	Clearly Unacceptable
Residential – Low Density, Single- Family, Duplex, Mobile Homes	50–65	65–70	70–75	75–85
Residential – Multiple Family	50–65	65–70	70–75	75–85
Transient Lodging – Motel, Hotels	50–65	65–70	70–80	80–85
Schools, Libraries, Churches, Hospitals, Nursing Homes ¹	50–65	65–70	70–80	80–85
Auditoriums, Concert Halls, Amphitheaters	50–60	60–70	NA	70–85
Sports Arenas, Outdoor Spectator Sports	50–65	65–75	NA	75–85
Playgrounds, Neighborhood Parks	50–70	NA	70–75	75–85
Golf Courses, Riding Stables, Water Recreation, Cemeteries	50–75	NA	75–80	80–85
Office Buildings, Business Commercial, and Professional	50–70	70–75	75–85	NA
Industrial, Manufacturing, Utilities, Agriculture	50–75	75–80	80–85	NA

 Table 6. Santee General Plan Land Use Compatibility Guidelines (Ldn)

Source: City of Santee 2003.

Notes: Ldn = day-night noise level; NA = not applicable

¹ Applies to noise-sensitive areas which serve a significant function for the use which could be adversely affected by noise such as outside areas used primarily for instruction, meditation areas, rest and relaxation areas, and other areas where general peace and quiet are important.

Normally Acceptable: Specified land use is satisfactory, based upon the assumption that any buildings involved are of normal conventional construction, without any special noise insulation requirements.

Conditionally Acceptable: New construction or development should be undertaken only after a detailed analysis of the noise reduction requirements is made and needed noise insulation features have been included in the design. Conventional construction, but with closed windows and fresh air supply systems or air conditioning, will normally suffice.

Normally Unacceptable: New construction or development should be discouraged. If new construction or development does proceed, a detailed analysis of the noise reduction requirements must be made and needed noise insulation features must be included in the design.

Clearly Unacceptable: New construction or development should generally not be undertaken.

The Noise Element further states that when new development may result in the exposure of existing or future noise-sensitive uses to noise levels in excess of 65 dBA Ldn, an acoustical study will be required. If the acoustical study shows that the noise levels at any noise-sensitive area will exceed 65 dBA Ldn, the development should not be approved unless the following findings are made:

- a. Modifications to the development have been, or will be made, which will reduce the exterior noise levels in noise-sensitive areas to 65 dB Ldn or less, or
- b. If, with current noise abatement technology, it is not feasible to reduce the exterior noise levels to 65 dBA Ldn or less, then modifications to the development have been, or will be made, which reduce the exterior noise level to the maximum extent feasible and the interior noise level to 45 dB Ldn or less. Particular attention shall be given to noise-sensitive spaces such as bedrooms.

c. For rooms in noise-sensitive areas which are occupied only for a part of the day (schools, libraries, or similar), the interior 1-hour average sound level during occupation, due to noise outside, should not exceed 45 dBA Leq.

Further, noise impacts shall be considered significant if any of the following occur as a result of the proposed development:

- 1. If, as a direct result of the proposed development, noise levels for any existing or planned development will exceed the noise levels considered compatible for that use as identified in Table 6.
- 2. If, as a direct result of the proposed development, noise levels which already exceed the levels considered compatible for that use are increased by 3 dB or more.

If mitigation is necessary, the City, in Section 8.0 of the Noise Element, Implementation, lists the following measures that may be incorporated into a proposed project as mitigation measures. The following measures are not required, and mitigation is not limited to this list:

- 1. The use of site design techniques, such as the provision of buffers to increase distances between the noise source and receiver, siting of buildings and parking areas, and the careful siting of noise-sensitive outdoor features to minimize noise impacts
- 2. Provision of berms, landscaping, and other sound barriers, without the exclusive use of walls (e.g., a combination of a small wall and a berm in concert with the overall streetscape in the area could be appropriate)
- 3. Insulation of buildings against noise, including thicker-than-standard glazing and mechanical ventilation
- 4. Improvement of traffic circulation to "smooth" flow by such measures as interconnecting traffic signals
- 5. Consideration of the use of innovative construction technologies and materials in constructing or reconstructing streets
- 6. Setting of time limits on certain noisy activities
- 7. Purchasing of demonstrably quiet equipment for City use

3.3.3.2 City of Santee Noise Ordinance

The City's Noise Ordinance is found in Section 5.04 of the Santee Municipal Code (City of Santee 2020). Section 5.04.040, which establishes the City's noise regulation, generally prohibits nuisance noise and states that it is unlawful for any person to make, continue, or cause to be made or continued within City limits any disturbing, excessive, or offensive noise that causes discomfort or annoyance to reasonable persons of normal sensitivity residing in the area. This section details several specific sources of nuisance noise and outlines how it may be determined that the noise is in violation of the code. Specific sources of nuisance noise include, but are not limited to, devices for producing or reproducing sound, drums and other musical instruments, yelling, and animals.

Section 5.04.160 limits noise between 10:00 p.m. and 7:00 a.m. from sources that are not specifically addressed in the City's Noise Ordinance, or exempted from the ordinance, to levels that do not exceed average conversational levels at a distance of 50 feet from the property line from which the noise is being generated, or 50 feet from the source in a public area. The typical noise level for normal conversation is 65 dBA at 3 feet from the source (Caltrans 2013a).

Section 5.04.090, which specifically pertains to construction equipment, makes operation of any construction equipment outside the hours of 7:00 a.m. through 7:00 p.m., Monday through Saturday, except holidays, unlawful unless the operation is expressly approved by the Director of Development Services. Construction equipment with a manufacturer's noise rating of 85 dBA Lmax or greater may only operate at a specific location for 10 consecutive workdays. If work involving such equipment would involve more than 10 consecutive workdays, a notice must be provided to all property owners and residents within 300 feet of the site no later than 10 days before the start of construction. The notice must be approved by the City and describe the proposed project and the expected duration of work and provide a point of contact to resolve noise complaints.

The following noise sources are exempt in Section 5.04.170 of the City's Noise Ordinance:

- A. Sporting, Entertainment, Public Events:
 - 1. Reasonable sounds emanating from school band, school athletic, and school entertainment events;
 - 2. Sporting, entertainment and public events which are conducted pursuant to a license or permit issued by the City for which noise has been a consideration;
 - 3. Reasonable sounds emanating from a sporting, entertainment, or public event; provided, however, it is unlawful to exceed the average noise level at or within the property lines of any property which is developed and used either in part or in whole for residential purposes unless an exception has been granted allowing sounds in excess of the levels.
- B. Agricultural Operations. Equipment associated with agricultural operations may not exceed the average noise level, provided that all equipment and machinery powered by internal-combustion engines is equipped with a proper muffler and air intake silencer in good working order; and provided further, that:
 - 1. Motorized farm equipment operations do not take place between 7 p.m. and 7 a.m.;
 - 2. Such operations and equipment are used to protect or salvage agricultural crops during periods of potential or actual frost damage or other adverse weather conditions; or
 - 3. Such operations and equipment are associated with agricultural pest control through pesticide application, provided the application is made in accordance with all applicable laws, regulations and permits.

3.3.3.3 City of Santee Zoning Ordinance

Section 13.30.030 of the Zoning Ordinance, Performance Standards, applies to operation of land uses and states that no operation or activity is permitted which will create vibration noticeable without instruments at the perimeter of the subject property.

3.3.3.4 County of San Diego Noise Ordinance

Sensitive receptors east of the project site are in the unincorporated County. Section 36.404 of the County Municipal Code establishes hourly average sound level limits for non-construction noise. The daytime (7:00 a.m. to 10:00 p.m.) hourly average sound level limit for low-density residential areas is 50 dBA, and the nighttime (10:00 p.m. to 7:00 a.m.) hourly average sound limit is 45 dBA.

Section 36.409 of the County's Noise Ordinance establishes the following limit on construction: Except for emergency work, it shall be unlawful for any person to operate construction equipment or cause construction equipment to be operated that exceeds an average sound level of 75 dB for an 8-hour period between 7:00 a.m. and 7:00 p.m. when measured at the boundary line of the property where the noise source is located or on any occupied property where the noise is being received.

3.4 Existing Noise Environment

Existing noise sources that affect the project site are described below.

3.4.1 Existing Conditions

The project site is currently undeveloped and there are no noise-generating sources on the site. The primary existing sources of noise in the vicinity of the project site are vehicular traffic on local streets near the project site. The existing average daily traffic (ADT) volume ranges from 2,600 to 3,800 along Fanita Parkway, north of Mast Boulevard (LLG 2020). The existing traffic volume along Cuyamaca Street is 8,800 ADT between Mast Boulevard and El Nopal (LLG 2020). Other major area roadways include Mast Boulevard (7,700 to 26,000 ADT), Carlton Hills Boulevard (5,800 to 25,000 ADT), Magnolia Avenue (2,000 to 13,000 ADT north of Mast Boulevard), and SR-67 (77,000 to 93,000 ADT).

Land adjacent to the northern boundary of the property is under the jurisdiction of the County and is primarily undeveloped, with the exception of an aggregate mining facility (quarry), the westerly edge of which is located approximately 1,000 feet northeast of the project site on Slaughterhouse Canyon Road. Most of the quarry's operations occur on the eastern portion of the facility, separated from the project site by SR-67, more than 1 mile from the project site. Noise levels generated by equipment typical of mining in the County range from 50 to 91 dBA at 50 feet from the equipment (County of San Diego 2011). Due to distance and topography, the quarry is not a source of noise on the project site.

MCAS Miramar is north and west of the project site. This area includes thousands of acres of undeveloped land, much of it in its natural state. The portion adjacent to the proposed project is undeveloped. Aircraft noise generated from MCAS Miramar is described in Section 3.4.3, Transportation Noise Sources.

Land adjacent to the northwestern boundary of the project site development area is within the jurisdiction of the City of San Diego. These lands are designated for very-low-density residential, open space, and a sanitary landfill. Noise from the landfill operation to the project site is blocked by intervening topography. Due to the generally undeveloped nature of the land adjacent to the northern and western portions of the project site, existing noise levels within the northern portion of the project site are low. PDMWD facilities are located immediately to the west of the Fanita Parkway alignment, including Santee Lakes Recreation Preserve. This 190-acre area includes recreational facilities (boating, picnicking, camping, and fishing) and a wastewater treatment plant. The primary noise from this facility is the vehicle traffic on Fanita Parkway. A new residential neighborhood (Weston) is located west of the Santee Lakes Recreation Preserve recreational area.

Residential development occurs south of the project site in the City and east of the project site in the Eucalyptus Hills development in the unincorporated County. Noise levels in this area are also low, originating primarily from traffic in the residential areas.

3.4.2 Ambient Noise Monitoring

An ambient sound level survey was conducted on January 30, 2019, to quantify the noise environment within the project boundary and the surrounding vicinity. An additional survey was conducted on March 5, 2019, to characterize operational noise levels at the Coastal Roots Farm located at 441 Saxony Road in the City of Encinitas. This farm is similar to the proposed Farm and operated by the anticipated Farm manager. A total of 11 measurements were taken across the project site and in the residential neighborhoods surrounding the site. A total of three measurements were taken at the existing Coastal Roots Farm and surrounding residential neighborhood. The measurements were taken during the daytime (9:00 a.m. to 4:30 p.m.) and were 16 minutes in duration. A Larson Davis SoundExpert LxT Type I Integrating Sound Level Meter calibrated with a Larson Davis CAL200 calibrator was used to record ambient sound levels. Weather conditions during the measurements were calm with a mild temperature and partly-cloudy skies. Table 7 summarizes the measured Leq and noise sources for each monitoring location. The monitoring locations are shown on Figure 5, Project Area Noise Monitoring Locations, and Figure 6, Farm Noise Monitoring Locations.

Site	Location	Observed Noise Sources	Date/Time	Leq	Lmax	Lmin
		On-Site Proposed Project Noise Measurements				•
1	PDMWD Wastewater Treatment Plant near western edge of project site at proposed Orchard Village location	Sounds from operation of the facility, including running water, squealing from equipment, and a small tractor. Helicopter and small plane flyovers, and human activities including talking and bicycling	1-30-2019/ 9:28 a.m.	57.3	72.8	50.5
2	Area proposed for Low Density Residential use at southern boundary of Orchard Village	Gunfire from a small arms range at MCAS Miramar, jet and plane flyovers	1-30-2019/ 10:04 a.m.	54.6	77.3	31.0
3	Proposed Habitat Preserve area in the center of the project site surrounded by Orchard Village, Street "V," Vineyard Village, and Street "W"	Jet flyover, gunfire from a small arms range at MCAS Miramar, distant emergency vehicle sirens, bicyclists, birds	1-30-2019/ 10:50 a.m.	40.5	57.6	27.7
4	Area proposed for Active Adult community at northern boundary of Orchard Village	Jet and plane flyovers, birds, talking from hikers	1-30-2019/ 11:16 a.m.	57.4	76.0	31.7
5	Area proposed for Low Density Residential use at the northeast edge of Vineyard Village	Plane flyovers, birds, traffic on SR-67	1-30-2019/ 11:53 a.m.	60.7	83.5	38.4
6	Area proposed for Low Density Residential use at the southeast edge of Vineyard Village	Rooster cawing, birds, dogs, jet flyovers	1-30-2019/ 12:25 p.m.	45.0	61.2	30.2
7	Western project boundary at proposed Special Use area	Children playing and talking outside at Sycamore Canyon School, dog barking, distant construction noise, jet flyover	1-30-2019/ 2:21 p.m.	49.8	61.6	42.6
		Off-Site Santee Noise Measurements		•	•	
1	Intersection of Fanita Parkway and Ganley Road	Vehicle noise, pedestrian activity, dog barking, bicyclists, birds, distant plane flyover	1-30-2019/ 3:06 p.m.	61.2	80.0	38.2
2	Intersection of Fanita Parkway and Lake Canyon Road	Vehicle noise, small plane flyover, pedestrian activity	1-30-2019/ 3:25 p.m.	68.3	91.7	44.4
3	Intersection of Cuyamaca Street and El Nopal	Vehicle noise, helicopter flyovers	1-30-2019/ 3:50 p.m.	63.9	80.7	39.3
4	Intersection of Magnolia Avenue and Princess Joann Road	Vehicle noise, dogs barking, birds, pedestrian activity, helicopter flyovers	1-30-2019/ 4:12 p.m.	57.5	73.6	38.0

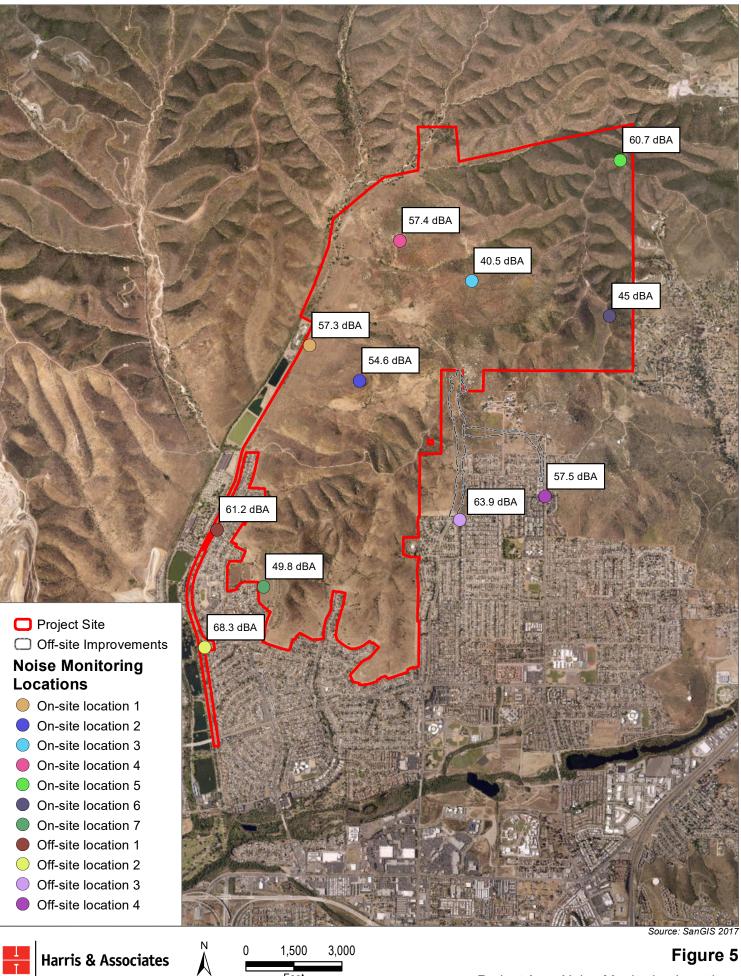
Table 7. Ambient Sound Level Measurements (dBA)

Site	Location	Date/Time	Leq	Lmax	Lmin				
Off-Site Escondido Farm Noise Measurements									
1	Saxony Road, north of Ecke Ranch Road, adjacent to residences	Vehicle noise on Saxony Road, normal conversation, use of hand tools, and UTV operation on farm property	3-5-2019/9:49 a.m.	59.6	70.6	45.4			
2	Coastal Road farm property in the center of the site, north of Ecke Ranch Road	Rooster cawing intermittently, vehicle noise, sprinkler operation, dumpster receptacle moving activity, normal conversation, birds	3-5-2019/10:12 a.m.	54.4	57.4	51.2			
3	Saxony Road, south of Ecke Ranch Road, adjacent to residences	Vehicle noise on Saxony Road, operation of farm truck and farm equipment, UTV operation, bicyclists, birds	3-5-2019/10:43 a.m.	66.7	78.3	48.0			

Table 7. Ambient Sound Level Measurements (dBA)

Note: dBA = A-weighted decibel; Leq = equivalent continuous sound level; Lmax = maximum sound level; Lmin = minimum sound level; PDMWD = Padre Dam Municipal Water District; UTV = utility task vehicle

Ambient measurements were 16 minutes in duration.



Feet

Project Area Noise Monitoring Locations

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The results of the ambient noise survey reflect daytime noise levels that range between 40.5 dBA Leq and 60.7 dBA Leq on the project site. The primary noise sources on the project site are birds, recreational use of the site, and intermittent flyovers. As described in Table 6, normally acceptable ambient community noise levels up to 65 dBA Ldn are considered compatible with residential development as specified in the Santee General Plan (City of Santee 2003). Ambient community noise levels of up to 70 dBA Ldn are acceptable for Neighborhood Parks and commercial buildings. Although the City's guidelines refer to 24-hour weighted average noise levels, daytime noise levels (Leq) were used in this study to screen for general noise compatibility. A daytime noise level that is within the General Plan compatible noise level range indicates general compatibility because this is when noise sources are at the highest levels. Based on these compatibility guidelines, ambient noise levels across the site are compatible with the proposed land uses. Measured noise levels at the off-site locations range from 57.5 dBA Leq to 68.3 dBA Leq. Daytime noise levels of 65 dBA Leq or less in the areas surrounding the project site would generally be considered normally acceptable under the City's compatibility guidelines, and all measurements are within the conditionally acceptable (acceptable with noise attenuation features) noise compatibility guideline of 70 dBA Ldn or below. Noise levels at the Coastal Roots Farm range between 54.4 dBA Leq and 66.7 dBA Leq, which is within the conditionally compatible noise standard for residences. However, the measurements and field notes indicate that the dominant noise source in the area of the Coastal Roots Farm is vehicle noise on Saxony Road. The result of the measurement taken at the center of the Coastal Roots Farm property was 54.4 dBA Leq, which is well within the normally compatibility guideline of 65 dBA Ldn for residential development.

3.4.3 Transportation Noise Sources

3.4.3.1 Aviation

MCAS Miramar is located adjacent to the west/northwestern boundary of the project site. The runways are located approximately 6 miles west of the project site. Aircraft currently flown at MCAS Miramar include F-35, F/A-18, KC-130, and C-12 aircraft, as well as CH-46 and CH-53 helicopters (MCAS Miramar 2018). The maximum presently authorized mission of the airfield is 112,242 annual aircraft operations. MCAS Miramar also typically hosts an annual air show that includes additional aircraft and higher than normal levels of aircraft operations during the event. As noise abatement measures for normal operations, fixed-wing aircraft and helicopter flight routes have been designed to follow major rail lines and highways or to remain over base property. The current Airport Land Use Compatibility Plan adopted by the County Airport Land Use Commission for MCAS Miramar indicates that the entire project site is outside the 60 dBA CNEL noise contour (SDCRAA 2011).

Gillespie Field airport operated by the County is also identified as a noise source in the Santee General Plan. This airport is located approximately 1.75 miles south of the project site in the City of El Cajon. Annual operations from Gillespie Field totaled approximately 233,969 flights in 2018 (County of San Diego 2020) and are projected to reach 294,050 by 2025 (SDCRAA 2010). The project site is located entirely outside of the 60 dBA CNEL noise contour for Gillespie Field; however, the Special Use area is within the overflight notification area (SDCRAA 2010).

3.4.3.2 Roadways

The proposed project lies north of SR-52 and west of SR-67 and would be accessed from the future northerly extensions of Fanita Parkway and Cuyamaca Street via Mast Boulevard and the future extension of Magnolia Avenue to Cuyamaca Street. There are no existing roadways on the project site. Table 8 shows the calculated existing noise levels generated by the roadways surrounding the project site. Existing noise levels were calculated using the methods described in Section 5.1.1.4. As shown in Table 8, existing noise levels from Mast Boulevard, Mission Gorge Road, Carlton Hills Boulevard, Cuyamaca Street, Magnolia Avenue, and SR-52 currently exceed the normally acceptable noise compatibility standard of 65 dBA Ldn for residences, schools, and other NSLUs. Noise generated along Mast Boulevard, Mission Gorge Road, Cuyamaca Street, and SR-52 currently exceeds the normally acceptable noise compatibility standard of 70 dBA Ldn for parks and commercial uses.

Roadway	Segment	Existing Average Daily Trips	Noise Level at 50 Feet from Roadway Centerline (dBA Ldn)
Mast Boulevard	SR-52 to West Hills Parkway	26,440	72
	West Hills Parkway to Medina Drive	19,540	70
	Pebble Beach Drive to Fanita Parkway	19,590	70
Mission Gorge Road	SR-125 to Fanita Drive	45,440	78
	Fanita Drive to Carlton Hills Boulevard	41,100	77
Fanita Parkway	Ganley Road to Lake Canyon Road	2,610	60
	Lake Canyon Road to Mast Boulevard	3,860	62
	Mast Boulevard to Carlton Oaks Drive	3,330	59
Carlton Hills Boulevard	Carlton Oaks Drive to Mission Gorge Road	24,960	69
Cuyamaca Street	Chaparral Drive to Woodglen Vista Drive	670	54
	Woodglen Vista Drive to El Nopal	4,360	62
	El Nopal to Mast Boulevard	8,860	66
	Mast Boulevard to River Park Drive	19,600	69
	River Park Drive to Town Center Parkway	26,690	70
	Town Center Parkway to Mission Gorge Road	21,850	72
Magnolia Avenue	Princess Joann Road to Woodglen Vista Drive	2,020	60
	Woodglen Vista Drive to El Nopal	9,030	67
	El Nopal to Mast Boulevard	13,690	68
SR-52	Santo Road to Mast Boulevard	96,000	77 ¹

Source: LLG 2020 (traffic data). See Appendix B for noise model assumptions and output.

Note: dBA = A-weighted decibel; Ldn = day-night noise level; SR- = State Route

¹ Noise level at 100 feet from centerline due to roadway width.

3.4.3.3 Railroads

The Green Line route of the San Diego Trolley operated by the Metropolitan Transit Service terminates in the Santee Town Center area at the northwest corner of Mission Gorge Road and Cuyamaca Street. It is not a significant noise generator in the City due to its intermittent operation and its alignment, which passes through a primarily commercial corridor on Cuyamaca Street (City of Santee 2003). Noise from the Green Line route typically does not exceed 60 dBA at 100 feet or more from the centerline of the track (RECON 2017). The route is located approximately 1 mile south of the project site and noise from operation of the Green Line is not audible at the project site.

3.4.4 Noise-Sensitive Land Uses

NSLUs are land uses that may be subject to stress or interference from excessive noise. The Santee General Plan defines NSLUs as areas containing residences, schools, hospitals, rest homes, or long-term medical or mental care facilities. Industrial and commercial land uses are generally not considered sensitive to noise. There are no NSLUs currently located on the project site. The nearest NSLUs to the project site are the single-family neighborhoods adjacent to the western, southern, and eastern boundaries of the project site and the campground and RV park at the Santee Lakes Recreation Preserve adjacent to the western boundary of the site. Other NSLUs in the project vicinity are Cajon Park, located approximately 0.6 mile east of the project site; Santana High School, located approximately 0.75 mile east of the project site; Rio Seco School, located approximately 0.3 mile south of the project site; the Santee Public Library, located approximately 0.85 mile south of the project site; Sycamore Canyon School, located approximately 250 feet (0.05 mile) east of the Fanita Parkway improvement area; and West Hills High School, located approximately 1 mile southwest of the project site.

3.4.5 Vibration-Sensitive Land Uses

Land uses in which groundborne vibration could potentially interfere with operations or equipment, such as research, manufacturing, hospitals, and university research operations, are considered vibration sensitive (FTA 2018). The degree of sensitivity depends on the specific equipment that would be affected by the groundborne vibration. Excessive levels of groundborne vibration of either a regular or an intermittent nature can result in annoyance to residential uses. The nearest vibration-sensitive land use to the project site is the Edgemoor Skilled Nursing Facility, located approximately 0.6 mile to the southeast of the project site.

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Section 4 Methods and Significance Criteria

4.1 Methods

4.1.1 Excessive Noise Levels

Impacts related to potential exposure to excessive noise levels from operation of the proposed project have been assessed based on a comparison of noise levels anticipated to be generated by the proposed project land uses (Figure 3) to the applicable City noise standard for existing off-site receptors. Estimated noise levels are based on a variety of sources, including noise technical reports for similar facilities. Noise levels at a particular receptor from a stationary noise source are based on an attenuation rate of 6 dBA for every doubling of distance. The compatibility of the proposed land uses with existing ambient noise levels is based on a comparison of the results of the ambient noise survey and existing traffic noise calculations to the Santee General Plan Land Use Compatibility Guidelines and the proposed project land uses.

The potential for implementation of the proposed project to permanently increase ambient noise levels as a result of increased traffic was assessed using standard noise modeling equations adapted from the Federal Highway Administration noise prediction model. The modeling calculations take into account the posted vehicle speed, ADT volume, and the estimated vehicle mix. The noise model assumes that roadways would experience a decrease of approximately 3 dBA for every doubling of distance from the roadway. Traffic data is provided in the project-specific traffic study prepared by Linscott, Law & Greenspan, Engineers (LLG 2020). Noise modeling for construction and operation assumes the Specific Plan design speed of 50 miles per hour for Fanita Parkway from Mast Boulevard to Ganley Street and for Cuyamaca Street from Mast Boulevard to Woodglen Vista Drive. This assumption is conservative because the posted speed limits of 40 miles per hour on Fanita Parkway and 35 miles per hour on Cuyamaca Street may be maintained by the City following project implementation.

Impacts related to temporary increases in ambient noise levels from construction of the proposed project were assessed using estimates of sound levels from typical construction equipment provided by the Federal Highway Administration in the Roadway Construction Noise Model (RCNM) (FHWA 2008), assuming an attenuation rate of 6 dBA per doubling of distance from the source. Impacts related to rock crushing and blasting activities resulting from construction were assessed using reference noise levels provided by noise analyses for similar equipment use (Shasta County 2011; FHWA 2006).

4.1.2 Groundborne Vibration

Groundborne vibration impacts were assessed based on the FTA vibration impact criteria listed in Table 5 and typical vibration source levels provided by the FTA (2018).

4.1.3 Aircraft Noise

Impacts related to aircraft noise were assessed based on a review of published noise contours and planning documents for area airports (SDCRAA 2010, 2011).

4.2 Significance Criteria

Based on Appendix G of the California Environmental Quality Act (CEQA) Guidelines and significance criteria outlined in the Santee General Plan, Santee Municipal Code, County Noise Ordinance, and FTA guidance, implementation of the proposed project would result in a significant adverse impact if it would:

• **Threshold 1:** Generate a substantial temporary or permanent increase in ambient noise levels in the vicinity of the proposed project in excess of standards established in the local General Plan or Noise Ordinance, or applicable standards of other agencies.

New operational noise sources would be significant if these sources would expose offsite persons to or generate noise levels at off-site uses in excess of standards established in the Noise Element of the Santee General Plan or the City's Noise Ordinance (Section 5.04 of the Santee Municipal Code), as applicable.

A substantial permanent increase in vehicle traffic noise would occur if implementation of the proposed project would result in an ambient noise level that exceeds the normally acceptable land use compatibility limits (Table 6) established in the Santee General Plan. If the normally acceptable standard would be exceeded without project implementation, an increase of more than 3 dBA would be considered significant. Temporary construction activity would be considered significant if it would violate the limits established in Section 5.04.090 of the Santee Municipal Code for receptors in the City and Section 36.409 of the County Municipal Code for receptors in unincorporated San Diego County. The City's Noise Ordinance prohibits operation of any construction equipment outside the hours of 7:00 a.m. through 7:00 p.m., Monday through Saturday. Also, construction equipment with a manufacturer's noise rating of 85 dBA Lmax or greater may only operate at a specific location for 10 consecutive workdays absent specific public notice. The County's Noise Ordinance prohibits the operation of construction equipment that would exceed an average sound level of 75 dB for an 8-hour period, between 7:00 a.m. and 7:00 p.m., on an occupied property where the noise is being received.

- Threshold 2: Generate excessive groundborne vibration or groundborne noise levels. Groundborne vibration is defined as in excess of the FTA criteria listed in Table 5. Additionally, an impact would occur related to architectural and structural damage to buildings if existing buildings were affected by a PPV in excess of 0.2 in/sec.
- **Threshold 3:** For a project located within the vicinity of a private airstrip or an airport land use plan or, where such a plan has not been adopted, within 2 miles of a public airport or public use airport, expose people residing or working in the project area to excessive noise levels.

The proposed project would have a significant impact if it would construct residences within the 65 CNEL noise contour of an airport, or result in a change in air traffic patterns that would result in new noise exposure.

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Section 5 Impact Analysis and Mitigation Measures

5.1 Impact Analysis

Potential project-related noise and vibration impacts from construction and operation of the proposed project are discussed below. This analysis focuses on the potential for existing off-site sensitive receptors to be exposed to noise or vibration levels in excess of applicable thresholds. CEQA is intended to protect the existing environment from impacts that would result from the proposed project. Generally, CEQA does not consider impacts of the existing environment on a proposed land use to be significant (see Section 15126.2 of the CEQA Guidelines). Likewise, sensitive receptors proposed as part of the proposed project are not part of the existing environment, and impacts to these receptors from implementation of other project components are not addressed. The exception is the analysis of consistency with the Santee General Plan provided in Section 5.1.1. The Santee General Plan Noise Element specifically states that a significant impact would occur if noise levels at any planned development site would exceed the noise levels considered compatible for that use, as identified in Table 6. Therefore, the potential for ambient noise levels to impact the proposed project is addressed in the context of demonstrating consistency with the Santee General Plan.

5.1.1 Threshold 1: Exceedance of Noise Standards

Potential project-related noise impacts from operational sources, transportation sources, and construction activities are discussed below.

5.1.1.1 Impact Analysis

The proposed project would have the potential to generate excessive noise levels as defined in Table 7, as a result of increases in traffic volumes, developing new stationary sources of noise, and by increasing human activity throughout the project site. Proposed potential noise-generating land uses on site include commercial uses, agricultural uses, and public uses, including parks. The proposed project would also have the potential to result in temporary increases in noise levels during construction.

Operational Noise Generated by the Proposed Development

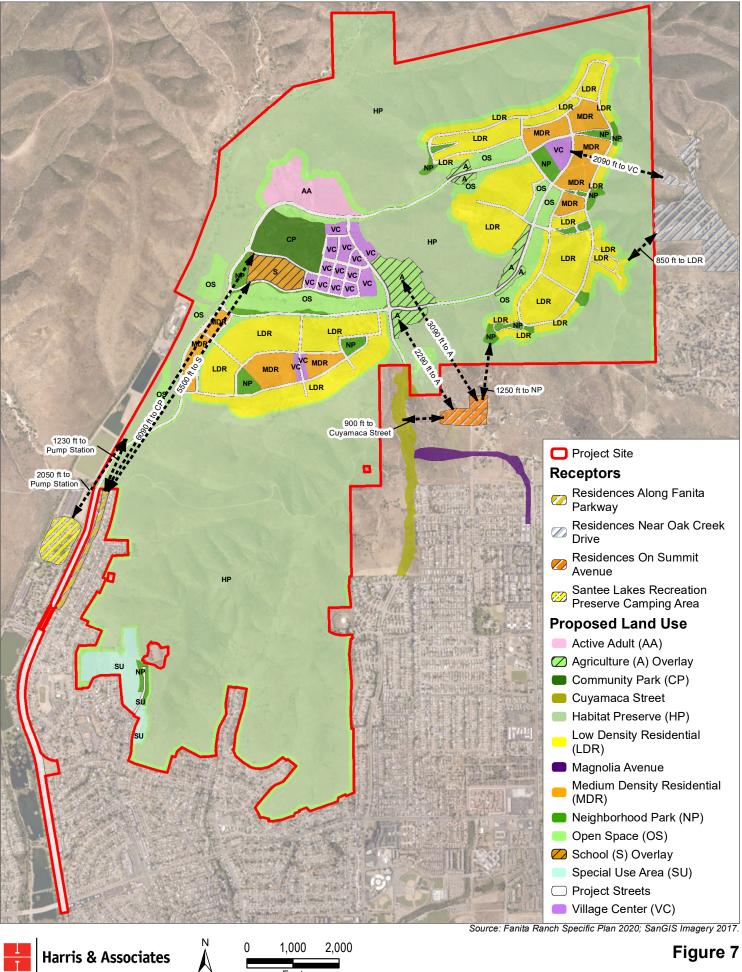
The proposed project would include a range of uses that have the potential to generate noise that may affect existing noise-sensitive receptors. These uses include commercial and retail development, residential development, agricultural operations, special events, recreational facilities, maintenance activities, a school, a fire station, special uses, and on-site infrastructure. Figure 7, Noise Receptors and Sources, summarizes the potential on-site noise sources and distance to the nearest NSLUs that are addressed below.

Commercial Development

Proposed commercial development would be located primarily in the areas designated as Village Center on the eastern side of Fanita Commons and in the middle of Vineyard and Orchard Villages. The Village Center component would comprise a total of approximately 36.5 acres across the site. The approximately 28-acre Village Center in Fanita Commons would accommodate commercial uses to serve the entire proposed development. The smaller Village Center areas in Vineyard and Orchard Villages would consist of smaller-scale mixed-use retail, service, or office spaces to serve the residents of the surrounding villages. Allowable uses would include retail stores, offices, retail nursery, restaurants, live entertainment establishments, craft breweries or other gourmet food shops, studios and galleries, pet services, business or trade schools, civic uses, health and wellness services, private recreation facilities, religious or spiritual facilities, daycare, tutoring facilities, museums or cultural facilities, and education or event facilities associated with the Farm.

The future mix of retail and office uses is currently unknown, along with the specific noise producing equipment associated with each use. The noise level generated by commercial uses on site would vary depending upon the specific types of commercial uses that would occupy available space. The exact noise level generated cannot be specifically quantified at this time because of many variables involved. These include the specific land use type, size of equipment, location and orientation of equipment, number and location of loading docks, and parking areas. Therefore, it is not possible to determine the level of noise impact of individual commercial uses at specific locations at this time. Thus, this analysis focuses on typical noise produced from commercial truck deliveries at loading docks; parking lots; and evening or nighttime noise from dining or entertainment uses at worst-case distances from NSLUs. These noise sources are addressed below.

The specifications and locations of the HVAC systems that would be installed at commercial or mixed-use buildings are unknown at this time. Therefore, for the purposes of this analysis, it is assumed that the HVAC systems of a mixed-use commercial and residential project would be typical of a community-serving retail and office building (ABC Acoustics 2018). HVAC units not installed within an enclosure would have the potential to generate a noise level of up to 79 dBA Leq at the unit (approximately 3 feet). A single HVAC unit could have the potential to generate noise that may exceed typical conversation noise levels of 65 dBA up to 15 feet from the unit. As shown on Figure 7, the nearest existing NSLUs to the proposed Village Center areas on the project site are the off-site single-family residences located off Oak Creek Drive, approximately 2,090 feet east of the Village Center planned for Vineyard Village. Due to distance and intervening structures and topography, noise from HVAC units in the proposed Village Centers would not be audible at existing, off-site receptors and impacts would be less than significant.



Feet

Noise Receptors and Sources

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In addition to HVAC systems, commercial land uses also have the potential to generate noise from truck deliveries, such as engines idling and beeping from back up warning signals at commercial loading docks. Truck trips to the proposed project site would involve deliveries of supplies and products to commercial uses. State law (13 CCR 2485) currently prohibits heavy-duty diesel delivery trucks from idling more than five minutes. Therefore, noise from idling would be limited to five minutes during truck deliveries. Noise levels measured at a typical loading dock registered 78 dBA Leq at a distance of 5 feet outside an open loading dock (ABC Acoustics 2018). A loading dock that generates a noise level of 78 dBA at 5 feet would have the potential to generate noise that may exceed typical conversational noise levels of 65 dBA up to 25 feet from the unit. Noise levels would be reduced on the project site because the Land Use and Development Regulations in Chapter 3 of the Fanita Ranch Specific Plan require loading areas to be designed and located to minimize impacts on adjoining properties, including use of sound baffling. Additionally, as previously stated, the nearest existing NSLUs to a proposed Village Center are residences approximately 2,090 feet east of the Village Center planned for Vineyard Village. Due to design guidelines, distance, and intervening structures and topography, impacts to off-site NSLUs related to truck deliveries and loading would be less than significant.

Noise sources from parking areas include car alarms, door slams, radios, and tire squeals. These sources typically range from about 51 to 66 dBA at a distance of 10 feet (Gordon Bricken & Associates 2012), and are generally short-term and intermittent. Parking lots have the potential to generate noise levels that are audible above ambient levels depending on the location of the source; however, noise sources from a parking lot would be different from each other in kind, duration, and location, so that the overall effects would be separate and in most cases would not affect noise-sensitive receptors at the same time. Similar to truck delivery noise, due to distance and intervening structures and topography, impacts to the nearest off-site NSLUs related to parking areas would be less than significant.

Noise from human activity within outdoor seating areas, restaurants, and public gathering places would be limited to normal conversation noise levels, which would generally be consistent with the City's Noise Ordinance and Santee General Plan Noise Element compatibility standards for surrounding land uses. However, the proposed project would accommodate restaurant uses and live entertainment venues that would have the potential to result in intermittent noise that could exceed Noise Ordinance standards. This may include bars or nightclubs that operate into late night hours (10:00 p.m. to 2:00 a.m.). Section 5.22.130 of the Santee Municipal Code prohibits music at dancehalls between 2:00 a.m. and 11:00 a.m. If these establishments would include outdoor areas, nighttime use could result in loud conversation or amplified music that would be annoying or disturbing to nearby residents. Section 3.2.11.10(B) of the Fanita Ranch Specific Plan establishes performance standards for the sale of alcohol within the proposed project site. These standards require that all alcoholic beverages sales, offerings, and consumption be conducted completely within an enclosed building on premises, except for permitted outdoor seating areas. Nighttime

uses would mostly be located within enclosed buildings, although permitted patios may result in crowds or amplified sound that would exceed normal conversation levels. As shown on Figure 7, the nearest existing off-site NSLUs to a proposed Village Center are residences approximately 2,090 feet away in the unincorporated County. Reference noise levels for loud conversation and amplified music are available for indoor noisy restaurants (85 dBA) and school dances (100 dBA) (Center for Hearing and Communication 2020). Based on these reference noise levels, noise levels from loud conversation and amplified music in the proposed Village Center would be reduced to approximately 28 dBA and 43 dBA, respectively, at 2,090 feet away at the nearest off-site NSLUs. These noise levels would not exceed normal conversation levels at City receptors and would not exceed the County's nighttime hourly average sound level limit of 45 dBA at residences along Oak Creek Drive. Impacts would be less than significant.

Residential Development

A variety of residential densities would be accommodated in all three development villages. Noise generated from residential uses is generally described as nuisance noise. Nuisance noise is defined as intermittent or temporary neighborhood noise from sources such as amplified music, barking dogs, and landscape maintenance equipment that may be disturbing to receptors. Nuisance noise impacts are more likely to occur in higher density areas (such as Village Center and Medium Density Residential areas). Section 5.04.040 of the City's Noise Ordinance prohibits nuisance noise. Specific sources of nuisance noise covered by the City's Noise Ordinance include, but are not limited to, devices for producing or reproducing sound, drums and other musical instruments, yelling, and animals. Compliance with the City's Noise Ordinance would limit exposure to excessive nuisance noise. The County Sheriff's Department enforces the nuisance noise provisions of the City's Noise Ordinance, in accordance with Section 5.04.180 of the City's Noise Ordinance, Enforcement. Nuisance noises would also be different from each other in kind, duration, and location, so that the overall effects would be separate and in most cases would not affect the receptors at the same time. Nuisance noise would be a less than significant impact.

Residences may include HVAC units. As described previously for commercial uses, a single HVAC unit would generally not exceed typical conversation noise levels of 65 dBA beyond 15 feet from the unit. The nearest existing off-site receptors to a proposed residential area are the existing residences along Crazy Horse Drive in the County, approximately 700 feet east of Vineyard Village. Therefore, due to distance and the interment nature of noise sources, HVAC noise from proposed residential neighborhoods would not result in significant impact to existing receptors.

Agricultural Operations

The Farm is a central feature of the proposed land use plan. The working farm is planned to include terraced vegetable fields, pasture lands, limited housing for employees, raised gardens, and small-scale animal husbandry. Regular agricultural-related events would be hosted at the Farm, including

commercial and educational events. Other special events at the proposed event barn on the Farm are addressed below. The 27.3-acre Farm would be located along the eastern border of Fanita Commons near the center of the proposed development. Additional agricultural areas are designated at the entrances to Vineyard Village on either side of Street "V" and Street "W." Community gardens and community-supported agriculture are allowable land uses in all proposed development areas except the Special Use area. Orchards, vineyards, and crops are allowed in the Open Space designation.

Based on the noise survey conducted on March 5, 2019, and discussion with the farm operations manager (Farmer D Consulting, pers. comm. 2018), the primary sources of noise associated with agricultural use would be use of one or two tractors in agricultural fields and approximately two utility task vehicles (UTVs) across the Farm site. Fans, pumps, and generators may also be required. The proposed community-scale Farm would not require the use of industrial farm equipment for harvesting or processing. As observed at the Coastal Roots Farm in Encinitas, hand tools would generally be used on the Farm and would not generate noise. Equipment used in agricultural spaces outside the Farm, such as community gardens, would be limited to hand tools.

Regular events at the Farm would include farmers markets and farm-based education in the form of tours, volunteer opportunities, camps, workshops related to gardening and farmer training, nutrition, cooking, herbal medicines, home preservation of food, and more. Farmers market and educational activity hours would be limited of 7:00 a.m. and 7:00 p.m. on weekdays and 7:00 a.m. and 10:00 p.m. on weekends and are anticipated to be similar to nearby commercial uses in the Village Center. With the exception of farm equipment, noise associated with orchards and vineyards, regular events, and limited employee housing would be generally limited to normal conversation and occasional nuisance noise, similar to noise anticipated from surrounding proposed residential development, described above.

The design plan for the Farm includes a condition of operation that the use of mechanical equipment such as tractors, exhaust fans, circulating pumps, or generators, and other exterior noise-generating operations that result in a 1-hour average sound level of 50 dB or more, as measured at the nearest adjacent on-site residential property line, shall be limited to the hours of 7:00 a.m. and 7:00 p.m. every day (Farmer D Consulting 2020). Noise barriers shall be installed around any stationary noise-generating equipment if necessary to meet the required limitations. A tunnel would be constructed under Street "W" to connect the two sections of the Agricultural Overlay to allow for the movement of agriculture equipment to less than nuisance levels on the project site, noise levels would be less than significant at off-site existing sensitive receptors.

The use of UTVs and tractors are anticipated to generate the highest equipment noise levels from farm operation. The average noise level for UTVs for farm use is 86 dBA and the average noise

level for a tractor is 92 dBA (Depczynski et al. 2005). Noise level is reported at the driver's seat. Noise levels from UTVs would be reduced to below normal conversation levels of 65 dBA approximately 35 feet from the source, and tractors approximately 70 feet from the equipment. Additionally, when UTVs are in use, they would be in motion across the Farm and individual receptors would only be exposed to UTV noise briefly during any given pass-by. Due to the modest size of the orchards and vineyards, duration of tractor use would be limited to a portion of a day, when needed. Therefore, use of farm equipment would not result in a significant impact.

The Farm would primarily be cultivated with crops but may include limited livestock, such as poultry, sheep, goats, or aquaponics (fish). Livestock would not exceed five animals per acre. Livestock noise would include intermittent animal noises that may occasionally be a source of nuisance noise. Intermittent poultry noise was observed during the March 5, 2019, noise survey at Coastal Roots Farm in Encinitas. Poultry activity consisted of several chickens roaming the property and was similar to the level anticipated for the proposed Farm. Noise levels with poultry noise did not exceed 54 dBA. However, poultry at the Farm may also include roosters. Rooster crowing can produce sound levels up to 100 dBA at 1 meter (3.3 feet) (Claes et al. 2018). The nearest existing receptors to the Farm are along Summit Avenue, approximately 2,290 feet from the Farm (see Figure 7). At this distance, noise from rooster crowing would be reduced to 43 dBA and would not exceed typical ambient noise levels. Due to the limited number of animals allowed, and because animals would be spread out across the pasture area throughout the day, intermittent animal noise would not be anticipated to exceed average ambient community noise levels. Regular Farm operations are not anticipated to be audible off site. A significant impact would not occur from Farm operation.

Special Events

The Farm is planned to include a large iconic barn that would set the architectural theme of the community and provide a venue for special events and Farm operations. The Farm would allow for a range of special events including farm-to-table events, community harvests, weddings, and other celebrations and festivals, such as pumpkin patches. Special events would potentially involve the use of amplified noise or crowds that would result in noise levels above typical conversation levels. As a condition of operation, events would be permitted between the hours of 7:00 a.m. and 7:00 p.m. on weekdays and 7:00 a.m. and 10:00 p.m. on weekends. Therefore, weekday events would not result in nighttime noise impacts, and weekend events would not extend into late night hours. The event barn and associated outdoor event areas would be located directly east of the Village Center, approximately 3,090 feet from the nearest existing residences, located along Summit Avenue (see Figure 7). Activity hours for events would be similar to the commercial uses in the Village Center.

Special and temporary event attendance would be limited to a maximum of 300 attendees. The reference noise level for the events anticipated to occur at the Farm is taken from a noise analysis conducted for the Point View Master Plan Project in the City of Rancho Palos Verdes, which included a similar venue for hosting public and private events. The event area was an existing

outdoor ceremony area with the capacity for 300 guests, including weddings, corporate parties, conferences, and charity events (City of Rancho Palos Verdes 2012). Therefore, the analysis for the similar event venue is considered representative of weddings or other special events proposed at the Farm. To determine the impact of the event venue on the community, the representative noise analysis for the Point View Master Plan Project recreated a maximum capacity event at the venue and recorded noise levels. The study determined that crowd noise from 300 guests could generate noise levels of up to 101 dBA at approximately 10 feet from the source. Crowd noise would be intermittent, such as at the end of speeches during a ceremony. The Initial Study/Mitigated Negative Declaration for the Point View Master Use Plan Project determined that crowd noise would generally not exceed 15 minutes in a 60-minute period (City of Rancho Palos Verdes 2013).

Based on the results of the analysis for the similar event venue, and conservatively assuming the existing measured ambient noise level is approximately 41 dBA in the Farm area, events attended by 300 guests would have the potential to result in a 1-hour average noise level of 95 dBA at 10 feet from the source. Event noise would have the potential to exceed the average conversation noise level of 65 dBA up to 315 feet from the event. As shown on Figure 7, the nearest existing NSLUs to the event area are the residences along Summit Avenue, approximately 3,090 feet south of the event area. Therefore, event noise would not exceed the noise level limits at off-site NSLUs. This impact would be less than significant.

Recreational Facilities

The proposed project would provide a variety of recreational opportunities, including the Community Park, Neighborhood Parks, Mini-Parks, and trails throughout the project site. According to the Santee Municipal Code, Section 8.08.150, parks are permitted to operate dawn to dusk or such alternative hours as designated by the Director of the Community Services Department. Therefore, it is assumed that all proposed recreational facilities would have similar operating hours of dawn to dusk, with the exception of trails. Trails would be available at all hours for transportation and access in the development area; however, nighttime use of open space primitive trails would be limited because lighting is not proposed. Recreational facilities are addressed by type below.

Community Park

Visitors to the Community Park in the center of Fanita Commons would participate in active and passive recreational activities. The Community Park would include two multipurpose ballfields, sport courts, restrooms, parking, playground, open play areas, and passive picnicking areas, and may include an aquatic element, community gathering plaza, and a dog park. Within the Community Park, a community center would provide multipurpose, flexible spaces to support recreation, learning, arts and crafts, social and service functions. The community center would also provide support spaces such as staff offices, reception area, restroom, and storage areas. The park is designed so that passive uses would occupy the eastern portion of the Community Park, adjacent

to the Village Center. The northern edge of the park would be bordered by a designated Open Space riparian area. Active uses would be concentrated in the southwestern portion of the park, including lighted sports fields adjacent to the proposed school.

Recreational activity participants are expected to generate a range of noise levels typical of recreational activities. Active uses such a playgrounds and sports fields typically generate incidental recreational noise such as cheering for sports activities or children at play. Passive recreational activities such as walking, reading, and dining in open turf and picnic areas typically generate lower noise levels as compared to active sports play.

Noise levels typically generated by multipurpose fields, one of the most active proposed uses, are assumed to be representative of worst-case noise levels from daily use of the Community Park. The noise impact analysis for the City of Lake Forest Sports Park and Recreation Center, which proposed a similar mix of active and passive uses, including multiple sports fields and play areas, determined that noise levels from simultaneous use of the sports fields would generate noise levels of 47 dBA at approximately 400 feet from the fields, or 59 dBA at 100 feet (City of Lake Forest 2010). Similarly, the noise analysis for a new 4-acre sports field complex in San José determined that average noise levels resulting from active use of the fields would be approximately 60 dBA at a distance of 100 feet from the center of the field, with maximum noise levels from shouting as high as 67 dBA (Illingworth & Rodkin 2016). The active Community Park uses would be located at the far west edge of development in Fanita Ranch, and active uses would be located more than 6,000 feet from existing residences on Strathmore Drive, which are the nearest existing receptors (see Figure 7). Due to distance, activity at the park would be reduced to below an audible level at the nearest existing receptors. Impacts would be less than significant.

Electronic amplification equipment would not be permanently installed at any of the parks, but temporary systems may be used in conjunction with permitted active sports leagues or events. Public events may also occur that require temporary permitted amplified noise. Activities that require permitted amplified noise would be limited to normal park operation hours in compliance with the Santee Municipal Code, Section 8.08.150. Additionally, amplified noise would not be a constant source of noise. Activities would occur on various dates and times and at varied locations and would typically not occur after dusk, in conformance with the Santee Municipal Code. Therefore, use of amplified noise from permitted uses would not result in a significant impact.

Future uses at the community center are unknown; however, activities would be enclosed within the center and would not be anticipated to generate excessive noise outside the facility. It can be reasonably assumed that the community center would require an HVAC unit. As described under the discussion of commercial development, HVAC equipment would have the potential to generate noise that may exceed conversational noise levels up to 15 feet from the unit. Due to distance, operation of the HVAC system at the community center would not be audible at the nearest offsite NSLUs located along Fanita Parkway, more than 6,000 feet from the proposed Community Park (see Figure 7). Additionally, the Community Park would be separated from off-site receptors by on-site development that would provide a noise barrier to further attenuate noise levels. This impact would be less than significant.

Neighborhood Parks

Eight Neighborhood Parks are proposed throughout all three villages, as shown on Figure 3. Specifically, Neighborhood Parks 1 and 2 would be located between Medium Density Residential and Low Density Residential development in Orchard Village. Neighborhood Park 3 would be located adjacent to the riparian open space feature between Fanita Commons and Orchard Village. Neighborhood Park 4 would be located along the western edge of Vineyard Village. Parks 5 and 6 would be located on either side of the Village Center in Vineyard Village. Neighborhood Park 7 would be located at the southern edge of Vineyard Village, and 8 would be located adjacent to the School Overlay in Fanita Commons. Neighborhood Parks may be active-recreation oriented, or non-sports use oriented with more passive uses. Sports-oriented Neighborhood Parks would include amenities similar to the Community Park, but at a smaller scale, including open play fields, playgrounds, sport courts, gardens, picnic facilities, and restrooms. Neighborhood Park 5 adjacent to the Village Center in Vineyard Village would be a sports-oriented park, while Neighborhood Park 3 adjacent to the riparian area along Street "A" in Orchard Village would be a passive Linear Park. It is unknown which of the remaining Neighborhood Parks would be sports-oriented. Passive Neighborhood Parks would not be expected to generate noise other than general conversational levels and would not be expected to be audible outside of the park. However, noise levels for use of sports-oriented Neighborhood Parks are conservatively assumed to be 47 dBA at approximately 400 feet, as estimated for the Community Park described previously. The nearest off-site receptors to a Neighborhood Park are the residences located at the northern terminus of Summit Avenue, approximately 1,250 feet south of the proposed Neighborhood Park at the southwestern boundary of Vineyard Village. Due to distance, noise from the use of the Neighborhood Parks would not be audible off site. Noise impacts from Neighborhood Parks would be less than significant.

Other Recreational Facilities

Additional parks and trails would be located throughout the site, including Mini-Parks and trails such as the AgMeander circuit. The proposed trails would be used for walking and bicycling. Mini-Parks, with the exception of the Village Green discussed below, would include passive recreation features, such as seating, trail connections, and interpretive stations. These amenities would generally not support activities that generate noise levels higher than normal conservation. Therefore, these facilities would not generate noise levels that would result in excessive noise levels. Impacts from the trails and Mini-Parks would be less than significant.

Village Green

The Village Green would be a special Mini-Park located directly west of the Farm in Fanita Commons that would provide a public gathering and event space. The park would provide a large open turf area, with possible shade trellises and seating along the perimeter. When not in use for community events, the Village Green would provide passive use space for Fanita Commons residents and would not generate excessive noise levels, similar to the other Mini-Parks in the proposed project. However, the turf area would also serve as a multipurpose space to accommodate events such as performances, art fairs, outdoor movies and other social functions. In addition, it would potentially provide a focal point for larger community festivals and concerts, with connections to the Farm and farmers markets east of Cuyamaca Street, the mixed-use Village Center, and Community Park.

Similar to events at the Farm, regular ongoing events such as community gatherings, farmers markets, and art shows would generally not result in noise levels higher than normal conservation and would be similar to ongoing activity in the Village Center. It is not anticipated that the Village Green would be able to accommodate events with a larger capacity that events at the Farm event area. As discussed previously, special events at the Farm with up to 300 guests, such as weddings, would not result in noise levels that would exceed the City's Noise Ordinance limit of normal conversation levels (65 dBA) during the evening at any off-site NSLUs. Development in the Village Center would also provide a noise buffer between events in the Village Green and development outside the Village Center. As such, because events in the Village Green would be smaller and located farther from off-site receptors than the Farm, events would not be expected to exceed noise level limits at existing off-site NSLUs. This impact would be less than significant.

Trash Collection

Commercial and residential trash hauling would be provided by Waste Management, Inc., under a contractual franchise agreement with the City. Single-family residences would have individual trash and recycling bins subject to weekly pickup. Commercial and multi-family residences would be expected to have on-site garbage and recycling dumpsters that may require multiple pickups per week. As trash service would be provided by Waste Management, Inc., noise associated with operation of refuse collection vehicles is beyond the control of the proposed project. However, Waste Management, Inc., currently operates in Santee and is subject to Section 5.04.130 of the City's Noise Ordinance, Loading and Unloading Operations, which prohibits waste collection vehicles from operating between the hours of 10:00 p.m. and 7:00 a.m. in such a manner as to cause a noise disturbance within or adjacent to a residential district. Additionally, individual pickup events would be short in duration and occur at most a few times per week in the vicinity of an individual receptor. Due to its intermittent nature, short duration, and compliance with the City's Noise Ordinance limitations, waste collection in the proposed project would not generate excessive noise levels at the nearest off-site NSLUs. This impact would be less than significant.

Landscape Equipment

Scheduled maintenance would occur on a regular basis across the proposed project, including maintenance of proposed recreational facilities, decorative landscaping, and private residences. Maintenance activities would potentially include the use of gasoline-powered mowers, trimmers, blowers, and edgers resulting in intermittent short-term temporary noise increases. Maintenance equipment would not be operating at any one location for more than a few minutes, and all equipment would not be operating simultaneously. Due to the limited amount of time equipment would be operating in one location, and distance to off-site receptors, operation of landscape equipment would generally not exceed average community ambient noise levels at a particular existing receptor. Therefore, landscape maintenance would result in a less than significant impact.

School

A school site land use overlay is proposed for the western portion of Fanita Commons, south of the proposed Community Park. If acquired by the Santee School District, the site could accommodate up to 700 students. A school would potentially generate amplified noise such as bells and loudspeaker announcements. Bells or other announcements would typically be brief and intermittent throughout the school day. Speaker volume would be audible above typical activity on the campus but not to a level that would be a nuisance or uncomfortable to staff and students on-site in the immediate vicinity of the speakers. As such, the use of the school announcement and bell system would not generate noise levels that would violate the City's Noise Ordinance by exceeding conversational noise levels at the nearest off-site NSLUs.

If developed, a school would also likely include recreational facilities such as playgrounds and play fields. The level of activity during recess and afterschool activities is assumed to be similar to active use of the sports fields at the Community Park, and no amplified speakers would be installed. Therefore, the proposed school would have the potential to generate noise levels up to 47 dBA at approximately 400 feet. Similar to the Community Park, the school site would be located at the western edge of development in the proposed project, approximately 5,500 feet north of the nearest sensitive receptors, located along Strathmore Drive (see Figure 7). Additionally, the school would be separated from off-site receptors by on-site development that would provide a noise barrier to further attenuate noise levels. Due to distance, activity at the school would not be audible off site at the nearest existing NSLUs. This impact would be less than significant.

Fire Station

A new fire station is proposed in the Village Center in Fanita Commons, although the precise location is currently unknown. Routine operations such as vehicle maintenance and periodic training activities would occur during daytime hours and would not be expected to generate noise levels above ambient noise levels in the active Village Center. Potential nuisance noise impacts of the fire station would primarily be limited to on-site emergency address systems and sirens from vehicles leaving the station, although not all emergency calls would require a siren, depending on traffic conditions. Similar to the school alarm or announcement system, the fire station address

system would be set at a volume loud enough to be clear and noticeable to fire station personnel, but not so loud to be harmful or an unnecessary nuisance to neighboring land uses. Additionally, the fire station would be located more than 0.5 mile from any off-site noise-sensitive uses and would not be expected to be audible off-site. Emergency vehicle sirens typically generate a noise level of 124 dBA at 10 feet (Daly 2017). As such, individual emergency sirens would be a potential noise nuisance, if required for a particular emergency, but would be short-term and intermittent in nature. Sirens would be less likely to be required at night, when receptors would be more sensitive to siren noise, due to lighter traffic conditions. However, off-site receptors are currently served by emergency services and occasional emergency sirens are an existing part of the ambient noise environment in the City. The occasional response of emergency service vehicles originating from the project site would be similar to existing conditions throughout the City and would not be a significant impact.

Off-Site Improvements

The infrastructure improvements associated with the proposed project include roadway improvements that would not generate operational noise themselves. However, these improvements would accommodate higher traffic volumes associated with the proposed project. The potential noise impacts associated with changes in traffic volume and roadway configuration are addressed under Permanent Increase in Traffic Noise Levels. Additionally, construction of these improvements is addressed under Temporary Noise Increase.

Special Use Area

The Special Use area is adjacent to an existing residential area on Carlton Hills Boulevard, Swanton Drive, Las Lomas Drive, and Settle Road. The specific use of the Special Use area in the southern area of the project site would be limited to primarily passive uses such as a solar farm, RV and boat storage, aboveground agriculture without irrigation, or other similar uses not exceeding a height of 35 feet. As such, utilization of this area would not be anticipated to generate noise levels at surrounding land uses in excess of average conversation noise levels. Any use of the site would likely include an automatic gate system for access. Newer model gates may generate minimal noise, 56 dBA or below, that would generally not be noticeable to surrounding existing residences (Consumer Mentor 2019). However, because gate specifications are currently unknown and existing receptors are located within 50 feet of the boundary of the Special Use area, this impact is considered potentially significant.

Likely uses for the Special Use area include vehicle or boat storage or a solar facility. RV storage would generate intermittent noise from vehicle loading and unloading. Similar to a parking lot, noise sources would be different from each other in kind, duration, and location. It is unlikely that existing residences in the neighborhood surrounding the Special Use area would be exposed to regular noise in excess of normal conversational levels. A noise analysis for a proposed RV facility in the City of Wildomar included noise monitoring at existing storage facilities. Measured noise sources from vehicle loading and unloading included RV idling, air brake operation, and vehicle movements. The reference measurement results showed a noise level of 62.4 dBA Leq at 50 feet, which is below

normal conversation levels (Urban Crossroads 2017). However, due to the close proximity of offsite NSLUs (within 50 feet of the project site boundary), activities at the Special Use area would be considered a potential nuisance if access would occur during nighttime hours in close proximity to sensitive receptors. Noise levels would have the potential to exceed 65 dBA within approximately 40 feet of pickup and drop-off activities. Assuming a 10 dBA penalty to account for nighttime sensitivity to noise, consistent with Ldn methods, pickup and drop-off noise would have the potential to exceed 55 dBA up to 125 feet from the source. This impact would be potentially significant.

Solar panels are passive; however, the associated inverters or transformers typically generate some noise. The noise is typically described as buzzing or humming white noise. The exact specifications of solar panels, if installed, at the Special Use area are unknown at this time. However, a similar project that proposed solar panels on an over 300-acre site in the County determined that noise levels from inverters and transformers would generate noise levels of up to 60 dBA at 5 feet (County of San Diego 2016). As such, operation of a solar facility on a smaller (approximately 32-acre) site would not be expected to generate noise levels that exceed 65 dBA at existing residences located adjacent to the Special Use area. A more conservative estimate of 70 dBA at 3 feet for transformer noise has also been reported (Nagel pers comm. 2019); however, noise levels would still be expected to attenuate to below 65 dBA less than 6 feet from the transformer. The limited impact of solar panels is further evidenced by the County's requirements for solar panels in residential zones; only a 3-foot setback from the property line is required for solar panels (County of San Diego 2014). This impact would be less than significant.

As noted, uses in the Special Use area are anticipated to be passive, and daytime impacts from the Special Use area would be less than significant. However, potential nuisance noise from nighttime access at the Special Use area is considered a potentially significant impact.

On-Site Water Infrastructure

Development of the proposed project would involve construction of water infrastructure improvements, including pipelines, storage tanks, and pump stations. Following construction, proposed underground pipelines and aboveground storage tanks would be passive and would not generate operational noise. However, two pump stations are proposed to provide potable water to the project site. One pump station would be located along Fanita Parkway, adjacent to the Santee Lakes Recreation Preserve. The second pump station would be located at the eastern edge of Fanita Commons at Street "W." The size and specifications of the pump stations are currently unknown. A review of a variety of pump stations proposed by PDMWD and other local jurisdictions indicate that typical pump station equipment generates a noise level of approximately 90 dBA at 3 feet. The proposed pump stations would be installed in a masonry enclosure to provide noise shielding to surrounding land uses. A typical equipment enclosure can provide 40 dBA or more of noise reduction (HUD 2009). As such, noise levels at each pump station would be approximately 50 dBA. The nearest pump station to existing NSLUs would be approximately 1,230 feet north of

residences on Strathmore Drive and approximately 2,050 feet north of the Santee Lakes Recreation Preserve camping area. Even without shielding, at this distance, noise levels would be reduced to 40 dBA or below, and impacts would be less than significant.

Open Space Preserve Area

The proposed project would retain 256 acres of Open Space and approximately 1,650.4 acres of Habitat Preserve, primarily along the perimeter of the project site, separating the proposed development area from off-site uses. These areas would be primarily passive, but would include existing and new trails for pedestrians and bicycles. Noise from these activities would be limited to normal conversation levels. Occasional maintenance activities would be required along the trails at the edge of development, such as vegetation and sediment removal; however, these activities would not require heavy construction equipment that would generate excessive noise. Occasional maintenance vehicle trips would not result in a substantial increase in noise levels. Therefore, impacts would be less than significant.

Permanent Increase in Traffic Noise Levels

The following analysis is based on traffic data provided in the project-specific traffic study prepared by LLG (2020). The potential for the proposed project to permanently increase traffic noise is addressed under the following traffic impact analysis scenarios: Existing + Project Buildout, Near-Term + Project Buildout, and Year 2035 + Project Buildout. The Near-Term scenario assumes development of the proposed project and cumulative development projects. Traffic levels for each roadway are provided in Appendix B.

A substantial permanent increase would occur if implementation of the proposed project were to result in an ambient noise level at 50 feet from the roadway centerline that exceeds the land use compatibility limits (Table 6) established in the Santee General Plan, including 65 dBA Ldn at the property line for residential properties and schools and 70 dBA Ldn for commercial uses and Neighborhood Parks. For conditions where the roadway exceeds the standard without project implementation, a significant impact would occur if the proposed project would result in an increase of 3 dBA or greater at 50 feet from the roadway centerline. The following presents a conservative analysis since actual noise levels at nearby receptors would decrease based on their distance from the roadway and would vary based on each individual receptor's location.

Existing + Project Scenario

Existing noise levels and future increases in traffic with implementation of the proposed project are provided in Table 9. As shown in this table, 12 of the 24 existing roadway segments currently generate noise levels at 50 feet from the roadway centerline that exceed applicable thresholds. A significant project-related traffic noise impact would occur on one of these already impacted segments, Magnolia Avenue from Woodglen Vista to El Nopal, because there would be an increase

in noise level of 3 dBA Ldn. An additional five roadway segments would be significantly impacted because the project-related traffic noise would cause the existing noise level to exceed the applicable threshold. Therefore, a total of six segments would be significantly impacted.

Table 9 also identifies three segments that exceed applicable thresholds but are not identified as significant. The segment of Cuyamaca Street from the project site to Magnolia Avenue currently does not exist. It would be constructed as part of the proposed project, and noise levels with project operation at 50 feet from the roadway would exceed the applicable threshold of 65 dBA Ldn with implementation of project. However, actual noise levels at the nearest receptors to the impacted segments of Cuyamaca Street would be reduced by distance compared to the estimated noise level in Table 9. The nearest residences, located on Summit Avenue, are located more than 900 feet east of the centerline of Cuyamaca Street. At this distance, noise levels would be reduced to less than 65 dBA Ldn and a significant impact would not occur to this segment. Noise levels on Cuyamaca Street from Chaparral Drive to El Nopal would exceed 65 dBA with operation of the proposed project. However, the existing residential subdivision on Cuyamaca Street north of El Nopal was constructed with masonry and glass barriers along the edge of development on Cuyamaca Street that would likely reduce noise levels compared to the estimated noise level in Table 9. At a minimum, noise barriers that break the line of sight to the source, such as the existing barriers, typically provide at least 5 dBA noise reduction (Caltrans 2013a). Therefore, the existing noise barriers at residences along Cuyamaca Street would reduce the estimated roadway noise level of 68 dBA Ldn on Cuyamaca Street from Chaparral Drive to Woodglen Vista Drive to the acceptable noise level of 63 dBA Ldn and the estimated roadway noise level of 69 dBA Ldn from Woodglen Vista Drive to El Nopal to the acceptable noise level of 64 dBA Ldn. Impacts to these segments would be less than significant.

In summary, as shown in Table 9, with the addition of project-related traffic, six roadway segments would result in a potentially significant noise impact under the Existing + Project scenario.

Roadway	Segment	Applicable Threshold (dBA Ldn)	Existing (dBA Ldn)	Exceeds Threshold Without Project?	Existing + Project (dBA Ldn)	Increase in Noise Level from Existing	Significant Impact?
Mart Dalla and	SR-52 to West Hills Parkway	70	71	Yes	72	+1	No
Mast Boulevard	West Hills Parkway to Medina Drive	65	70	Yes	71	+1	No
	Pebble Beach Drive to Fanita Parkway	65	70	Yes	71	+1	No
Mission Cores Dood	SR-125 to Fanita Drive	70	77	Yes	78	+1	No
Mission Gorge Road	Fanita Drive to Carlton Hills Boulevard	70	77	Yes	77	0	No
	On-Site Portion to Ganley Road	65	Does Not Exist	No	66	NA	Yes
	Ganley Road to Lake Canyon Road	65	59	No	69	+10	Yes
Fanita Parkway	Lake Canyon Road to Mast Boulevard	65	61	No	70	+9	Yes
	Mast Boulevard to Carlton Oaks Drive	65	58	No	61	+3	No
Carlton Hills Boulevard	Carlton Oaks Drive to Mission Gorge Road	65	69	Yes	70	+1	No
	On-Site Portion to Magnolia Avenue	65	Does Not Exist	No	67	NA	No ¹
	Magnolia Avenue to Princess Joann Road	65	Does Not Exist	No	64	NA	No
	Princess Joann Road to Chaparral Drive	65	Does Not Exist	No	64	NA	No
	Chaparral Drive to Woodglen Vista Drive	65	54	No	68	+14	No ²
Cuyamaca Street	Woodglen Vista Drive to El Nopal	65	62	No	69	+7	No ²
	El Nopal to Mast Boulevard	65	65	No	71	+6	Yes
	Mast Boulevard to River Park Drive	65	68	Yes	70	+2	No
	River Park Drive to Town Center Parkway	65	70	Yes	71	+1	No
	Town Center Parkway to Mission Gorge Road	70	72	Yes	73	+1	No

Table 9. Existing + Project Traffic Noise Levels

Roadway	Segment	Applicable Threshold (dBA Ldn)	Existing (dBA Ldn)	Exceeds Threshold Without Project?	Existing + Project (dBA Ldn)	Increase in Noise Level from Existing	Significant Impact?
	Cuyamaca Street to Princess Joann Road	65	Does Not Exist	No	63	NA	No
Magnolia Avenue	Princess Joann Road to Woodglen Vista Drive	65	60	No	66	+6	Yes
	Woodglen Vista Drive to El Nopal	65	66	Yes	69	+3	Yes
	El Nopal to Mast Boulevard	65	68	Yes	69	+1	No
SR-52	Santo Road to Mast Boulevard	70	76	Yes	76	0	No

Table 9. Existing + Project Traffic Noise Levels

Notes: dBA = A-weighted decibel; Ldn = day-night average sound level; NA = not applicable; SR- = State Route

Unless otherwise noted, a substantial permanent increase in vehicle traffic noise would occur if implementation of the proposed project would result in an ambient noise level that exceeds the applicable threshold established in the Santee General Plan. If the normally acceptable standard would be exceeded without project implementation, an increase of more than 3 dBA would be considered significant.

The existing condition represents conditions in 2018. Noise levels are calculated at 50 feet from roadway centerline, except SR-52 (100 feet from centerline due to roadway width). Noise levels are based on traffic data provided by LLG (2020). Traffic levels for each roadway are included in Appendix B. Decibel levels are rounded to the nearest whole number. Significant impacts shown in **bold** and **shading**. See Appendix B for data sheets.

¹ The nearest residences, located on Summit Avenue, are more than 900 feet east of the centerline of Cuyamaca Street. At this distance, noise levels would be reduced to less than 65 dBA Ldn.

² Existing noise wall would reduce noise to an acceptable level.

Near-Term Scenario

The Near-Term scenario includes development of the proposed project and cumulative projects (LLG 2020). Near-term traffic noise levels, with and without the proposed project, are provided in Table 10. As shown in this table, 12 of the 24 study area roadway segments would exceed applicable thresholds without implementation of the proposed project.

Significant impacts are identified in Table 10 for project-related traffic noise increases that would cause noise along five roadway segments on Fanita Parkway, Magnolia Avenue, and Cuyamaca Street to exceed the applicable threshold. A significant impact is also identified for project-related traffic noise that would result in an increase in noise levels of 3 dBA Ldn along one roadway segment of Cuyamaca Street (Woodglen Vista Drive to El Nopal) that would exceed the applicable threshold without project implementation.

Table 10 also identifies three segments that exceed applicable thresholds but are not identified as significant. Cuyamaca Street from the project site to Magnolia Avenue currently does not exist and would exceed the applicable threshold of 65 dBA Ldn at 50 feet with implementation of project. However, due to distance, the actual noise levels at the nearest receptors to the proposed Cuyamaca Street alignment would be reduced compared to the noise level shown in Table 10. The nearest residences, located along Summit Avenue, would be more than 900 feet east of the proposed centerline of Cuyamaca Street. At this distance, noise levels would be reduced to less than 65 dBA Ldn, and a significant impact would not occur. As previously described, the existing barriers constructed at the subdivision on Cuyamaca Street north of El Nopal would reduce the estimated roadway noise level of 63 dBA Ldn, and the estimated roadway noise level of 69 dBA Ldn from Woodglen Vista Drive to El Nopal would be reduced to the acceptable noise level of 64 dBA Ldn. Therefore, impacts to these segments would be less than significant.

In summary, six roadway segments would result in a potentially significant noise impact under the Near-Term scenario.

Roadway	Segment	Applicable Threshold (dBA Ldn)	Near-Term No Project (dBA Ldn)	Exceeds Threshold Without Project?	Near-Term + Project (dBA Ldn)	Increase in Noise Level from Near- Term No Project	Significant Impact?
	SR-52 to West Hills Parkway	70	72	Yes	73	+1	No
Mast Boulevard	West Hills Parkway to Medina Drive	65	70	Yes	72	+2	No
	Pebble Beach Drive to Fanita Parkway	65	70	Yes	72	+2	No
	SR-125 to Fanita Drive	70	77	Yes	78	+1	No
Mission Gorge Road	Fanita Drive to Carlton Hills Boulevard	70	77	Yes	78	+1	No
	On-Site Portion to Ganley Road	65	Does Not Exist	No	66	NA	Yes
Fasita Dadavav	Ganley Road to Lake Canyon Road	65	60	No	70	+10	Yes
Fanita Parkway	Lake Canyon Road to Mast Boulevard	65	61	No	70	+9	Yes
	Mast Boulevard to Carlton Oaks Drive	65	59	No	62	+3	No
Carlton Hills Boulevard	Carlton Oaks Drive to Mission Gorge Road	65	69	Yes	70	+1	No

Table 10. Near-Term Traffic Noise Levels

Roadway	Segment	Applicable Threshold (dBA Ldn)	Near-Term No Project (dBA Ldn)	Exceeds Threshold Without Project?	Near-Term + Project (dBA Ldn)	Increase in Noise Level from Near- Term No Project	Significant Impact?
	On-Site Portion to Magnolia Avenue	65	Does Not Exist	No	67	NA	No ¹
	Magnolia Avenue to Princess Joann Road	65	Does Not Exist	No	64	NA	No
	Princess Joann Road to Chaparral Drive	65	Does Not Exist	No	64	NA	No
	Chaparral Drive to Woodglen Vista Drive	65	54	No	68	+14	No ²
Cuyamaca Street	Woodglen Vista Drive to El Nopal	65	62	No	69	+7	No ²
	El Nopal to Mast Boulevard	65	65	No	71	+6	Yes
	Mast Boulevard to River Park Drive	65	69	Yes	70	+1	No
	River Park Drive to Town Center Parkway	65	70	Yes	71	+1	No
	Town Center Parkway to Mission Gorge Road	70	72	Yes	73	+1	No

Table 10. Near-Term Traffic Noise Levels

Roadway	Segment	Applicable Threshold (dBA Ldn)	Near-Term No Project (dBA Ldn)	Exceeds Threshold Without Project?	Near-Term + Project (dBA Ldn)	Increase in Noise Level from Near- Term No Project	Significant Impact?
	Cuyamaca Street to Princess Joann Road	65	Does Not Exist	No	63	NA	No
Magnolia Avenue	Princess Joann Road to Woodglen Vista Drive	65	60	No	66	+6	Yes
	Woodglen Vista Drive to El Nopal	65	66	Yes	69	+3	Yes
	El Nopal to Mast Boulevard	65	68	Yes	69	+1	No
SR-52	Santo Road to Mast Boulevard	70	76	Yes	77	+1	No

Table 10. Near-Term Traffic Noise Levels

Note: dBA = A-weighted decibel; Ldn = day-night average sound level; NA = not applicable; SR- = State Route

Unless otherwise noted, a substantial permanent increase in vehicle traffic noise would occur if implementation of the proposed project would result in an ambient noise level that exceeds the applicable threshold established in the Santee General Plan. If the normally acceptable standard would be exceeded without project implementation, an increase of more than 3 dBA would be considered significant.

Noise levels are calculated at 50 feet from roadway centerline, except SR-52 (100 feet from centerline due to roadway width). Noise levels are based upon traffic data provided by LLG (2020). Traffic levels for each roadway are included in the Appendix B. Decibel levels are rounded to the nearest whole number. Significant impacts shown in **bold** and **shading**. See Appendix B for data sheets.

¹ The nearest residences, located on Summit Avenue, are located more than 900 feet east of the centerline of Cuyamaca Street. At this distance, noise levels would be reduced to less than 65 dBA Ldn.

² Existing noise wall would reduce noise to an acceptable noise level.

Year 2035 Scenario

The Year 2035 scenario compares buildout of the adopted Santee General Plan and buildout of the Santee General Plan with the proposed project. Year 2035 traffic noise levels, with and without the proposed project, are provided in Table 11. As shown in this table, 17 of the 24 study area roadway segments would exceed applicable thresholds without implementation of the proposed project.

Table 11 identifies significant impacts from project-related traffic on three segments of Fanita Parkway. Table 11 also identifies two segments that would exceed applicable thresholds but are not ultimately identified as significant. Traffic noise on Cuyamaca Street from the project site to Magnolia Avenue would exceed 65 dBA Ldn with project implementation. However, the actual noise level at the nearest receptors to the proposed Cuyamaca Street extension would be reduced by distance compared to the noise level estimated in Table 11. These residences along Summit Avenue would be more than 900 feet from the proposed centerline of Cuyamaca Street. At this distance, noise levels would be reduced to less than 65 dBA Ldn, and a significant impact would not occur to this segment. Project-related traffic noise would result in an increase in noise levels of 3 dBA Ldn along one segment of Cuyamaca Street north of El Nopal would reduce the estimated roadway noise level of 66 dBA Ldn from Princess Joann Road to Chaparral Drive to the acceptable noise level of 61 dBA. Therefore, impacts to this segment would be less than significant. Three roadway segments of Fanita Parkway would result in a potentially significant noise impact under the Year 2035 scenario.

Roadway	Segment	Applicable Threshold (dBA Ldn)	Year 2035 No Project (dBA Ldn)	Exceeds Threshold Without Project?	Year 2035 + Project (dBA Ldn)	Increase in Noise Level from Year 2035 No Project	Significant Impact?
	SR-52 to West Hills Parkway	70	72	Yes	72	0	No
Mast Boulevard	West Hills Parkway to Medina Drive	65	71	Yes	72	+1	No
	Pebble Beach Drive to Fanita Parkway	65	71	Yes	72	+1	No
	SR-125 to Fanita Drive	70	78	Yes	78	0	No
Mission Gorge Road	Fanita Drive to Carlton Hills Boulevard	70	77	Yes	78	+1	No
	On-Site Portion to Ganley Road	65	64	No	66	+2	Yes
	Ganley Road to Lake Canyon Road	65	65	No	70	+5	Yes
Fanita Parkway	Lake Canyon Road to Mast Boulevard	65	66	Yes	70	+4	Yes
	Mast Boulevard to Carlton Oaks Drive	65	61	No	62	+1	No
Carlton Hills Boulevard	Carlton Oaks Drive to Mission Gorge Road	65	70	Yes	70	0	No

Table 11. Year 2035 Traffic Noise Levels

Roadway	Segment	Applicable Threshold (dBA Ldn)	Year 2035 No Project (dBA Ldn)	Exceeds Threshold Without Project?	Year 2035 + Project (dBA Ldn)	Increase in Noise Level from Year 2035 No Project	Significant Impact?
	On-Site Portion to Magnolia Avenue	65	65	No	67	+2	No ¹
	Magnolia Avenue to Princess Joann Road	65	64	No	65	+1	No
	Princess Joann Road to Chaparral Drive	65	65	No	66	+1	No ²
	Chaparral Drive to Woodglen Vista Drive	65	68	Yes	69	+1	No
Cuyamaca Street	Woodglen Vista Drive to El Nopal	65	70	Yes	70	0	No
	El Nopal to Mast Boulevard	65	71	Yes	71	0	No
	Mast Boulevard to River Park Drive	65	70	Yes	70	0	No
	River Park Drive to Town Center Parkway	65	71	Yes	71	0	No
	Town Center Parkway to Mission Gorge Road	70	73	Yes	74	+1	No
Magnolia Avenue	Cuyamaca Street to Princess Joann Road	65	61	No	63	+2	No
	Princess Joann Road to Woodglen Vista Drive	65	66	Yes	68	+2	No

Table 11. Year 2035 Traffic Noise Levels

Roadway	Segment	Applicable Threshold (dBA Ldn)	Year 2035 No Project (dBA Ldn)	Exceeds Threshold Without Project?	Year 2035 + Project (dBA Ldn)	Increase in Noise Level from Year 2035 No Project	Significant Impact?
	Woodglen Vista Drive to El Nopal	65	68	Yes	69	+1	No
	El Nopal to Mast Boulevard	65	71	Yes	71	0	No
SR-52	Santo Road to Mast Boulevard	70	77	Yes	77	0	No

Table 11. Year 2035 Traffic Noise Levels

Note: dBA = A-weighted decibel; Ldn = day-night average sound level; NA = not applicable; SR- = State Route

Unless otherwise noted, a substantial permanent increase in vehicle traffic noise would occur if implementation of the proposed project would result in an ambient noise level that exceeds the applicable threshold established in the Santee General Plan. If the normally acceptable standard would be exceeded without project implementation, an increase of more than 3 dBA would be considered significant.

Noise levels are calculated at 50 feet from roadway centerline except SR-52 (100 feet from centerline due to roadway width). Noise levels are based upon traffic data provided by LLG (2020). Traffic levels for each roadway are included in the Appendix B. Decibel levels are rounded to the nearest whole number. Significant impacts shown in **bold** and **shading**. See Appendix B for data sheets.

¹ The nearest residences, located on Summit Avenue, are located more than 900 feet east of the centerline of Cuyamaca Street. At this distance, noise levels would be reduced to less than 65 dBA Ldn.

² Existing noise wall would reduce noise to an acceptable level.

Land Use Plan Without School

If the proposed school is not developed on the project site as proposed in the preferred land use plan with school, the school site would be developed with 59 additional single-family units. Traffic noise levels for the land use plan without school have been analyzed to the same extent as the proposed project and are provided in Appendix C. Traffic noise level impacts under the land use plan without school would be identical to the preferred land use plan with school, with the exception of two segments:

- Fanita Parkway from Ganley Road to Lake Canyon Road: Noise levels under the land use plan without school are estimated to be 70 dBA Ldn under the Existing + Project scenario compared to 69 dBA Ldn under the preferred land use plan with school. Long-term noise levels under either land use plan are estimated to be 70 dBA Ldn. A potentially significant impact would occur under either land use plan.
- Magnolia Avenue from Cuyamaca Street to Princess Joann Road: Noise levels under the land use plan without school are estimated to be 64 dBA Ldn under the Year 2035
 + Project scenario compared to 63 dBA Ldn under the preferred land use plan with school. A significant impact would not occur under either land use plan.

The potentially significant impacts identified previously for the preferred land use plan with school would also occur under the land use plan without school, and no additional significant impacts have been identified for this scenario.

On-Site Exposure to Ambient Noise Levels

This section addresses the potential for on-site sensitive receptors to be exposed to ambient noise levels in excess of the 65 dBA Ldn standard established in the Santee General Plan Noise Element. CEQA is intended to protect the existing environment from impacts that would result from the proposed project. Generally, CEQA does not consider impacts of the existing environment on a proposed land use to be significant (see Section 15126.2 of the CEQA Guidelines). However, the Santee General Plan Noise Element states that a significant impact would occur if noise levels at any planned development site would exceed the noise levels considered compatible for that use as identified in Table 6. Therefore, the potential for ambient noise levels, primarily from vehicle traffic, to impact the proposed project is addressed below.

As shown in Table 7, the results of the ambient noise survey reflect daytime noise levels that range between 40 dBA and 60 dBA Leq on the project site. As described previously in Table 6, a normally acceptable ambient community noise level of up to 65 dBA Ldn is considered compatible with residential developments as specified in the Santee General Plan and is the applicable threshold of significance for NSLUs (City of Santee 2003). An ambient community noise level of up to 70 dBA Ldn is the applicable significance threshold for Neighborhood Parks and commercial buildings. Based on these compatibility guidelines, existing ambient noise levels across the site are compatible with the proposed land uses.

Following development, vehicle noise is anticipated to be the dominant source of ambient noise on the project site. Table 11 shows future noise levels on the major proposed on-site roadways, including Fanita Parkway (on-site portion to Ganley Road) and Cuyamaca Street (on-site portion to Magnolia Avenue). As shown in Table 11, traffic noise levels along major roadways would be approximately 66 dBA Ldn at 50 feet from the centerline of Fanita Parkway and 67 dBA Ldn at 50 feet from the centerline of Cuyamaca Street. Ambient noise levels would be compatible with parks and commercial buildings. Noise levels at Fanita Parkway and Cuyamaca Street would attenuate to acceptable levels of 65 dBA Ldn beyond approximately 65 feet of the centerline of Fanita Parkway and 75 feet from the centerline of Cuyamaca Street. Noise levels on other roadways on the project site would serve fewer vehicles and would generate lower noise levels. Additionally, masonry and glass walls are proposed along roadways throughout neighborhoods that would provide additional noise attenuation at receptors. Therefore, noise levels throughout the project site more than 75 feet from Fanita Parkway and Cuyamaca Street would be compatible with the proposed development. However, development within 75 feet of these roadways would be potentially exposed to noise levels in excess of 65 dBA Ldn.

Low Density Residential units proposed along Cuyamaca Street in Orchard Village would be separated from Cuyamaca Street by more than 75 feet and would not be exposed to noise levels above acceptable limits from Cuyamaca Street. However, the Low Density Residential units and Active Adult units that would be located adjacent to Fanita Parkway, and multi-family residential units located adjacent to Cuyamaca Street in the Village Center in Fanita Commons, would potentially be exposed to conditionally compatible noise levels. According to the Santee General Plan, conventional construction with closed windows is typically sufficient for compatibility. However, noise insulation features would potentially be required for these residences for consistency with the Santee General Plan. This on-site impact would be potentially significant.

Temporary Noise Increase

Construction of the proposed project would have the potential to result in temporary noise level increases as a result of increased traffic volumes and the operation of heavy equipment. The potential for these sources to result in a significant temporary noise increase is addressed below.

Construction Traffic Noise

This section addresses the potential for construction of the proposed project to temporarily increase ambient noise levels as a result of increased traffic noise. Existing traffic volumes without construction, and near-term volumes without construction, are provided in the traffic impact analysis prepared by LLG (2020). In addition, traffic construction volumes are provided by the Air Quality Technical Analysis prepared by LSA (2020). Grading cut and fill would be balanced on the project site. Construction equipment would remain on the site once it has arrived. Therefore, off-site truck noise during these activities would be minimal. However, daily worker trips and vendor truck trips would be required and would have the potential to temporarily increase ambient noise levels.

The highest volumes of construction vehicle trips are anticipated during building construction activities. During building construction, approximately 1,099 worker trips and 312 vendor trips are estimated daily for Phase 1 (see Section 2.2.10, Development Phasing, for construction phasing). These volumes are assumed as the worst-case scenario for Phase 1 construction. Following Phase 1, when operation and construction would potentially overlap, the worst-case scenario for building construction trips would occur during Phase 4. The worst-case construction traffic scenario was determined based on daily truck traffic because truck trips are the primary noise concern for vehicle noise impacts. Approximately 838 worker trips and 235 vendor trips are estimated daily during building construction activities in Phase 4. Worker and vendor trips calculated by the California Emissions Estimator Model for the air quality analysis are based on the amount of building construction required (residential units or square footage) during each phase (LSA 2020). These estimates are anticipated to be conservative. For example, calculations based on estimated material requirements provided by the applicant estimate daily vendor trips on certain days would be less than 20 one-way trips per day (O'Connor pers comm. 2019).

During the other construction activities (e.g., grading, paving, coating) during all phases, a maximum of 150 worker trips and no vendor trips are anticipated. A substantial temporary increase would occur if construction trips would result in an ambient noise level that would exceed the applicable exterior land use compatibility criteria, or would result in an increase of more than 3 dBA if the roadway already exceeds the standard without the addition of construction traffic. During Phase 1 of construction, all construction trips would access the project site via Fanita Parkway because the extensions to Cuyamaca Street and Magnolia Avenue would not be completed prior to this phase. Therefore, the existing analysis does not include the off-site segments of Cuyamaca Street and Magnolia Avenue would not serve the proposed project's operational traffic. The analysis of near-term conditions assumes that the Cuyamaca Street and Magnolia Avenue extensions would be accessible following Phase 1 and that construction trips may use any roadway. Following Phase 1, the analysis conservatively assumes 100 percent of construction traffic on each segment of Fanita Parkway and Magnolia Avenue. This represents a worst-case scenario for Cuyamaca Parkway and Magnolia Avenue because construction traffic is anticipated to primarily access the site from Fanita Parkway.

Existing + Construction Scenario

Table 12 provides the estimated traffic noise levels for Phase 1 construction activities other than building construction, including site preparation, grading, paving, utilities installation, and surface improvements. Table 13 provides estimated traffic noise levels compared to existing noise levels during the building construction period of any phase. As shown in Table 12, no significant increase in traffic noise levels would occur during construction activities other than building construction during Phase 1. However, as shown in Table 13, the additional construction traffic that would occur during the building construction phase would cause a significant increase in traffic noise levels on two segments of Fanita Parkway. Therefore, building construction would result in a temporary significant increase in traffic noise to existing receptors on two roadway segments.

Roadway	Segment	Applicable Threshold (dBA Ldn)	Existing (dBA Ldn)	Exceeds Threshold Without Construction?	Existing + Construction (dBA Ldn)	Increase in Noise Level from Existing	Significant Impact?
	SR-52 to West Hills Parkway	70	71	Yes	71	0	No
Mast Boulevard	West Hills Parkway to Medina Drive	65	70	Yes	70	0	No
	Pebble Beach Drive to Fanita Parkway	65	70	Yes	70	0	No
	SR-125 to Fanita Drive	70	77	Yes	77	0	No
Mission Gorge Road	Fanita Drive to Carlton Hills Boulevard	70	77	Yes	77	0	No
	On-Site Portion to Ganley Road	65	Does Not Exist	No	47	NA	No
Fanita Parkway	Ganley Road to Lake Canyon Road	65	59	No	62	+3	No
Falilla Falkway	Lake Canyon Road to Mast Boulevard	65	61	No	64	+3	No
	Mast Boulevard to Carlton Oaks Drive	65	58	No	59	+1	No
Carlton Hills Boulevard	Carlton Oaks Drive to Mission Gorge Road	65	69	Yes	69	0	No
SR-52	Santo Road to Mast Boulevard	70	76	Yes	76	0	No

Table 12. Existing + Construction Traffic Noise Levels (Construction Activities Other than Building Construction)

Note: dBA = A-weighted decibel; Ldn = day-night average sound level; NA = not applicable; SR- = State Route

Unless otherwise noted, a substantial temporary increase in vehicle traffic noise would occur if implementation of proposed project construction would result in an ambient noise level that exceeds the applicable threshold established in the Santee General Plan. If the normally acceptable standard would be exceeded without the addition of construction traffic, an increase of more than 3 dBA attributable to construction traffic would be considered significant.

The existing condition represents conditions in 2018. Noise levels are calculated at 50 feet from roadway centerline, except SR-52 (100 feet from centerline due to roadway width). Noise levels are based upon traffic data provided by LLG (2020) and LSA (2020). Traffic levels for each roadway are included in Appendix D. Decibel levels are rounded to the nearest whole number. See Appendix D for data sheets. Assumes 100 percent of construction traffic would access the site using Fanita Parkway; therefore, Cuyamaca Street and Magnolia Avenue are not included in the table.

Roadway	Segment	Applicable Threshold (dBA Ldn)	Existing (dBA Ldn)	Exceeds Threshold Without Construction?	Existing + Construction (dBA Ldn)	Increase in Noise Level from Existing	Significant Impact?
	SR-52 to West Hills Parkway	70	71	Yes	72	+1	No
Mast Boulevard	West Hills Parkway to Medina Drive	65	70	Yes	71	+1	No
	Pebble Beach Drive to Fanita Parkway	65	70	Yes	71	+1	No
	SR-125 to Fanita Drive	70	77	Yes	78	+1	No
Mission Gorge Road	Fanita Drive to Carlton Hills Boulevard	70	77	Yes	77	0	No
	On-Site Portion to Ganley Road	65	Does Not Exist	No	64	NA	No
	Ganley Road to Lake Canyon Road	65	59	No	67	+8	Yes
Fanita Parkway	Lake Canyon Road to Mast Boulevard	65	61	No	68	+7	Yes
	Mast Boulevard to Carlton Oaks Drive	65	58	No	64	+6	No

 Table 13. Existing + Building Construction Traffic Noise Levels

Roadway	Segment	Applicable Threshold (dBA Ldn)	Existing (dBA Ldn)	Exceeds Threshold Without Construction?	Existing + Construction (dBA Ldn)	Increase in Noise Level from Existing	Significant Impact?
Carlton Hills Boulevard	Carlton Oaks Drive to Mission Gorge Road	65	69	Yes	70	+1	No
SR-52	Santo Road to Mast Boulevard	70	76	Yes	76	0	No

 Table 13. Existing + Building Construction Traffic Noise Levels

Note: dBA = A-weighted decibel; Ldn = day-night average sound level; NA = not applicable; SR- = State Route

Unless otherwise noted, a substantial temporary increase in vehicle traffic noise would occur if implementation of the proposed project construction would result in an ambient noise level that exceeds the applicable threshold established in the Santee General Plan. If the normally acceptable standard would be exceeded without the addition of construction traffic, an increase of more than 3 dBA attributable to construction traffic would be considered significant.

The existing condition represents conditions in 2018. Noise levels are calculated at 50 feet from roadway centerline, except SR-52 (100 feet from centerline due to roadway width). Noise levels are based upon traffic data provided by LLG (2020) and LSA (2020). Traffic levels for each roadway are included in Appendix E. Decibel levels are rounded to the nearest whole number. Significant impacts shown in **bold** and shading. See Appendix E for data sheets. Assumes 100 percent of construction traffic with access the site via Fanita Parkway; therefore, Cuyamaca Street and Magnolia Avenue are not included in the table.

Near-Term + Interim Operation + Construction Scenario

Following completion of Phase 1, area roadways would experience an increase in vehicle trips as a result of incremental increases in operational trips, as well as construction traffic through project buildout. The Near-Term + Interim Operation + Construction scenario assumes 50 percent of traffic volumes from full operation of the proposed project to determine whether construction would result in a significant temporary increase in noise level compared to noise levels without construction. Table 14 provides the estimated traffic noise levels for interim operation and construction activities other than building construction compared to near-term noise levels without the proposed project. Table 15 provides estimated traffic noise levels compared to near-term noise levels during a building construction period and interim operation. Normal construction activities from a later phase would have the potential to overlap with normal construction or building construction from a previous phase. A scenario that includes interim operation with a simultaneous normal construction period and building construction period was modeled and is included in Appendix D. Impacts were the same as those identified in Table 15. As such, Table 15 also represents potential impacts from potential overlap in construction phases.

As shown in Tables 14 and 15, compared to existing conditions, several roadways would experience a significant increase in noise level in the Near-Term + Interim Operation + Construction scenario. However, these increases would be primarily attributable to the increase in permanent operational traffic rather than construction traffic. As shown in Table 14, no significant impacts associated with construction traffic noise would occur during activities without building construction. As shown in Table 15, construction traffic noise levels during building construction would result in temporary significant noise impacts on one segment of Fanita Parkway and two segments of Magnolia Avenue.

Roadway	Segment	Applicable Threshold (dBA Ldn)	Near Term (dBA Ldn)	Exceeds Threshold Without Interim Operation and Construction?	Near Term+ Interim Operation (dBA Ldn)	Near Term + Interim Operation + Construction (dBA Ldn)	Increase Attributable to Construction ¹	Significant Additional Impact?
	SR-52 to West Hills Parkway	70	72	Yes	72	73	+1	No
Mast Boulevard	West Hills Parkway to Medina Drive	65	70	Yes	71	71	0	No
	Pebble Beach Drive to Fanita Parkway	65	70	Yes	71	71	0	No
Missian Osma	SR-125 to Fanita Drive	70	77	Yes	78	78	0	No
Mission Gorge Road	Fanita Drive to Carlton Hills Boulevard	70	77	Yes	77	77	0	No
	On-Site Portion to Ganley Road	65	Does Not Exist	No	63	64	+1	No
Conito Dorkwow	Ganley Road to Lake Canyon Road	65	60	No	67	67	0	No
Fanita Parkway	Lake Canyon Road to Mast Boulevard	65	61	No	68	68	0	No
	Mast Boulevard to Carlton Oaks Drive	65	59	No	60	61	+1	No
	On-Site Portion to Magnolia Avenue	65	Does Not Exist	No	64	64	0	No
Cuyamaca Street	Magnolia Avenue to Princess Joann Road	65	Does Not Exist	No	61	61	0	No
	Princess Joann Road to Chaparral Drive	65	Does Not Exist	No	61	61	0	No

Table 14. Near-Term + Interim Operation and Construction Traffic Noise Levels (Construction Activities Other than Building Construction)

		-		Exceeds	,	Near Term +		
Roadway	Segment	Applicable Threshold (dBA Ldn)	Near Term (dBA Ldn)	Threshold Without Interim Operation and Construction?	Near Term+ Interim Operation (dBA Ldn)	Interim Operation + Construction (dBA Ldn)	Increase Attributable to Construction ¹	Significant Additional Impact?
	Chaparral Drive to Woodglen Vista Drive	65	54	No	65	65	0	No
	Woodglen Vista Drive to El Nopal	65	62	No	68	68	0	No
	El Nopal to Mast Boulevard	65	65	No	70	70	0	No
	Mast Boulevard to River Park Drive	65	69	Yes	69	69	0	No
	River Park Drive to Town Center Parkway	65	70	Yes	70	70	0	No
	Town Center Parkway to Mission Gorge Road	65	72	Yes	73	73	0	No
	Cuyamaca Street to Princess Joann Road	65	Does Not Exist	No	60	60	0	No
Magnolia Avenue	Princess Joann Road to Woodglen Vista Drive	65	60	No	64	64	0	No
	Woodglen Vista Drive to El Nopal	65	66	Yes	68	68	0	No
	El Nopal to Mast Boulevard	65	68	Yes	69	69	0	No

Table 14. Near-Term + Interim Operation and Construction Traffic Noise Levels (Construction Activities Other than Building Construction)

Table 14. Near-Term + Interim Operation and Construction Traffic Noise Levels (Construction Activities Other than Building Construction)

Roadway	Segment	Applicable Threshold (dBA Ldn)	Near Term (dBA Ldn)	Exceeds Threshold Without Interim Operation and Construction?	Near Term+ Interim Operation (dBA Ldn)	Near Term + Interim Operation + Construction (dBA Ldn)	Increase Attributable to Construction ¹	Significant Additional Impact?
Carlton Hills Boulevard	Carlton Oaks Drive to Mission Gorge Road	65	69	Yes	70	70	0	No
SR-52	Santo Road to Mast Boulevard	70	76	Yes	76	76	0	No

Note: dBA = A-weighted decibel; Ldn = day-night average sound level; SR- = State Route

Unless otherwise noted, a substantial temporary increase in vehicle traffic noise would occur if implementation of the proposed project construction would result in an ambient noise level that exceeds the applicable threshold established in the Santee General Plan. If the normally acceptable standard would be exceeded without the addition of construction traffic, an increase of more than 3 dBA attributable to construction traffic would be considered significant.

The existing condition represents conditions in 2018. Noise levels are calculated at 50 feet from roadway centerline, except SR-52 (100 feet from centerline due to roadway width). Noise levels are based upon traffic data provided by LLG (2020) and LSA (2020). Traffic levels for each roadway are included in Appendix D. Decibel levels are rounded to the nearest whole number. See Appendix D for data sheets.

¹ In increase attributable to construction is the increase in noise level from Near-Term + Interim Operation to Near-Term + Interim Operation + Construction.

Roadway	Segment	Applicable Threshold (dBA Ldn)	Near Term (dBA Ldn)	Exceeds Threshold Without Construction?	Near Term + Interim Operation (dBA Ldn)	Near Term + Interim Project + Construction (dBA Ldn)	Increase Attributable to Construction ¹	Significant Additional Impact?
	SR-52 to West Hills Parkway	70	72	Yes	72	73	+1	No
Mast Boulevard	West Hills Parkway to Medina Drive	65	70	Yes	71	72	+1	No
	Pebble Beach Drive to Fanita Parkway	65	70	Yes	71	72	+1	No
Mission Gorge Road	SR-125 to Fanita Drive	70	77	Yes	78	78	0	No
	Fanita Drive to Carlton Hills Boulevard	70	77	Yes	77	78	+1	No
Fanita Parkway	On-Site Portion to Ganley Road	65	Does Not Exist	No	63	66	+3	Yes
	Ganley Road to Lake Canyon Road	65	60	No	67	69	+2	No
	Lake Canyon Road to Mast Boulevard	65	61	No	68	70	+2	No
	Mast Boulevard to Carlton Oaks Drive	65	59	No	60	64	+4	No

Table 15. Near Term + Interim Operation and Building Construction Traffic Noise Levels

Roadway	Segment	Applicable Threshold (dBA Ldn)	Near Term (dBA Ldn)	Exceeds Threshold Without Construction?	Near Term + Interim Operation (dBA Ldn)	Near Term + Interim Project + Construction (dBA Ldn)	Increase Attributable to Construction ¹	Significant Additional Impact?
Cuyamaca Street	On-Site Portion to Magnolia Avenue	65	Does Not Exist	No	64	66	+2	No ²
	Magnolia Avenue to Princess Joann Road	65	Does Not Exist	No	61	65	+4	No
	Princess Joann Road to Chaparral Drive	65	Does Not Exist	No	61	65	+4	No
	Chaparral Drive to Woodglen Vista Drive	65	54	No	65	68	+3	No ³
	Woodglen Vista Drive to El Nopal	65	62	No	68	70	+2	No
	El Nopal to Mast Boulevard	65	65	No	70	71	+1	No
	Mast Boulevard to River Park Drive	65	69	Yes	69	70	+1	No
	River Park Drive to Town Center Parkway	65	70	Yes	70	71	+1	No
	Town Center Parkway to Mission Gorge Road	65	72	Yes	73	74	+1	No

Table 15. Near Term + Interim Operation and Building Construction Traffic Noise Levels

Roadway	Segment	Applicable Threshold (dBA Ldn)	Near Term (dBA Ldn)	Exceeds Threshold Without Construction?	Near Term + Interim Operation (dBA Ldn)	Near Term + Interim Project + Construction (dBA Ldn)	Increase Attributable to Construction ¹	Significant Additional Impact?
	Cuyamaca Street to Princess Joann Road	65	Does Not Exist	No	60	64	+4	No
Magnolia Avenue	Princess Joann Road to Woodglen Vista Drive	65	60	No	64	67	+3	Yes
	Woodglen Vista Drive to El Nopal	65	66	Yes	68	69	+1	Yes
	El Nopal to Mast Boulevard	65	68	Yes	69	70	+1	No
Carlton Hills Boulevard	Carlton Oaks Drive to Mission Gorge Road	65	69	Yes	70	70	0	No
SR-52	Santo Road to Mast Boulevard	70	76	Yes	76	77	+1	No

Table 15. Near Term + Interim Operation and Building Construction Traffic Noise Levels

Note: dBA = A-weighted decibel; Ldn = day-night average sound level; NA = not applicable; SR- = State Route

Unless otherwise noted, a substantial temporary increase in vehicle traffic noise would occur if implementation of the proposed project construction would result in an ambient noise level that exceeds the applicable threshold established in the Santee General Plan. If the normally acceptable standard would be exceeded without the addition of construction traffic, an increase of more than 3 dBA attributable to construction traffic would be considered significant.

Noise levels are calculated at 50 feet from roadway centerline, except SR-52 (100 feet from centerline due to roadway width). Noise levels are based upon traffic data provided by LLG (2020) and LSA (2020). Traffic levels for each roadway are included in Appendix E. Decibel levels are rounded to the nearest whole number. Significant impacts shown in **bold** and **shading**. See Appendix E for data sheets.

¹ In increase attributable to construction is the increase in noise level from Near-Term + Interim Operation to Near-Term + Interim Operation + Construction

² The nearest residences, located on Summit Avenue, are located more than 900 feet east of the centerline of Cuyamaca Street. At this distance, noise levels would be reduced to less than 65 dBA Ldn.

³ Existing noise wall would reduce noise to an acceptable level.

Construction Equipment Noise

Construction of the proposed project would generate noise that could expose nearby receptors to elevated noise levels that may disrupt communication and routine activities. The magnitude of the impact would depend on the type of construction activity, equipment, duration of the construction phase, distance between the noise source and receiver, and intervening structures. Sound levels from typical construction equipment range from 60 dBA to 90 dBA Leq at 50 feet from the source (FHWA 2008). Noise from construction equipment generally exhibits point source acoustical characteristics. Strictly speaking, a point source sound decays at a rate of 6 dBA per doubling of distance from the source. The rule applies to the propagation of sound waves with no ground interaction.

Construction of the proposed project is anticipated to begin in 2021 and would occur in four phases, with a buildout of approximately 10 to 15 years. The anticipated construction phasing for the proposed project is provided on Figure 4. Temporary construction activity noise would be considered significant if it would violate the limits established in Section 5.04.090 of the City's Noise Ordinance. The ordinance prohibits operation of any construction equipment outside the hours of 7:00 a.m. through 7:00 p.m., Monday through Saturday, excluding legal holidays, without approval from the Director of Development Services. Also, construction equipment with the potential to exceed 85 dBA at the construction site shall not be operated at the same location for more than 10 consecutive workdays without notification to properties within 300 feet of the site.

Construction Noise

Standard equipment, such as dozers, loaders, graders, backhoes, scrapers, and miscellaneous trucks would be required for most construction days. Some blasting may be required and is described separately below. Noise levels from construction on the project site were determined based on typical equipment noise levels determined by the RCNM (FHWA 2008). A semi-portable rock crushing/processing facility is anticipated to be used for aggregate plant operations during on-site grading activities so that excavated material may be used on site rather than exported. Aggregate plant operations are anticipated to be stationed in the northern portion of Fanita Commons during Phase 1 and Phase 2 of construction, in approximately the middle of the eastern boundary of Vineyard Village during Phase 3, and in approximately the northeast corner of Vineyard Village during Phase 4. Based on estimated noise levels for a quarry project that would include rock crushing and processing, noise levels from these activities would be approximately 85 dBA at a distance of 100 feet from equipment (91 dBA at 50 feet) (Shasta County 2011). The eight noisiest pieces of construction equipment (excavator, dozer, grader, dump truck, loader, scraper, rock crusher, and aggregate processing plant²) that could be required for on-site construction were assumed to operate in the same location, and would have the potential to generate noise levels up

² The RCNM model does not include an option for rock crushing or processing (aggregate plant). Sand blasting equipment, which is estimated to have an Lmax of 95.7 at 50 feet, is conservatively assumed to represent this equipment.

to approximately 92.7 dBA at 50 feet from the construction site. These estimates are conservative because construction equipment for a single construction activity would likely be spread out over several acres.

Standard construction operation would have the potential to exceed 85 dBA at the construction site for more than 10 consecutive workdays, and would require notification in accordance with the City's Noise Ordinance (Appendix F). However, the bulk of construction activities would occur within the three proposed villages, which would be separated from existing development by the Habitat Preserve. The closest sensitive receptors to the villages are located approximately 850 feet east of the proposed Vineyard Village boundary along Oak Creek Drive in the unincorporated County. Construction of phases would have the potential to overlap. However, due to the distance between the villages, it would be unlikely for noise from simultaneous construction to be simultaneously audible at a given receptor. Additionally, off-site residences would continue to be located outside the 300-foot notification boundary. Therefore, typical construction activities within the villages would not require construction notification because no City receptors would be located within the 300-foot notification boundary. Additionally, at this distance, noise levels from worstcase construction with rock crushing would attenuate to 68 dBA and would not exceed the County's Noise Ordinance limit of 75 dBA for construction. Construction within the villages would take place during the allowable City Noise Ordinance hours of 7:00 a.m. to 7:00 p.m. A significant impact would not occur to off-site receptors during the on-site construction of Phase 1 (Fanita Commons and the easterly portion of Orchard Village), or during construction of Phases 2, 3, or 4. The timing of the construction of Magnolia Avenue will be tied to the certificate of occupancy of the 1,500th equivalent dwelling unit³ in the proposed project; however, the exact date of this is unknown.

However, on-site and off-site construction of Phase 1 would include development of new segments and improvements to Fanita Parkway and Cuyamaca Street, including the widening of Fanita Parkway north of Lake Canyon Drive, which would include construction adjacent to existing residential areas and near the campground at Santee Lakes Recreation Preserve. Construction of Magnolia Avenue would also be adjacent to existing residential and school areas. Additionally, dead-end roadway improvements along the southern boundary of the site in the existing neighborhood north of Mast Boulevard would potentially require some heavy construction equipment. Construction for roadway improvements would be linear and the active construction area would be much smaller than on-site land development. For roadway improvements, the four noisiest pieces of construction equipment (excavator, dozer, loader, and scraper) that are assumed for paving operations were anticipated to operate simultaneously in the same location. Construction of new segments and improvements to Fanita Parkway and Cuyamaca Street would

³ Equivalent dwelling unit is a unit of measure that defines impact relative to a typical single-family residence. Based on the Traffic Impact Analysis (LLG 2020), every 8.91 daily trips that a proposed use would generate would be its dwelling unit equivalent.

have the potential to generate noise levels up to approximately 85 dBA at 50 feet from the construction area (Appendix G).

Operation of heavy equipment during roadway construction would potentially create a substantial short-term noise increase affecting residences near the construction site and notification would be required to comply with the City's Noise Ordinance. The noise levels generated by construction equipment would vary greatly depending upon factors such as the type and specific model of the equipment, the operation being performed, and the condition of the equipment. The average sound level of the construction activity also depends upon the amount of time that the equipment operates and the intensity of the construction during the time period. Construction activities are anticipated to occur during the City's allowable hours of operation; however, some nighttime construction within roadways may be required to avoid traffic impacts. Existing residences are located within 300 feet of the construction areas along Fanita Parkway, Cuyamaca Street, and Magnolia Avenue, and dead-end roadway improvements on the southern boundary of the site. Because construction would be linear, individual receptors may not be exposed to construction noise for 10 consecutive workdays. However, operation of heavy equipment during construction would have the potential to create substantial short-term noise increases that require notification, and nighttime construction may be required that would conflict with the City's Noise Ordinance without approval from the Director of Development Services. This impact would be potentially significant.

Blasting Operation

Blasting may be required at locations within the development area (Hunsaker & Associates 2020). Construction blasting generates a maximum noise level of approximately 94 dB at a distance of 50 feet that is very short in duration (FHWA 2006). Drilling would also be necessary to bore holes for the blasting materials. Rock drills generate noise levels of approximately 85 dBA at a distance of 50 feet (FHWA 2006) and may be in operation for several hours in a day. It is anticipated that no more than one blast would occur in one area per day. However, even if more than one blast would occur in any one area per day, several hours would pass between blasts because of the time required to drill the holes and insert and connect the blasting materials.

Drilling and blasting are not anticipated to occur in the same area for more than 10 consecutive workdays. Additionally, the residences closest to village development are approximately 850 feet east of the proposed Vineyard Village boundary near Oak Creek Drive in the unincorporated County. At this distance, noise levels from blasting would be reduced to 69 dBA and would not exceed the County's Noise Ordinance limit of 75 dBA for construction noise. There are no existing City receptors within the 300 feet notification boundary for construction noise impacts. Additionally, drilling and blasting would occur during daytime hours. Therefore, temporary noise impacts as a result of drilling and blasting in the village development area would be consistent with the Noise Ordinance, and impacts would be less than significant.

5.1.1.2 Mitigation Measures

Implementation of the proposed project would have the potential to result in excessive noise levels as a result of potential nighttime nuisance noise at the Special Use area, temporary and permanent increases in ambient noise level, exposure of proposed NSLUs to noise levels in excess of Santee General Plan compatibility standards, and excessive noise levels during construction activities.

Operational Noise Mitigation Measures

Noise Exposure from Special Use Area

The following mitigation measure would eliminate commercial nighttime access in the Special Use area and reduce impacts to a less than significant level:

- **NOI-1: Special Use Area Noise Measures.** The following requirements for the Special Use area shall be included as conditions of approval in the development review permit between the applicant and the City of Santee:
 - Any electronic or automatic gate installed at Special Use area access points shall not generate noise levels that exceed 65 A-weighted decibels at the access point. The site operator shall provide specifications from the manufacturer prior to gate installation, and the site operator agreement shall include proper maintenance of the gate. Proper maintenance shall include response within 1 business day to complaints received by the site operator from residents or received from the City as a result of a complaint regarding nuisance noise as a result of disrepair. The response shall detail measures that the site operator will take to address the complaint and a timeline, such as a scheduled maintenance appointment.
 - Use of the Special Use area as a storage facility shall limit access to the site to the hours of 7:00 a.m. to 7:00 p.m., with the exception of a special after-hours pickup and drop-off location. Stored property shall be relocated to or from the after-hours location during normal business hours because access to the regular storage facilities shall be restricted to 7:00 a.m. to 7:00 p.m. The after-hours location shall be secured with an additional access gate that can only be opened with a temporary gate code provided through pre-arrangement with the site operator. The after-hours location shall be screened from existing receptors by the regular storage facilities.

Permanent Increase in Vehicle Noise

The proposed project would have the potential to result in significant vehicle noise impacts due to project operation. Table 16 provides a summary of the permanent vehicle impacts and where they would occur.

Scenario When Impact Maximum Nois								
Roadway	Segment	Would Occur	Feet (dBA Ldn)					
	On-Site Portion to Ganley Road	 Existing + Project Near Term + Project Year 2035 + Project Cumulatively Considerable 	66					
Fanita Parkway	Ganley Road to Lake Canyon Road	 Existing + Project Near Term + Project Year 2035 + Project Cumulatively Considerable 	70					
	Lake Canyon Road to Mast Boulevard	 Existing + Project Near Term + Project Year 2035 + Project Cumulatively Considerable 	70					
Cuyamaca Street (Silver Country Estates)	El Nopal to Mast Boulevard	Existing + ProjectNear Term + Project	71					
Magnolia Avenue	Princess Joann Road to Woodglen Vista Drive	Existing + ProjectNear Term + Project	68					
iviagnolia Avenue	Woodglen Vista Drive to El Nopal	Existing + ProjectNear Term + Project	69					

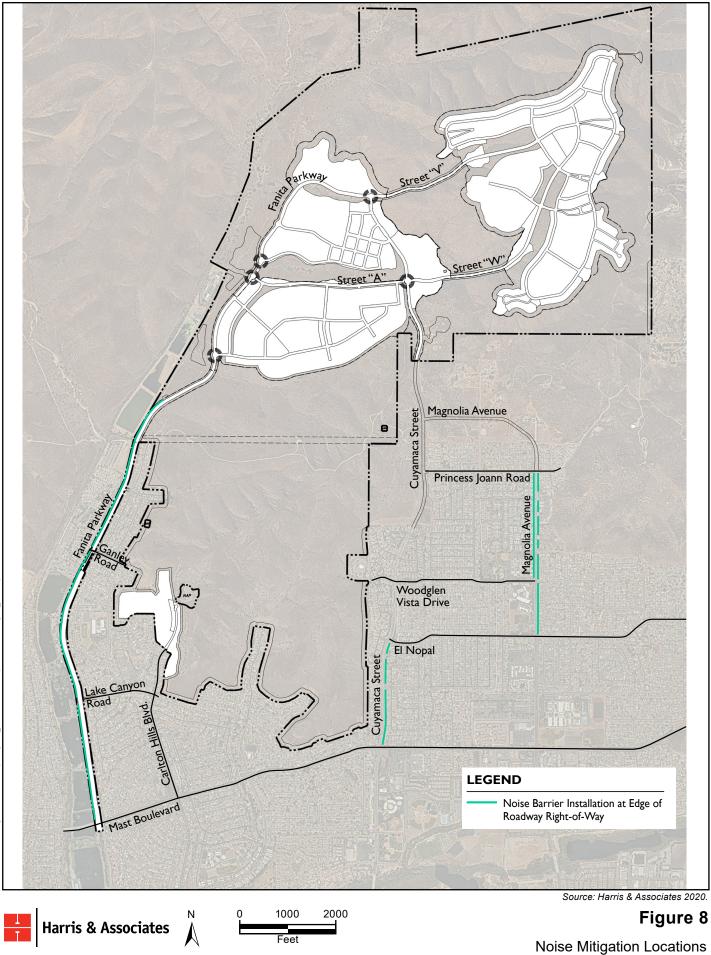
Table 16. Significant Permanent Vehicle Noise Impact Summary

Sources: LLG 2020.

Notes: dBA = A-weighted decibel; Ldn = day-night average sound level

As shown in Table 16, vehicle noise levels on Fanita Parkway and Magnolia Avenue under all scenarios would be within the conditionally compatible noise level range of 70 dBA Ldn or below for residential development but would exceed the applicable threshold of significance of 65 dBA Ldn (the normally acceptable noise level). Noise levels on the segment of Cuyamaca Street from El Nopal to Mast Boulevard would also potentially exceed the conditionally compatible noise level range. Mitigation Measure NOI-2 requires the installation of a noise barrier on some impacted segments of Fanita Parkway, Cuyamaca Street, and Magnolia Avenue, as shown on Figure 8, Noise Mitigation Locations. Noise barriers that break the line of sight between receptors and the roadway would provide at least 5 dBA in noise reduction, and additional reductions can be achieved with additional height or material selection. Typical noise barriers constructed for the purpose of reducing vehicle noise can provide 30 dBA of noise reduction (Caltrans 2013a). Appendix H includes a sample noise barrier calculation for Fanita Parkway.

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Due to the difference in elevation between the proposed Fanita Parkway improvements and the sensitive receptors at the Santee Lakes Recreation Preserve campground (vertical difference of approximately 12 feet), it is calculated that a 4-foot wall at the western edge of the Fanita Parkway roadway right-of-way for the entire length of the campground would break the line of sight between the source and receptor. Taking distance, change in elevation, and barrier height into account, a 4-foot wall at the roadway right-of-way is calculated to reduce noise levels to 60 dBA Ldn at the nearest campsites (Appendix H). Noise barriers in the roadway right-of-way are anticipated to be feasible on the western side of Fanita Parkway from the project entrance to Mast Boulevard (as mentioned previously), from El Nopal to Mast Boulevard on the eastern side of Cuyamaca Street, and at individual neighborhoods north of El Nopal on Magnolia Avenue.

However, it is not feasible to construct noise barriers on all impacted segments identified in Table 16 due to existing cross streets, driveways, and differences in grade between the roadways and receptors that would make barriers installed within the roadway right-of-way ineffective. Noise walls up to approximately 20 feet in height in the roadway right-of-way would be required on the eastern side of Fanita Parkway to break the line of sight and provide noise attenuation at adjacent receptors. Noise walls up to approximately 23 feet in height would be required on the western side of Cuyamaca Street (Appendix H). At these heights, noise walls would be visually incompatible with the surrounding community and above the Caltrans maximum noise barrier height of 14 to 16 feet, depending on distance from travel lanes (Caltrans 2017). Additionally, the City's Zoning Ordinance generally limits noise walls to a maximum height of 8 feet (Santee Municipal Code, Section 13.10.050[F][2]). Therefore, noise walls are not considered feasible along these segments of Fanita Parkway and Cuyamaca Street. Additional noise barriers may be feasible on Fanita Parkway and Cuyamaca Street if barriers can be negotiated with private property owners to be installed at existing fence lines rather than in the roadway right-of-way; however, such agreements cannot be guaranteed at this time, and even if some property owners agree, the barriers would need to be continuous across multiple properties to be effective. Therefore, this is not considered to be a feasible mitigation measure. Table 17 shows project noise levels with implementation of noise barriers on either side of impacted roadways, where feasible.

The installation of asphalt rubber pavement was considered for mitigation on impacted segments where installation of a noise barrier would not be feasible. As explained in detail in the Use of Asphalt Rubber as CEQA Mitigation Memorandum, provided as Appendix I, studies have demonstrated that asphalt rubber pavement can reduce on-board sound intensity (noise level where tire meets the pavement) by 3 dBA at the time of installation, although the reduction in sound intensity varied based on material (UCPRC 2012). In some instances, compared to traditional asphalt, asphalt rubber pavement has achieved community noise level reductions of 5 dBA and up to 14 dBA in several case studies (Putman and Amirkhanian 2005). The noise-reducing properties of asphalt rubber pavement cannot be demonstrated with certainty to reduce noise levels to below the threshold of 65 dBA Ldn, and the success of asphalt rubber to reduce noise levels varies between available case studies. Additionally, the noise-reducing properties of asphalt rubber to reduce noise levels varies between available case studies. Additionally, the noise-reducing properties of asphalt rubber pavement deteriorate over time, and the effectiveness of community noise reduction cannot be guaranteed prior to installation. Based on review of available research, it is

anticipated that asphalt rubber pavement would require replacement approximately every 7 to 9 years to maintain noise reduction benefits (UCPRC 2012). This replacement schedule would result in additional impacts compared to regular pavement, which the City currently replaces at an average of every 15 years or more. Unlike traditional pavement, the entire length of asphalt rubber would need to be removed and replaced rather than limiting maintenance to worn areas. More frequent replacement would cause nuisance impacts and disruption from more frequent street closures, additional exposure to construction noise, and additional criteria pollutant and greenhouse gas emissions. Finally, PDMWD has major water and sewer facilities within affected roadways that require frequent maintenance. PDMWD emailed comments to the City on March 10, 2020 (Mael pers comm. 2020), related to the frequency of maintenance and replacement of asphalt rubber pavement, including nuisance noise impacts to Santee Lakes Recreation Preserve campground and undue burden to PDMWD's operations and budget. Therefore, it was determined that the potential adverse impacts of asphalt rubber pavement outweigh the potential benefits in this circumstance. After careful consideration, weighing all the factors for the proposed project, the use of asphalt rubber pavement as a mitigation measure to reduce traffic noise levels has been determined to be infeasible. Impacts to some segments of Fanita Parkway, Cuyamaca Street, and Magnolia Avenue would remain significant and unavoidable.

- Noise Barrier Installation. A permanent noise barrier shall be installed on the western NOI-2: side of Fanita Parkway from Mast Boulevard to the project site, on the eastern side of Cuyamaca Street from Mast Boulevard to El Nopal, and at individual neighborhoods on Magnolia Avenue north of El Nopal in conjunction with proposed improvements to these roadways. Installation of a noise barrier on Magnolia Avenue may interfere with current access from apartment buildings to the existing sidewalk. In these areas, noise barrier installation would include providing a new walkway adjacent to the wall to provide sidewalk access at existing driveways. The noise barriers shall be designed by a qualified acoustical engineer. The applicant shall submit an analysis to the Director of Development Services prior to the start of construction that demonstrates that the proposed noise barriers would reduce traffic noise exposure at residential receptors to 65-A-weighted-decibel community noise equivalent level or below on Fanita Parkway and Cuyamaca Street. The noise level on Magnolia Avenue is estimated to exceed 65 A-weighted decibels without project traffic. The barrier on Magnolia Avenue shall demonstrate a reduction in noise exposure to a 66-A-weighteddecibel day-night average sound level or below. Noise barriers shall be installed concurrently with the following proposed roadway improvements:
 - Extension and widening of Fanita Parkway prior to the commencement of building construction activity on site
 - Extension and widening of Cuyamaca Street prior to issuance of the first certificate of occupancy
 - Extension of Magnolia Avenue prior to construction and certificate of occupancy of the 1,500th equivalent dwelling unit

Roadway	Segment	Mitigation	Unmitigated Worst-Case Noise Level (dBA Ldn)	Worst Case + Project Noise Level with Mitigation (dBA Ldn) ¹	Significant Impact?
	On-Site Portion to Ganley Road – western side of street	Noise Barrier Installation (NOI-2)	66	61	No
	On-Site Portion to Ganley Road – eastern side of street	No feasible mitigation	66	66	Yes
Fanita Parkway	Ganley Road to Lake Canyon Road – western side of street	Noise Barrier Installation (NOI-2)	70	65	No
,	Ganley Road to Lake Canyon Road – eastern side of street	No feasible mitigation	70	70	Yes
	Lake Canyon Road to Mast Boulevard – western side of street	Noise Barrier Installation (NOI-2)	70	65	No
	Lake Canyon Road to Mast Boulevard – eastern side of street	No feasible mitigation	70	70	Yes
Cuyamaca Street	El Nopal to Mast Boulevard – western side of street	No feasible mitigation	71	71	Yes
(Silver Country Estates)	El Nopal to Mast Boulevard – east side of street	Noise Barrier Installation (NOI-2)	71	65	No
	Princess Joann Road to Woodglen Vista Drive	Noise Barrier Installation (NOI-2)	68	63	No
Magnolia Avenue	Woodglen Vista Drive to El Nopal – residential neighborhoods	Noise Barrier Installation (NOI-2)	69	64	No
	Woodglen Vista Drive to El Nopal – schools	No feasible mitigation	69	69	Yes ²

Table 17. Permanent Vehicle Noise Impact with Noise Barrier Installation Mitigation

Note: dBA = A-weighted decibel; Ldn = day-night average sound level

Noise levels are calculated at 50 feet from roadway centerline. Noise levels are based upon traffic data provided by LLG (2020). Traffic levels for each roadway are included in Appendix B. Decibel levels are rounded to the nearest whole number. Significant and unavoidable impacts shown in **bold** and **shading**. See Appendix B for data sheets.

¹ Due to differences in topography between receptors and roadways along the impacted segments, required noise barrier height and design will vary. As previously stated, at a minimum, a noise reduction of 5 dBA would be achieved, and up to 30 dBA is typical. Table 17 assumes a 5 dBA reduction, or the minimum noise reduction required to mitigate impacts for the segment of Cuyamaca Street from El Nopal to Mast Boulevard (6 dBA reduction). Final barrier design may achieve higher reductions.

² Due to multiple driveway entrances, noise barriers are not considered feasible for schools on Magnolia Avenue.

On-Site Noise Compatibility

The following mitigation measures would minimize on-site exposure to noise generated from Fanita Parkway and Cuyamaca Street to achieve Santee General Plan compatibility. According to the Santee General Plan, conventional construction with closed windows and air conditioning is normally sufficient to achieve acceptable interior noise levels. As such, Mitigation Measure NOI-3 requires a detailed analysis to demonstrate that interior noise levels would be at or below 45 dBA Ldn, in accordance with federal and state guidance. Because the design of buildings is currently unknown, this level of analysis cannot be completed at this time. However, according to Caltrans, typical building construction with closed windows reduces interior exposure to exterior noise levels by approximately 30 dBA (Caltrans 2013a). Exterior noise levels are not predicted to exceed 67 dBA Ldn; therefore, it is reasonable to assume that an interior noise level of 45 dBA Ldn could be achieved and impacts would be reduced to a less than significant level with implementation of Mitigation Measure NOI-3.

- NOI-3: On-Site Ambient Noise Exposure. Prior to issuance of a building permit for any first-row Low Density Residential units or Active Adult units that would be located adjacent to Fanita Parkway and first-row multi-family residential units located adjacent to Cuyamaca Street in the Village Center, the applicant shall prepare an acoustical analysis ensuring that interior noise levels due to exterior noise sources would be at or below 45-A-weighted-decibel day-night average sound level. The analysis shall be submitted to the Director of Development Services for approval. One or a combination of the following measures shall be incorporated as necessary to ensure interior noise would be at or below 45-A-weighted-decibel day-night average sound level:
 - 1. Use non-noise-sensitive structures such as garages to shield noise-sensitive areas
 - 2. Orient bedrooms away from noise sources
 - 3. Limit opening and penetrations on portions of buildings impacted by noise
 - 4. Apply noise insulation to walls, roofs, doors, windows, and other penetrations
 - 5. Enclose patios or balconies using a clear material, such as glass
 - 6. Install dual-paned windows

For some units, it may be necessary for the windows to be able to remain closed to ensure that interior noise levels meet the interior standard of 45-A-weighted-decibel day-night average sound level. Consequently, a ventilation or air conditioning system shall be required for these units to provide a habitable interior environment with the windows closed.

Construction Noise Mitigation Measures

Temporary Construction Vehicle Noise

The proposed project would result in potentially significant temporary vehicle noise impacts on Fanita Parkway and Magnolia Avenue that would occur during project construction prior to mitigation. Table 18 provides a summary of the noise levels on the impacted roadways and during which scenarios these impacts would occur.

Roadway Segment		Scenario When Impact Would Occur	Maximum Noise Level at 50 Feet (dBA Ldn)
	On-Site Portion to Ganley Road	Near Term + Interim Operation + Building Construction (see Table 15)	66
Fanita Parkway	Ganley Road to Lake Canyon Road	Existing + Building Construction (see Table 13)	67
	Lake Canyon Road to Mast Boulevard	Existing + Building Construction (see Table 13)	68
Magnolia Avenue	Princess Joann Road to Woodglen Vista Drive	Near Term + Interim Operation + Building Construction (see Table 15)	67
	Woodglen Vista Drive to El Nopal	Near Term + Interim Operation + Building Construction (see Table 15)	69

Table 18. Interim Traffic Noise	Impacts	(Unmitigated)
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Sources: Hunsaker and Associates 2020; LLG 2020.

Notes: dBA = A-weighted decibel; Ldn = day-night average sound level

Mitigation Measure NOI-4 would limit the speed on construction access routes. However, a limit on the maximum number of truck trips on Fanita Parkway during this phase would also be required. The anticipated increase in noise levels on Fanita Parkway and Magnolia Avenue during interim operation and construction would primarily be a result of the increase in vendor truck trips during building construction. Mitigation Measure NOI-5 would prohibit medium- and heavy-duty truck trips on Magnolia Avenue and require all truck traffic to use Fanita Parkway and Cuyamaca Street only for site access. Vendor truck trips would be allowed but limited on Fanita Parkway. Worker vehicle trips would be allowable on all roadways. Diversion of truck trips from Fanita Parkway and Magnolia Avenue to Cuyamaca Street would not result in an impact to Cuyamaca Street because, as shown in Table 15, use of Cuyamaca Street for 100 percent of all construction traffic would not result in a significant increase in ambient noise levels.

NOI-4: Construction Access Road Speed Limitations. As a condition of approval for the proposed project, the applicant shall not seek to increase the posted speed limit on Fanita Parkway south of Ganley Road from the existing posted speed limit of 40 miles per hour to the post-project improvement design speed of 50 miles per hour until the building construction phase of Phase 1 is complete. The speed limit for construction-related traffic shall be stipulated in project construction documents,

including the grading plans and the contract with the construction contractor. Construction-related traffic shall not exceed existing posted speed limits.

NOI-5: Vendor Trip Route Limitations. During building construction activities, the construction contractor shall prohibit the use of Magnolia Avenue for medium- and heavy-duty truck trips. During building construction activities, all trucks shall access the site via Fanita Parkway and Cuyamaca Street only. Additionally, medium- and heavy-duty truck trips shall be limited on Fanita Parkway. Truck trips shall be limited to 170 one-way trips (85 two-way trips) on Fanita Parkway during Phase 1 building construction activities and to a maximum of 140 one-way trips (70 two-way trips) on Fanita Parkway during simultaneous building construction activities and project operation. These requirements shall be included in project construction contractor. Prior to issuance of a grading permit, temporary signage prohibiting proposed project truck access shall be installed at the Magnolia Avenue and Mast Boulevard intersection.

As shown in Table 19, implementation of Mitigation Measures NOI-4 and NOI-5 would reduce temporary impacts to Fanita Parkway and Magnolia Avenue to a less than significant level during building construction.

Roadway	Segment	Applicable Threshold (dBA Ldn)	Conditions without Construction (dBA Ldn)	Conditions Exceed Threshold Without Construction?	Mitigated Construction Noise Level (dBA Ldn)	Increase in Noise Level	Significant Impact?
	On-Site Portion to Ganley Road (NOI-5)	65	Does Not Exist	No	65	_	No
Fanita Parkway	Ganley Road to Lake Canyon Road (NOI-4 and NOI-5)	65	59	No	64	+5	No
	Lake Canyon Road to Mast Boulevard (NOI-4 and NOI-5)	65	61	No	65	+4	No
Magnolia Avenue	Princess Joann Road to Woodglen Vista Drive (NOI-5)	65	64	No	65	+1	No
	Woodglen Vista Drive to El Nopal (NOI-5)	65	68	Yes	68	0	No

Table 19. Mitigated Interim Traffic Noise Impacts

Notes: dBA = A-weighted decibel; Ldn = day-night average sound level

Noise levels are calculated at 50 feet from roadway centerline. Noise levels are based upon traffic data provided by LLG (2020) and LSA (2020). Traffic levels for each roadway are included in Appendix E. Decibel levels are rounded to the nearest whole number. See Appendix E for data sheets.

Temporary Construction Equipment Noise

Implementation of Mitigation Measures NOI-6 and NOI-7 would minimize temporary construction noise from operation of heavy equipment to a less than significant level.

- NOI-6: **Roadway Construction Notification.** In accordance with Section 5.04.090 of the Santee Municipal Code, the construction contractor shall provide written notification to any existing uses within 300 feet of roadway construction activities. The notification shall be provided no later than 10 days before the start of construction activities. The notice shall describe the nature of the construction activities, including the expected duration, and provide a point of contact to resolve noise complaints. If a complaint is received, construction noise shall be monitored by a qualified acoustical consultant at the nearest affected receptor for the duration of a normal day of construction. If the hourly average monitored noise level from construction exceeds a normal conversation level (65 A-weighted decibels) at the nearest sensitive receptor, or the ambient noise level at the receptor if the ambient noise level exceeds 65 A-weighted decibels, construction activities in the immediate area of the affected receptor shall cease. Construction shall not resume until activities can be adjusted or noise reduction measures are implemented to reduce noise at the affected receptor to below normal conversation levels (65 Aweighted decibels) or the ambient noise level at the receptor if the ambient noise level exceeds 65 A-weighted decibels. Measures to reduce noise shall include but not be limited to the following:
 - Stationary construction noise sources, such as temporary generators, shall be located as far from nearby noise-sensitive receptors as possible.
 - Trucks shall be prohibited from idling along streets serving the construction site where noise-sensitive residences are located.
 - Construction equipment shall be outfitted with properly maintained, manufacturer-approved or recommended sound abatement tools on air intakes, combustion exhausts, heat dissipation vents, and the interior surfaces of engine hoods and power train enclosures.
 - Construction laydown and vehicle staging areas shall be positioned (to the extent practical) as far from noise-sensitive land uses as feasible.
 - Simultaneous operation of construction equipment shall be limited, or construction time within an hour shall be limited, to reduce the average noise level.
 - Temporary noise barriers, such as noise blankets, shall be implemented around the perimeter of the construction area to minimize construction noise at affected receptors.

NOI-7: Nighttime Noise Sound Management Plan. The construction contractor shall be required to obtain authorization from the Director of Development Services for any construction activities that would occur between 7:00 p.m. and 7:00 a.m. As part of the authorization process, the construction contractor shall prepare a Sound Management Plan to be included in construction documents, including the grading plan and construction contract. The Sound Management Plan shall include all or a combination of the measures listed in Mitigation Measure NOI-6, as deemed necessary by a qualified acoustical engineer, to minimize noise at nearby receptors. In addition to the measures listed in Mitigation Measure NOI-6, construction activities that must take place between 7:00 p.m. and 7:00 a.m. that could generate high noise levels at residences shall be scheduled during times that would have the least impact on sensitive receptor locations, such as the evening hours between 7:00 p.m. and 10:00 p.m. rather than the nighttime hours between 10:00 p.m. and 7:00 a.m.

5.1.1.3 Significance After Mitigation

Future operational noise levels at the Special Use area would be compatible with existing land uses with implementation of the noise attenuation proposed in Mitigation Measure NOI-1. Implementation of Mitigation Measure NOI-2 would reduce vehicle noise impacts to certain receptors to less than significant but would not fully mitigate impacts to any entire road segment due to infeasibility. This impact would be potentially significant and unavoidable. On-site land use compatibility impacts would be reduced to a less than significant level with Mitigation Measure NOI-3. Mitigation Measures NOI-4 and NOI-5 would reduce noise levels from temporary construction traffic to a less than significant level. Mitigation Measures NOI-6 and NOI-7 would implement construction noise management programs to reduce construction equipment noise to a less than significant level.

5.1.1.4 Cumulative Impacts

The cumulative analysis below addresses the potential cumulative impacts that would result from noise generated by proposed land uses, permanent increases in vehicle traffic noise, and temporary construction impacts from other planned projects in the City in combination with the proposed project.

Operational Impacts

Approved or planned projects in the City are considered in the cumulative analysis for the proposed project. This analysis incorporates the cumulative projects assumed in the traffic impact analysis for the proposed project (LLG 2020). These approved or planned projects include multi-family and single-family residential development, commercial uses, light industrial use, and a church. Similar to the proposed project, residential land uses would generate nuisance noise that would not be considered a significant impact. However, some of the cumulative development projects would potentially include HVAC systems that would have the potential to result in significant impacts to NSLUs up to 275 feet from the source, as well as nuisance noise from parking lots and increased human activity. Industrial

uses may result in localized impacts from equipment operation. The nearest cumulative projects to the proposed development area are proposed at the existing northern terminus of the Summit Avenue public right-of-way, approximately 1,200 feet from the nearest on-site development area. Therefore, noise from operation of the proposed project is unlikely to combine with noise from operation of cumulative projects. A cumulative impact would not occur related to operational noise.

Permanent Increase in Ambient Noise Levels

A cumulative permanent ambient noise impact would occur if development associated with cumulative regional land use projects would result in an increase in ambient noise that would exceed the City's noise standards. Buildout of the proposed project, along with the cumulative projects and buildout of the Santee General Plan, would result in increases in traffic that would cumulatively increase traffic noise. An individual project would result in a cumulatively considerable contribution to a significant cumulative impact if the increase in noise attributable to the proposed project would cause a roadway to exceed the applicable noise standards or would be 3 dBA or higher on a roadway that would exceed the threshold without the proposed project. The potential noise impacts that would result from cumulative projects and regional growth are included in the Year 2035 scenario.

Table 20 compares Year 2035 traffic noise levels to existing conditions. The proposed project's contribution to cumulative noise impacts is based on the increase in traffic noise attributable to the proposed project under the Year 2035 scenario. Implementation of the proposed project would result in a cumulatively considerable noise level increase on three impacted roadways of Fanita Parkway. Specifically, the proposed project's contribution to noise level at a new roadway is enough to push the noise level over the applicable threshold compared to conditions without the proposed project. Therefore, implementation of the proposed project would result in cumulatively considerable contribution to a significant cumulative roadway noise impact.

Similar to the proposed project, implementation of Mitigation Measure NOI-2 would reduce noise levels to receptors on the western side of Fanita Parkway to below the normally acceptable noise level for sensitive receptors (65 dBA Ldn). Therefore, with implementation of Mitigation Measure NOI-2, the proposed project's contribution to a significant cumulative traffic noise impact would be reduced but not to below a cumulatively considerable level. This impact would be cumulatively considerable and unavoidable.

Roadway	Segment	Applicable Threshold (dBA Ldn)	Existing (No Project) (dBA Ldn)	Exceeds Threshold Without Project?	Year 2035 (dBA Ldn)	Year 2035 + Project (dBA Ldn)	Increase in Noise Level (Existing to Year 2035 + Project)	Significant Cumulative Impact?	Increase in Noise Level Attributable to Project (Year 2035 to Year 2035 + Project)	Cumulatively Considerable Contribution?
	SR-52 to West Hills Parkway	70	71	Yes	72	72	+1	No	0	No
Mast Boulevard	West Hills Parkway to Medina Drive	65	70	Yes	71	72	+2	No	+1	No
	Pebble Beach Drive to Fanita Parkway	65	70	Yes	71	72	+2	No	+1	No
Mission	SR-125 to Fanita Drive	70	77	Yes	78	78	+1	No	0	No
Gorge Road	Fanita Drive to Carlton Hills Boulevard	70	77	Yes	77	78	+1	No	+1	No
	On-Site Portion to Ganley Road	65	Does Not Exist	No	64	66	Does Not Exist	Yes	+2	Yes
Fanita	Ganley Road to Lake Canyon Road	65	59	No	65	70	+11	Yes	+5	Yes
Parkway	Lake Canyon Road to Mast Boulevard	65	61	No	66	70	+9	Yes	+4	Yes
	Mast Boulevard to Carlton Oaks Drive	65	58	No	61	62	+4	No	+1	No
Carlton Hills Boulevard	Carlton Oaks Drive to Mission Gorge Road	65	69	Yes	70	70	+1	No	0	No

Table 20. Cumulative Traffic Noise Impacts

Roadway	Segment	Applicable Threshold (dBA Ldn)	Existing (No Project) (dBA Ldn)	Exceeds Threshold Without Project?	Year 2035 (dBA Ldn)	Year 2035 + Project (dBA Ldn)	Increase in Noise Level (Existing to Year 2035 + Project)	Significant Cumulative Impact?	Increase in Noise Level Attributable to Project (Year 2035 to Year 2035 + Project)	Cumulatively Considerable Contribution?
	On-Site Portion to Magnolia Avenue	65	Does Not Exist	No	65	67	Does Not Exist	No ¹	+2	No
	Magnolia Avenue to Princess Joann Road	65	Does Not Exist	No	64	65	Does Not Exist	No	+1	No
	Princess Joann Road to Chaparral Drive	65	Does Not Exist	No	65	66	Does Not Exist	No ¹	+1	No
	Chaparral Drive to Woodglen Vista Drive	65	54	No	68	69	+15	No ¹	+1	No
Cuyamaca Street	Woodglen Vista Drive to El Nopal	65	62	No	70	70	+18	No ¹	0	No
	El Nopal to Mast Boulevard	65	65	No	71	71	+6	Yes	0	No ²
	Mast Boulevard to River Park Drive	65	68	Yes	70	70	+2	No	0	No
	River Park Drive to Town Center Parkway	65	70	Yes	71	71	+1	No	0	No
	Town Center Parkway to Mission Gorge Road	70	72	Yes	73	74	+2	No	+1	No

Table 20. Cumulative Traffic Noise Impacts

Roadway	Segment	Applicable Threshold (dBA Ldn)	Existing (No Project) (dBA Ldn)	Exceeds Threshold Without Project?	Year 2035 (dBA Ldn)	Year 2035 + Project (dBA Ldn)	Increase in Noise Level (Existing to Year 2035 + Project)	Significant Cumulative Impact?	Increase in Noise Level Attributable to Project (Year 2035 to Year 2035 + Project)	Cumulatively Considerable Contribution?
	Cuyamaca Street to Princess Joann Road	65	Does Not Exist	No	61	63	Does Not Exist	No	+2	No
Magnolia Avenue	Princess Joann Road to Woodglen Vista Drive	65	60	No	66	68	+8	Yes	+2	No ²
	Woodglen Vista Drive to El Nopal	65	66	Yes	68	69	+3	Yes	+1	No ²
	El Nopal to Mast Boulevard	65	68	Yes	71	71	+3	Yes	0	No ²
SR-52	Santo Road to Mast Boulevard	70	76	Yes	77	77	+1	No	0	No

Table 20. Cumulative Traffic Noise Impacts

Note: dBA = A-weighted decibel; Ldn = day-night average sound level; SR- = State Route

Unless otherwise noted, a cumulative impact would occur if vehicle traffic noise would result in an ambient noise level that exceeds the applicable threshold established in the Santee General Plan. If the normally acceptable standard would be exceeded in the existing condition, an increase of more than 3 dBA would be considered a cumulative impact. A cumulatively considerable contribution to a cumulative impact would be a 3 dBA or more increase attributable to the project.

The existing condition represents conditions in 2018. Noise levels are calculated at 50 feet from roadway centerline except SR-52 (100 feet from centerline due to roadway width). Noise levels are based upon traffic data provided by LLG (2020). Traffic levels for each roadway are included in the Appendix B. Decibel levels are rounded to the nearest whole number. Significant impacts shown in **bold** and **shading**. See Appendix B for data sheets.

¹ Distance or existing noise wall would reduce noise to an acceptable level.

² Cumulative projects would result in a significant increase in noise level on this segment compared to existing conditions. However, cumulative growth would cause the roadway to exceed the threshold without project implementation. The proposed project's contribution to the increase is less than 3 dBA and is, therefore, not cumulatively considerable.

Construction

Construction noise impacts are localized in nature because they are limited to the construction site where construction equipment is operating. As discussed previously, noise levels from onsite construction would attenuate to 75 dBA approximately 375 feet from the active construction area, and noise from off-site construction would attenuate to 75 dBA approximately 160 feet from the construction area. Due to the length of the construction period for the proposed project, it is likely that construction of multiple cumulative projects would occur simultaneously with the proposed project.

The nearest cumulative projects to the proposed area for on-site development are proposed at the existing northern terminus of the Summit Avenue public right-of-way, approximately 1,200 feet from the nearest on-site development area. Therefore, noise from construction of these projects is unlikely to combine with noise from construction of the proposed land uses.

In addition, a cumulative project (Santee View Estates) would potentially be within 160 feet of the proposed Cuyamaca Street extension. Similar to the proposed project, construction of this cumulative project would occur over a large area so that exposure of individual receptors to construction noise would vary depending on the location of construction activities during a certain day or phase. Construction of either project would only occur at the property line, within 160 feet of the other project, for a limited time. Due to the linear nature of the construction of Cuyamaca Street extension, it is unlikely that the two project's construction noise would combine simultaneously such that impacts from each project would affect the same receptors.

Additionally, cumulative projects and the proposed project would be subject to the construction limitations in the City's Noise Ordinance, which prohibits noise generated by construction activities between the hours of 7:00 p.m. and 7:00 a.m. and on Sundays and holidays without approval from the Director of Development Services. Similar to the proposed project, cumulative projects would be required to implement noise control best management practices in order to comply with the ordinance, such as those listed in Mitigation Measure NOI-7. Distance between projects and compliance with the City's Noise Ordinance would reduce impacts to a less than significant cumulative impact.

5.1.2 Threshold 2: Excessive Groundborne Vibration or Noise

5.1.2.1 Impact Analysis

The main concerns associated with groundborne vibration from this type of project are annoyance and damage; however, vibration-sensitive instruments and operations can be disrupted at much lower levels than would typically affect other uses. In extreme cases, the vibration can cause damage to buildings, particularly those that are old or otherwise fragile. Groundborne vibration occurring as part of the proposed project would result from construction equipment and blasting. Following construction, the proposed residential and commercial uses would not require heavy equipment anticipated to generate groundborne vibration. However, the use of tractors is anticipated to be required for the proposed Farm and is included in the analysis of heavy equipment below. The City uses the FTA groundborne vibration impact criteria, provided in Table 5, to determine whether vibration impacts would be significant.

Farm Equipment

Farm use would occur regularly in the limited Farm area; therefore, farm equipment use is subject to the frequent event FTA criteria. The project site is surrounded by residences where people normally sleep (Land Use Category 2). Therefore, operation of farm equipment would result in a significant impact if it would generate vibration levels greater than 72 VdB at the nearest existing residence.

FTA reference vibration levels are not available for the small tractor anticipated for Farm use. The typical vibration level for a small bulldozer provided in Table 21 is assumed to be representative of small tractor use. As shown in Table 21, small bulldozer use would not exceed 72 VdB at 25 feet from the source. There are no existing receptors within 25 feet of the proposed Farm area. Therefore, operational impacts from farm equipment would be less than significant.

Construction Equipment

Typical vibration levels for construction equipment required for the proposed project are provided in Table 21. Vibration levels for operation of a rock crusher are represented by drill operation because the FTA does not provide a specific reference noise level for rock crushing equipment. Construction vibration is subject to the infrequent event criteria because operation of vibrationgenerating equipment is anticipated to be intermittent throughout the day in the vicinity of an individual receptor. In accordance with the City's Noise Ordinance, construction would generally occur during the daytime and would not disturb sleep. However, residences may be occupied during daytime construction and construction may result in a nuisance to daily activities. Additionally, nighttime construction would generate vibration levels greater than 80 VdB at the nearest existing residence.

As shown in Table 21, vibration levels from all construction equipment would be reduced to 80 VdB or below beyond 75 feet from construction. The residences closest to the boundary of a village development area are approximately 850 feet east of the proposed Vineyard Village boundary near Oak Creek Drive. Therefore, due to distance to the nearest sensitive receptors, construction for on-site land development would not result in potentially significant vibration. However, some residences are located within 75 feet of the construction area for the extensions and off-site improvements to Fanita Parkway, Cuyamaca Street, and Magnolia Avenue, and dead-end roadway improvements at the southern boundary of the site. As shown in Table 21, at 45 feet from

construction, only operation of equipment equal to a vibratory roller would have the potential to exceed the significance criteria of 80 VdB at surrounding land uses during typical construction. Vibration levels would have the potential to exceed the applicable FTA criteria; therefore, construction activities that would require the use of a vibratory roller would have the potential to exceed the vibration impact criteria related to human response and result in a significant impact.

In addition to human annoyance, an impact related to architectural and structural damage to buildings would occur if existing buildings were affected by a PPV in excess of 0.2 in/sec. As shown in Table 21, vibration levels from vibratory construction equipment would be reduced to below 0.2 in/sec within 45 feet of the construction area. There are no existing structures within 45 feet of construction areas requiring use of vibratory equipment. Therefore, although construction would have the potential to result in significant nuisance impacts, as described previously, project construction equipment would not result in a significant impact related to structural damage.

Blasting

Blasting during construction would be infrequent and subject to the event criteria of 80 VdB at the nearest existing residence. As shown in Table 21, vibration levels from blasting would be reduced to 80 VdB or below beyond 235 feet from the blast area. No existing receptors are within 235 feet of potential blast areas. Due to distance to the nearest sensitive receptors, blasting would not exceed the applicable FTA criteria and would not result in a potentially significant vibration impact.

Construction Equipment	Approximate PPV/VdB at 25 Feet	Approximate PPV/VdB at 45 Feet ¹	Approximate PPV/VdB at 75 Feet ¹	Approximate PPV/VdB at 235 Feet ¹
Blasting for construction projects	0.400²/ 109	0.166/ 101	0.077/ 95	0.014/ 80
Large bulldozer	0.089/ 87	0.037/79	0.017/73	0.003/58
Caisson drilling	0.089/ 87	0.037/79	0.017/73	0.003/58
Loaded trucks	0.076/ 86	0.031/78	0.015/72	0.003/57
Small bulldozer	0.003/58	0.001/50	0.001/44	0.0001/29
Vibratory roller	0.21/ 94	0.087 /86	0.04/ 80	0.007/65

 Table 21. Vibration Source Levels for Construction Equipment

Source: FTA 2018.

Notes: PPV = peak particle velocity; VdB = vibration decibel

For impacts related to human annoyance, the threshold for construction equipment is 80 VdB at the nearest existing residence because use would be temporary and intermittent. Due to ongoing use, the threshold for operation of farm equipment is 72 VdB at the nearest existing residence. Vibration levels up to or that exceed the applicable threshold are in **bold**.

For impacts related to building damage, the threshold is 0.2 in/sec. Vibration levels up to or that exceed the threshold are in *italics*.

¹ Based on attenuation formulas provided by the FTA (2018)

² Source: FRA 2017.

Regarding structural damage, the details for individual project blasting operations cannot be known at this time, but would comply with applicable specifications prepared by the U.S. Bureau of Mines or Office of Surface Mining and Reclamation Enforcement. The estimated vibration from hard rock blasting for a major rail tunnel construction project has been used as a reference level for this analysis (FRA 2017). As shown in Table 21, vibration levels from blasting would be reduced to below 0.2 in/sec within 45 feet of the construction area. There are no existing structures within 45 feet of construction areas requiring blasting. Therefore, blasting would not result in a potentially significant impact related to structural damage.

5.1.2.2 Mitigation Measures

Implementation of Mitigation Measures NOI-8 and NOI-9, in addition to Mitigation Measures NOI-6 and NOI-7, would minimize temporary groundborne vibration impacts from construction activities at the nearby receptors.

- NOI-8: Vibration Best Management Practices. Prior to the commencement of construction activities that would involve use of a vibratory roller (or equivalent equipment) within 75 feet of a residence, the applicant shall retain a qualified acoustician to identify best management practices to be implemented by the construction contractor to reduce vibration levels to below 80 vibration decibels at the nearest residence. The best management practices shall be included in project construction documents, including the grading plan and contract with the construction contractor. Practices may include but are not limited to the following:
 - Use only properly maintained equipment with vibratory isolators
 - Operate equipment as far from sensitive receptors as possible
 - Use rubber-tired vehicles as opposed to tracked vehicles
- **NOI-9: Construction Vibration Notification.** The construction contractor shall provide written notification to receptors within 75 feet of construction activities at least 3 weeks prior to the start of any construction activities that would require the use of a vibratory roller or equivalent equipment. The notice would inform them of the estimated start date and duration of daytime vibration-generating construction activities. This notification shall include information warning about the potential for impacts related to vibration-sensitive equipment. The City of Santee shall provide a phone number for the affected receptors to call if they have vibration-sensitive equipment on their property. If a complaint is received, a vibration to below 80 vibration decibels at the nearest receptor. The vibration monitoring plan shall be prepared and administered by a qualified vibration consultant and submitted to the Director of Development Services for approval. The vibration

monitoring plan shall include the location of the vibration monitor, the vibration instrumentation used, a data acquisition and retention plan, and an exceedance notification and reporting procedures. The program shall include but not be limited to the following:

- Monitor vibration during construction activities with a seismograph or other instrument capable of measuring and recording displacement and frequency, particle velocity, or acceleration at the closest residence to the construction area
- Use equipment that includes dampeners or other modifications to reduce vibration
- Use alternative non-vibratory equipment where available
- Limit simultaneous operation of equipment

5.1.2.3 Significance After Mitigation

Implementation of Mitigation Measures NOI-6 through NOI-9 would reduce nuisance impacts from groundborne vibration impacts to a less than significant level. In addition, vibration impacts would be temporary and would cease following construction. Therefore, impacts related to groundborne vibration during construction would be less than significant after mitigation.

5.1.2.4 Cumulative Impacts

Similar to noise effects, vibration is a localized phenomenon and is progressively reduced as the distance from the source increases. Therefore, the area of projects that would be considered for the vibration cumulative analysis would be only those projects close to the project site. As discussed previously, vibration levels from typical construction would attenuate to below 80 VdB approximately 75 feet from the active construction area, and blasting from vibration would attenuate to 80 VdB approximately 235 feet from the construction area. Due to the length of the construction period for the proposed project, it is likely that construction of multiple cumulative projects would occur simultaneously with the proposed project.

The nearest cumulative projects are proposed at the existing northern terminus of the Summit Avenue public right-of-way, approximately 1,200 feet from the nearest on-site development area. Therefore, vibration from on-site construction is unlikely to combine with vibration from construction of the proposed project. A cumulative project would potentially be located within 235 feet of the proposed Cuyamaca Street extension: the Santee View Estates project proposed north of the existing terminus of Cuyamaca Street. Similar to the proposed project, construction of this cumulative project would occur over a large area so that exposure of individual receptors to construction vibration would vary depending on the location of construction activities during a certain day or phase. Construction would only occur within 235 feet of the proposed Cuyamaca Street extension for a limited time. Due to the linear nature of the construction of Cuyamaca Street, it is unlikely that construction noise from the two projects would combine simultaneously such that impacts from both projects would affect the same receptor. Distance between projects would reduce impacts to a less than significant cumulative impact. Once constructed, the proposed land use would not generate a significant source of vibration during normal operation. Therefore, a significant cumulative vibration impact would not occur.

5.1.3 Threshold 3: Aircraft Noise

5.1.3.1 Impact Analysis

MCAS Miramar is located adjacent to the west/northwestern boundary of the project site. The runways are located approximately 6 miles west of the project site. Additionally, Gillespie Field is located approximately 1.75 miles south of the project site. The project site is currently subject to periodic, audible overflights, particularly from MCAS Miramar. However, the proposed project site is not within the 60 dBA CNEL noise contour of either airport (SDCRAA 2010, 2011). Additionally, the proposed project does not include any components that would increase air traffic or require changes to existing air traffic patterns. As such, overflights are anticipated to continue to be audible at the project site; however, the proposed project is not anticipated to increase exposure to excessive noise levels from airport operation. Therefore, impacts would be less than significant.

5.1.3.2 Mitigation Measures

Impacts related to aircraft noise would be less than significant; therefore, no mitigation measures are required.

5.1.3.3 Significance After Mitigation

Impacts related to aircraft noise would be less than significant without mitigation.

5.1.3.4 Cumulative Impacts

No additional aviation uses are planned to be introduced in the immediate vicinity of the project site. In addition, the proposed project does not propose any new or air traffic patterns. No NSLUs would be exposed to excessive noise levels from aviation as a result of the proposed project. Impacts related to nuisance noise within noise contour areas are site specific and are not cumulative in nature. Therefore, a cumulative impact related to aircraft noise would not occur.

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Appendix A. Site Utilization Plan Statistical Summary

Planning Area ²	Area (Acres) ^ı	Target Dwelling Units ²	Target Density (Du/Ac)	Commercial Square Feet		
	RESIDE	INTIAL				
LOW DENSITY RESIDENTIAL (LE	DR)					
Orchard Village						
R-2	12.3	79	6			
R-3	10.7	53	5			
R-4	11.3	56	5			
R-5	18.5	80	4	N/A		
R-6	9.1	53	6			
R-7	9.9	50	5			
R-8	16.8	83	5			
LDR Subtotal - Orchard Village	88.6	454				
Vineyard Village						
R-9	9.5	48	5			
R-10	17.7	59	3			
R-11	6.0	33	6			
R-12	10.0	52	5			
R-13	12.8	43	3			
R-14	8.7	41	5			
R-15	6.4	26	4			
R-16	6.4	30	5			
R-17	15.8	52	3			
R-18	12.0	67	6	N/A		
R-19	16.2	67	4			
R-20	3.8	28	7			
R-21	6.8	70	10			
R-22	3.1	28	9			
R-23	2.4	20	8			
R-24	7.0	57	8	_		
R-25a	3.5	13	4			
R-25b	4.2	15	4			
LDR Subtotal - Vineyard Village	152.2	749				
LOW DENSITY RES. TOTAL	240.8	1,203				

Table 3.2: Site Utilization Plan Statistical Summary

Planning Area ²	Area (Acres)'	Target Dwelling Units ²	Target Density (Du/Ac)	Commercial Square Feet ²
	RESIDE	NTIAL		
MEDIUM DENSITY RESIDENTIAL (M	1DR)			
Orchard Village				
M-1	6.1	102	17	
M-2	8.9	111	13	N/A
M-3	6.5	79	12	
M-9	5.6	76	14	
MDR Subtotal - Orchard Village	27.2	368		
Vineyard Village				
M-4	8.5	106	13	
M-5	9.4	117	13	
M-6	6.8	85	13	N/A
M-7	10.3	129	13	
M-8	4.9	61	13	
MDR Subtotal - Vineyard Village	39.8	498		
MED. DENSITY RES. TOTAL	67.0	866		
ACTIVE ADULT (AA)				
Fanita Commons				
AC-1	31.0	445	14	N/A
ACTIVE ADULT TOTAL	31.0	445		

Table 3.2: Site Utilization Plan Statistical Summary (continued)

Planning Area ²	Area (Acres)'	Target Dwelling Units ²	Target Density (Du/Ac)	Commercial Square Feet		
	VILLAGE	CENTER				
VILLAGE CENTER (VC)						
Fanita Commons						
VC-1	2.6					
VC-2 ³	1.5					
VC-3	1.4					
VC-4	2.4					
VC-5	1.5					
VC-6	1.5					
VC-7	1.5					
VC-8	1.7	323	Up to 50	40,000		
VC-9	2.7	-				
VC-10	1.7					
VC-11	1.5	-				
VC-12	1.5					
VC-13	1.6	-				
VC-14	2.8					
VC-15	1.9	-				
VC Subtotal - Fanita Commons	27.7	323		40,000		
Orchard Village						
VC-16a	0.7					
VC-16b	0.7	22	Un 4 50	10.000		
VC-17a	0.6	33	Up to 50	10,000		
VC-17b	0.6]				
VC Subtotal - Orchard Village	2.6	33		10,000		
Vineyard Village						
VC-18	6.1	79	Up to 50	10,000		
VC Subtotal - Vineyard Village	6.1	79		10,000		
VILLAGE CENTER TOTAL	36.5	435		60,000		
RESIDENTIAL & VILLAGE CENTER TOTAL	375.3	2,949		60,000		

Table 3.2: Site Utilization Plan Statistical Summary (continued)

Planning Area ²	Area (Acres)'	Target Dwelling Units ²	Commercial Square Feet ²
	OTHER USE	S	
PARKS			
COMMUNITY PARK (CP)			
CP-1 (Active)	19.7	N/A	N/A
CP-1 (Passive)	11.5	IN/A	N/A
CP Total	31.2		
NEIGHBORHOOD PARK (NP)			
NP-1	4.6		
NP-2	3.3		
NP-3	3.2		
NP-4	2.6	N/A	N/A
NP-5	5.3		
NP-6	3.4		
NP-7	3.8		
NP-8	4.2		
NP Total	30.4		
MINI-PARK (MP)			
All MPs ⁴	16.4	N/A	N/A
MP Total	16.4		
PARK TOTAL	78.0		
SCHOOL (S) OVERLAY ⁶			
S-1 (School)	15.0	0	N/A
SCHOOL OVERLAY TOTAL	15.0		
SPECIAL USE (SU)	21.0	0	
SU-1	31.9	0	N/A
SPECIAL USE TOTAL	31.9		
OPEN SPACE (OS)			
OS (Open Space)	210.7		
OS-B (Open Space - Basin)	37.8		
OS-PS (Open Space - Pump Station)	2.5	N/A	N/A
OS-WT (Open Space - Water Tank)	5.0		
OPEN SPACE TOTAL	256.0		

Table 3.2: Site Utilization Plan Statistical Summary (continued)

Planning Area ²	Area (Acres)'	Target Dwelling Units ²	Commercial Squar Feet ²
	OTHER US	ES	
AGRICULTURE (A) OVERLAY ⁷			
Fanita Commons			
A-1	3.4		
A-2	5.7		
A-3	3.8	0	20,000
A-4	8.2		
A-5	6.3		
A Overlay Subtotal - Fanita Commons	27.3		20,000
Vineyard Village			
A-6	1.8		
A-7	5.3	0	0
A-8	2.0	0	0
A-9	1.8		
A Overlay Subtotal - Vineyard Village	10.9		0
AGRICULTURE OVERLAY TOTAL	38.2		20,000
HABITAT PRESERVE (HP)			
HP	1,650.4	N/A	N/A
HABITAT PRESERVE TOTAL	I,650.4		
ROADWAYS			
Major Roadways	56.4		
Neighborhood Roadways	136.8	N/A	N/A
ROADWAY TOTAL ⁵	193.3		
OTHER USES TOTAL	2,262.8		20,000
SPECIFIC PLAN TOTAL	2,638.1	2,9496	80,000

Notes:

1. Acreage reflects the rounding of numbers to the 1/10th of an acre and may vary slightly from the calculated total.

The planning areas in the Site Utilization Plan correspond to the neighborhoods and lots in the Tentative Map for Fanita Ranch. The transfer of
residential dwelling units and commercial square feet within the Specific Plan Area is permitted, subject to the provisions set forth in Section 10.7.1:
 Administrative Amendments (Minor Modifications).

3. VC-2 reserves a 1.5-acre fire station site.

4. There are 31 mini-parks on approximately 16.4 acres distributed throughout the Specific Plan Area, including the Village Green located in Fanita Commons.

5. Does not include approximately 28.6 acres of off-site roadway improvements.

6. The underlying land use for the S-1 planning area is MDR. If the reserved school site is not acquired for school use within 2 years of approval of the final map containing the S-1 planning area, the MDR land use may be implemented on the S-1 planning area and the maximum total number of units in the Specific Plan Area shall be 3,008 units - see *Section 3.2.5: School (S) Overlay* and *Section 10.7.1: Administrative Amendments (Minor Modifications)*.

7. The underlying land use for the A overlay planning areas is OS. If an A overlay planning area is not developed with agricultural related uses described in *Section 3.2.8: Agriculture (A) Overlay*, the OS land use shall be implemented on the A overlay planning areas.

Appendix B. FHWA Noise Prediction Model Results – Preferred Land Use Plan With School

TRAFFIC NOISE LEVELS AND NOISE CONTOURS

Project Number: Project Name:			osed Projec	t (with scho	ool)																					
ackground Information											•															
el Description: ce of Traffic Volumes: munity Noise Descriptor:	Linscott, I		se Prediction Greenspan, J CNEL:			7-108) with Ci	alifornia \	Vehicle Noise (CALVE	NO) Emission Levels.																	
med 24-Hour Traffic Distribution:			Evening		_	Distance is fr	om the c	ed within the roadway ri centerline of the roadwa																		
ADT Volumes m-Duty Trucks -Duty Trucks		77.70% 87.43% 89.10%	5.05%	9.60% 7.52% 8.06%		to the recept	or locatic	on.																		
ysis Condition oadway, Segment	Lanes	Median Width	ADT Volume	Design Speed (mph)	Alpha Factor	Vehicle Medium Trucks		Distance from Ldn at 50 Feet 70 Ldn	Centerline of Roadwa Distance to Contour 65 Ldn 60 Ldn	ay 55 Ldn		Volumes Eve Nigh	t MTd ⊦	fTd MTe	HTe M	Tn HTn	Ref. Energy A MT			Le IT Total A	MT HT	Ln Total A MT	T HT Total		CE TO CO	
Boulevard R-52 to West Hills Parkway, existing	4	25	26,440	40	0.5	3.0%	2.0%	71 62	134 288	620	0 50 20,544	0 0 1 3,358 2,5	0 38 693	0 0 471 40	0 15	0 0 60 43	67.4 76.3	81.2 1.4	69.5 64.0 6	37.2 72.2 66.	6 56.4 57.0	#### #### ## 67.4 55.6 54	4.6 57.9 61.0	0 62	0 134	
R-52 to West Hills Parkway, existing + project R-52 to West Hills Parkway, Near Term	4 4	25 25	33,010 30,730	40 40	0.5 0.5		2.0% 2.0%	72 72 72 69	155 334 148 318	719 685		9 4,192 3,1 7 3,903 2,9		588 50 548 47		74 53 69 50						68.4 56.5 55 68.1 56.2 55		72 69	155 148	
R-52 to West Hills Parkway, Near Term + project R-52 to West Hills Parkway, Year 2035	4	25 25	37,300 30,500	40 40	0.5		2.0% 2.0%	73 78 72 68	168 362 147 316	780 682		2 4,737 3,5 9 3,874 2,9		665 57 544 46		84 60 69 49						68.9 57.1 56 68.1 56.2 55		78 68	168 147	-
R-52 to West Hills Parkway, Year 2035 + project Boulevard	4	25	33,930	40	0.5	3.0%	2.0%	72 73	158 340	732	50 26,364 0	4,309 3,2		605 51 0 0	19 0	77 55 0 0						68.5 56.6 55		73	158 0	
est Hills Parkway to Medina Drive, existing est Hills Parkway to Medina Drive, existing + project	4	15 15	19,540 29,000	40 40	0.5 0.5		2.0% 2.0%	70 - 71 61	101 217 131 282	467 607		3 2,482 1,8 3 3,683 2,7		348 30 517 44		44 31 65 47						65.6 53.7 52 67.3 55.4 54		47 61	101 131	
lest Hills Parkway to Medina Drive, Near Term est Hills Parkway to Medina Drive, Near Term + project	4	15 15	22,962 32,422	40	0.5	3.0%	2.0%	70 52 72 65	112 241 141 304	520 654	50 17,841	2,916 2,2	04 602	409 35 578 49	13	52 37 73 52	67.4 76.3	81.2 0.9	68.4 62.9 6	6.0 71.1 65.	5 55.3 55.9	66.3 54.4 53 67.8 55.9 54	3.4 56.8 59.9	52 65	112	
ast Hills Parkway to Medina Drive, Year 2035 ast Hills Parkway to Medina Drive, Year 2035 + project	4	15	29,000 34,540	40 40	0.5	3.0%	2.0%	71 61 72 68	131 282 147 317	607 682	50 22,533		84 761	517 44 616 52	16	65 47 78 56	67.4 76.3	81.2 0.9	69.4 63.9 6	67.0 72.1 66.	5 56.3 56.9	67.3 55.4 54 68.1 56.2 55	4.4 57.8 60.9	61 68	131 147	
Soulevard bble Beach Drive to Fanita Parkway, existing	4	15	19.590	40	0.5		2.0%	70 -	101 217	467	0	0 0	0	0 0 349 30	0	0 0	##### #####	#### ####	#### #### #	### #### ###	# #### ####	##### ##### ## 65.6 53.7 52	## #### ####	0 47	0	
bble Beach Drive to Fanita Parkway, existing + project bble Beach Drive to Fanita Parkway, Near Term	4	15 15	29,050 21,361	40	0.5	3.0%	2.0%	71 61 70 -	131 282 107 230	608 495	50 22,572	2 3,689 2,7	89 762	518 44 381 32	17	66 47 48 34	67.4 76.3	81.2 0.9	69.4 63.9 6	67.1 72.1 66.	5 56.3 56.9	67.3 55.4 54 66.0 54.1 53	4.4 57.8 60.9	61 50	131 107	
bble Beach Drive to Fanita Parkway, Near Term + project bble Beach Drive to Fanita Parkway, Year 2035	4	15 15	30,821	40	0.5	3.0%	2.0%	72 63 71 61	136 294 131 282	632 607	50 23,948	3 3,914 2,9 3 3,683 2,7	59 808	549 47 517 44	18	70 50 65 47	67.4 76.3	81.2 0.9	69.7 64.1 6	67.3 72.4 66.	8 56.6 57.1	67.6 55.7 54 67.3 55.4 54	4.7 58.1 61.2	63 61	136	
abble Beach Drive to Fanita Parkway, Year 2035 + project	4	15	34,380	40	0.5		2.0%	72 68	147 316	680		3 4,366 3,3	00 902	613 52 0 0	20	78 55 0 0	67.4 76.3	81.2 0.9	70.1 64.6 6	67.8 72.8 67.	2 57.0 57.6	68.1 56.2 55	5.2 58.5 61.6	68	147	
R-125 to Fanita Drive, existing R-125 to Fanita Drive, existing + project	6	15 15	45,440 51,220	45 45	0.5 0.5		3.0% 3.0%	77 151 78 163	325 699 352 758	1,507 1.632	50 35,307		62 1,986	1,215 115 1.369 129	5 39	171 110 193 124	69.3 77.6	82.1 2.6	74.4 70.6 7	72.9 77.7 71.	6 63.0 62.8	72.6 62.8 61	1.1 63.7 67.4	151 163	325 352	6
R-125 to Fanita Drive, Near Term R-125 to Fanita Drive, Near Term R-125 to Fanita Drive, Near Term + project	6	15 15	48,026	45 45	0.5	5.0%	3.0% 3.0%	77 156 78 169	337 726 363 783	1,563		6 6,099 4,6	10 2,099	1,284 121 1,438 136	1 41	181 116 202 130	69.3 77.6	82.1 2.6	74.6 70.8 7	73.2 77.9 71.	8 63.2 63.0	72.9 63.1 61	1.3 63.9 67.7	156	337 363	7
k-125 to Fanita Drive, Near Term + project R-125 to Fanita Drive, Year 2035 R-125 to Fanita Drive. Year 2035 + project	6	15 15 15	53,806 49,200 52,630	45 45 45	0.5	5.0%	3.0% 3.0% 3.0%	78 169 78 159 78 166	363 783 342 737 358 771	1,686 1,589 1,662	50 38,228	3 6,248 4,7	23 2,151	1,438 138 1,315 124 1,407 133	4 42	202 130 185 119 198 127	69.3 77.6	82.1 2.6	74.7 70.9 7	73.3 78.0 71.	9 63.3 63.1	73.4 63.6 61 73.0 63.2 61 73.3 63.5 61	1.5 64.1 67.8	169 159 166	363 342 358	7
ion Gorge Road anita Drive to Carlton Hills Boulevard, existing	6	15	41,100	45	0.5	-	3.0%	78 100	304 654	1,002	0	0 0 5 5.220 3.9	0	1,407 133 0 0 1.099 104	0	198 127 0 0 155 99	##### #####	****	*****	**** ***** ***	# #### ####	73.3 63.5 61	## #### ####	0	0 304	6
anita Drive to Carlton Hills Boulevard, existing anita Drive to Carlton Hills Boulevard, existing + project anita Drive to Carlton Hills Boulevard. Near Term	6 6	15 15 15	41,100 47,670 43.029	45 45 45	0.5 0.5 0.5	5.0%	3.0% 3.0% 3.0%	77 141 77 156 77 145	304 654 335 722 313 674	1,409 1,556 1,453	50 37,040	5,220 3,9 6,054 4,5 5,465 4,1	76 2,084	1,099 104 1,274 120 1,150 109	0 41	155 99 179 115 162 104	69.3 77.6	82.1 2.6	74.6 70.8 7	73.2 77.9 71.	8 63.2 63.0	72.2 62.4 60 72.8 63.0 61 72.4 62.6 60	1.3 63.9 67.7	141 156 145	304 335 313	6 7 6
nita Drive to Cariton Hills Boulevard, Near Term nita Drive to Carlton Hills Boulevard, Near Term + project nita Drive to Carlton Hills Boulevard, Year 2035	6	15	43,029 49,599 48,700	45 45 45	0.5	5.0%	3.0% 3.0% 3.0%	78 160 77 158	313 674 344 741 340 732	1,453	50 38,538	3 6,299 4,7	62 2,168	1,150 105 1,326 125 1,302 123	5 42	186 120 183 118	69.3 77.6	82.1 2.6	74.7 70.9 7	73.3 78.0 72.	0 63.4 63.2	73.0 63.2 61 72.9 63.1 61	1.5 64.1 67.8	145 160 158	313 344 340	7
anita Drive to Cariton Hills Boulevard, Year 2035 anita Drive to Carlton Hills Boulevard, Year 2035 + project a Parkway	6	15	48,700 52,440	45 45	0.5		3.0%	78 166	340 732 357 769	1,578		0 0,185 4,6 <u>6,660 5,0</u> 0 0	34 2,292				69.3 77.6	82.1 2.6	75.0 71.2 7		2 63.6 63.4	73.3 63.4 61		158	340 357 0	7
roject Site to Ganley Drive, existing roject Site to Ganley Drive, existing + project	2	15 14	DNE 12.350	40 40	0.5		2.0% 2.0%	#VALUE! #VALUE! 66 -	#VALUE! #VALUE! # 62 134	#VALUE! 288	50 ######				## ###### ##		# 67.4 76.3	81.2 0.1	#### #### #	### #### ###	# #### ####		## #### #### 3.2 53.3 55.6	#VALUE! #V. 29		VALL
oject Site to Ganley Drive, existing + project oject Site to Ganley Drive, Near Term oject Site to Ganley Drive, Near Term + project	2	14 15 14	DNE 12,350	40 40 40	0.5	2.0%		#VALUE! #VALUE! 66 -			50 ######	# ###### #### 1.568 1.1			## ###### ##		# 67.4 76.3	81.2 0.1	#### #### #	**** ****	# #### ####		*** ***** ****			
oject Site to Ganley Drive, Year 2035 oject Site to Ganley Drive, Year 2035 oject Site to Ganley Drive, Year 2035 + project	2 2 2	14	7,380	40 40 40	0.5	2.0%	2.0%	64 -	44 95 62 134	205 288	50 5,734 50 9,596	937 70	8 129	132 7 220 12		19 20 11 12 19 20	67.4 76.3	81.2 0.1	62.8 55.4 6	65.2 59.	8 47.9 50.2	60.5 46.8 46 62.7 49.1 48	6.0 51.1 53.4	29 20 29	44 62	1
I Parkway Inve, Year 2035 + project I Parkway Inve, Year 2035 + project Inve, Year 2035 + project Inve, Year 2035 + project	2	0	2.610	40	0.5		2.0%	59 -	- 46	288	0 9,596 0 50 2.028	0 0	0	220 12 0 0 47 3	0	0 0	##### #####	#### ####	#### #### #	### #### ###	# #### ####	55.8 42.1 41	## #### ####	29 0 10	0 21	_
anley Drive to Lake Canyon Road, existing anley Drive to Lake Canyon Road, existing + project anley Drive to Lake Canyon Road, Near Term	2 3 2	0 14 0	2,610 14,960 2,782	40 50 40	0.5 0.5 0.5	2.0%	2.0% 2.0% 2.0%	59 - 69 46 60 -	- 46 99 214 - 48	99 462 104	50 2,028 50 11,624 50 2,162	1,900 1,4	36 262	47 3 267 15 50 3		4 4 22 24 4 4	71.1 78.8	83.0 0.4	68.9 60.3 6	64.6 70.7 66.	0 52.7 54.4	55.8 42.1 41 66.4 53.0 50 56.1 42.4 41	0.8 55.4 58.2	10 46 10	21 99 22	2
anley Drive to Lake Canyon Road, Near Term + project	2 3 2	0 14 0	2,782 15,132 9.920	40 50 40	0.5	2.0%	2.0% 2.0% 2.0%	60 - 70 47 65 -	- 48 100 216 52 112	104 465 242	50 11,758	353 26 3 1,922 1,4 1,260 95	53 265	50 3 270 15 177 10	9	4 4 23 24 15 16	71.1 78.8	83.0 0.4	68.9 60.3 6	64.6 70.7 66.	0 52.7 54.5	56.1 42.4 41 66.5 53.0 50 61.6 47.9 47	0.9 55.4 58.3	10 47 24	22 100 52	2
Inley Drive to Lake Canyon Road, Year 2035 Inley Drive to Lake Canyon Road, Year 2035 + project	2	0 14	9,920 15,130	40 50	0.5		2.0%	65 - 70 47	52 112 100 216	242 465	50 7,708 50 11,756 0		52 265	177 10 270 15 0 0		15 16 23 24 0 0	71.1 78.8	83.0 0.4	68.9 60.3 6	64.6 70.7 66.	0 52.7 54.5	61.6 47.9 47 66.5 53.0 50	0.9 55.4 58.3	24 47 0	52 100 0	2
ke Canyon Road to Mast Boulevard, existing ke Canyon Road to Mast Boulevard, existing + project	2	0 14	3,860 15,160	40 50	0.5 0.5		2.0% 2.0%	61 - 70 -	- 60 107 231	129 497	50 2,999 50 11.779	490 37	1 67	69 4 270 15	2	6 6 23 24	67.4 76.3	81.2 -0.1	59.7 52.4 5	57.4 62.2 56.	8 44.8 47.2	57.5 43.8 43 66.9 53.4 51	3.0 48.1 50.4	13 50	28 107	2
ke Canyon Road to Mast Boulevard, existing + project ke Canyon Road to Mast Boulevard, Near Term ke Canyon Road to Mast Boulevard, Near Term + project	2	0	4,158	40 50	0.5	2.0%	2.0% 2.0% 2.0%	61 - 70 -	- 63 109 234	497 135 504	50 11,779 50 3,231 50 12,011	528 39	9 73	270 15 74 4 275 16	2	23 24 6 7 23 25	67.4 76.3	81.2 -0.1	60.1 52.7 5	57.7 62.5 57.	2 45.2 47.5	57.8 44.1 43 67.0 53.5 51	3.3 48.4 50.7	14 50	29 109	2
e Canyon Road to Mast Boulevard, Year 2035	2	0	10,910	40	0.5	2.0%	2.0% 2.0% 2.0%	66 - 70 -	56 120 109 234	258 504	50 12,011 50 8,477 50 12,012	1,386 1,0	47 191	194 11 275 16	6	23 25 16 18 23 25	67.4 76.3	81.2 -0.1	64.3 56.9 6	61.9 66.7 61.	.3 49.4 51.7	62.0 48.3 47 67.0 53.5 51	7.5 52.6 54.9	26 50	56 109	
e Canyon Road to Mast Boulevard, Year 2035 + project Parkway st Boulevard to Carlton Oaks Drive, existing	4				0.5	-		-			0	0 0	0	0 0	0	0 0	##### #####	#### ####	*****	**** ***** ***	# #### ####	#### #### ##	## #### ####	0	0	
ast Boulevard to Carlton Oaks Drive, existing + project	2	0	3,330 6,750	35 35	0.5		1.0% 1.0%	58 - 61 -	- 39 - 62	84 134	50 5,245	857 64	8 118	30 3 60 7	1	5 3 10 5	65.1 74.8	80.0 -0.1	60.6 53.9 5	56.2 62.6 57.	6 46.4 46.1	55.1 41.7 41 58.2 44.8 44	4.5 47.0 50.4	8 13	18 29	
ast Boulevard to Carlton Oaks Drive, Near Term ast Boulevard to Carlton Oaks Drive, Near Term + project	2	0	3,713 7,133	35 35	0.5	2.0%	1.0%	59 - 62 -	- 42 - 65	90 139	50 2,885 50 5,542	906 68	5 125	33 4 64 7	2	6 3 11 6	65.1 74.8	80.0 -0.1	60.8 54.2 5	56.5 62.8 57.	8 46.6 46.3	55.6 42.2 41 58.4 45.1 44	4.7 47.2 50.6	9	19 30	
ast Boulevard to Carlton Oaks Drive, Year 2035 ast Boulevard to Carlton Oaks Drive, Year 2035 + project	2 2	0	6,000 7,380	35 35	0.5 0.5	2.0% 2.0%	1.0% 1.0%	61 - 62 -	- 58 - 66	124 143	50 4,662 50 5,734	937 70	8 129	53 6 66 7	2	9 5 11 6	65.1 74.8	80.0 -0.1	60.9 54.3 5	56.6 63.0 58.	0 46.8 46.5	57.7 44.3 44	4.9 47.4 50.7	12	27 31	
on Hills Boulevard Inton Oaks Drive to Mission Gorge Road, existing Inton Oaks Drive to Mission Gorge Road, existing + project	4	0	24,960 29,430	35 35	0.5 0.5		2.0% 2.0%	69 - 70 48	92 199 103 222	428 478	0 50 19,394 50 22.867	0 0 \$3,170 2,3 7 3.738 2.8	96 655	0 0 445 38 524 45		0 0 56 40 66 47	65.1 74.8	80.0 0.3	66.5 61.8 6	35.3 69.7 63.	7 54.2 55.2	#### #### ## 64.6 52.6 52 65.4 53.3 53	2.3 56.1 58.8	0 43 48	0 92 103	ļ
arlton Oaks Drive to Mission Gorge Road, existing + project arlton Oaks Drive to Mission Gorge Road, Near Term arlton Oaks Drive to Mission Gorge Road, Near Term + projec	4 4 ct 4	0	29,430 25,993 30,463	35 35 35	0.5 0.5 0.5	3.0%	2.0% 2.0% 2.0%	70 48 69 - 70 49	103 222 95 204 105 227	478 440 489	50 20,197	7 3,738 2,8 7 3,301 2,4 0 3,869 2,9	95 682	524 45 463 39 543 46	15	66 47 59 42 69 49	65.1 74.8	80.0 0.3	66.7 62.0 6	35.5 69.9 63.	8 54.4 55.3	65.4 53.3 53 64.8 52.8 52 65.5 53.4 53	2.5 56.3 59.0	48 44 49	103 95 105	
rlton Oaks Drive to Mission Gorge Road, Year 2035	4	0	30,463 32,800 33,820	35 35 35	0.5		2.0% 2.0% 2.0%	70 49 70 51 70 52	105 227 111 238 113 243	489 514 524	50 25,486	3,809 2,9. 3 4,166 3,1 3 4,295 3,2	49 860	584 50 603 51	19			80.0 0.3	67.7 63.0 6		8 55.4 56.4	65.8 53.8 53		49 51 52	105	
rlton Oaks Drive to Mission Gorge Road, Year 2035 + projec naca Street oject Site to Magnolia Avenue, existing	. 4	10	33,820 DNE	40	0.5	2.0%	2.0%	10 52	#VALUE! #VALUE! #		0	3 4,295 3,2 0 0 # ####### ####	0	0 0	0	76 55 0 0	#### ####	#### ####	##### ##### #	**** ****	# #### ####	#### #### ##		52 0 #\/ALLIEL #\/	0	
oject Site to Magnolia Avenue, existing + project oject Site to Magnolia Avenue, existing + project oject Site to Magnolia Avenue, Near Term	2	10 10	13,920 DNE	40 40 40	0.5	2.0%	2.0%	67 -	#VALUE! #VALUE! # 66 143 #VALUE! #VALUE! #	309	50 10,816	5 1,768 1,3	36 243	248 14	8	21 22	67.4 76.3	81.2 0.1	65.4 58.1 6	63.0 67.9 62.	5 50.5 52.9	63.2 49.5 48		31	66	1
oject Site to Magnolia Avenue, Near Term + project oject Site to Magnolia Avenue, Near Term + project oject Site to Magnolia Avenue, Year 2035	2	10 10	13,920	40 40	0.5	2.0%	2.0%	67 - 65 -	66 143 48 104	309 224	50 10,816	3 1,768 1,3 1.096 82	36 243	248 14 154 9	8	21 22	67.4 76.3	81.2 0.1	65.4 58.1 6	63.0 67.9 62.	5 50.5 52.9	63.2 49.5 48 61.1 47.4 46	3.7 53.8 56.0	31 22	66 48	1
oject Site to Magnolia Avenue, Year 2035 + project naca Street	2	10	13,920	40	0.5		2.0%	67 -	66 143	309		3 1,768 1,3 0 0	36 243	248 14 0 0	8	21 22 0 0	67.4 76.3	81.2 0.1	65.4 58.1 6	63.0 67.9 62.	5 50.5 52.9	63.2 49.5 48	3.7 53.8 56.0	31	40 66 0	1
Ignolia Avenue to Princess Joann Road, existing Ignolia Avenue to Princess Joann Road, existing + project	2	10 10	DNE 7,620	40 40	0.5 0.5		2.0% 2.0%	#VALUE! #VALUE! 64 -	#VALUE! #VALUE! # 44 96	#VALUE! 206		# ###### ####	***		## ###### ##		# 67.4 76.3	81.2 0.1	#### #### #	### #### ###	# #### ####		*** ***** ****	#VALUE! #V		VALU
agnolia Avenue to Princess Joann Road, Near Term agnolia Avenue to Princess Joann Road, Near Term agnolia Avenue to Princess Joann Road, Near Term + project	2	10	DNE	40 40 40	0.5	2.0%			#VALUE! #VALUE! #	#VALUE!	50 ######	# ###### ####			## ###### ##	<i></i>	# 67.4 76.3	81.2 0.1	#### #### #	***	# #### ####	*****	## #### ####			
gnolia Avenue to Princess Joann Road, Year 2035	2	10 10 10	7,620 6,800	40 40 40	0.5	2.0%	2.0%	64 - 65 -	41 89	206 191	50 5,921 50 5,284 50 6,939	864 65	3 119	121 7	4	10 11	67.4 76.3	81.2 0.1	62.3 55.0 5	59.9 64.8 59.	4 47.4 49.8	60.6 46.9 46 60.1 46.4 45	5.5 50.7 52.9	19	41	1
gnolia Avenue to Princess Joann Road, Year 2035 + project naca Street ncess Joann Road to Chaparral Drive, existing	2	10	8,930 DNE	40	0.5	-			49 107 #VALUE! #VALUE! #	229	0	0 0	0	159 9 0 0	0	13 14 0 0	#### ####	****	##### ##### #	****	# #### ####	61.3 47.6 46		23 0 #VALUEL #V	49 0	
ncess Joann Road to Chaparral Drive, existing ncess Joann Road to Chaparral Drive, existing + project ncess Joann Road to Chaparral Drive, Near Term	2 2 2	10 10 10	7,620 DNE	40 40 40	0.5 0.5 0.5	2.0%	2.0%	64 -	44 96 #VALUE! #VALUE! #	206	50 5,921	968 73	2 133	136 8	4	11 12		81.2 0.1	62.8 55.5 6	65.3 59.	9 47.9 50.3	60.6 46.9 46		21	44	
ncess Joann Road to Chaparral Drive, Near Term ncess Joann Road to Chaparral Drive, Near Term + project ncess Joann Road to Chaparral Drive, Year 2035		10 10 10	7,620 9,400	40 40 40	0.5	2.0%	2.0% 2.0% 2.0%	64 - 65 -	44 96 51 110	206 237	50 5,921	968 73 1,194 90	2 133	136 8 168 9		<u>11 12</u> 14 15	67.4 76.3	81.2 0.1	62.8 55.5 6	60.4 65.3 59.	9 47.9 50.3	60.6 46.9 46 61.5 47.8 46	6.0 51.2 53.4	21 24	44 51	VALU
ncess Joann Road to Chaparral Drive, Year 2035 Incess Joann Road to Chaparral Drive, Year 2035 + project	2	10	9,400 11,530	40 40	0.5		2.0%	66 -	51 110 59 126	237 272	50 7,304 50 8,959 0		07 202	205 12 0 0	5 7 0	14 15 17 19 0 0	67.4 76.3	81.2 0.1	64.6 57.3 6	62.2 67.1 61.	7 49.7 52.1	61.5 47.8 40 62.4 48.7 47	7.8 53.0 55.2	24 27 0	51 59 0	1
aparral Drive to Woodglen Vista Drive, existing aparral Drive to Woodglen Vista Drive, existing + project	2	40 16	670 8,290	35 50	0.5 0.5		2.0% 2.0%	54 - 68 -	77 167	359	50 521 50 6.441	85 64 1.053 79	18	12 1 148 13	ō	2 1 19 13	65.1 74.8	80.0 0.9	51.4 46.7 5	50.2 54.6 48.	5 39.1 40.0	49.5 37.4 37 64.5 52.8 50	7.2 41.0 43.7	4 36	9 77	1
aparral Drive to Woodglen Vista Drive, existing + project aparral Drive to Woodglen Vista Drive, Near Term aparral Drive to Woodglen Vista Drive, Near Term + project	2	40	683 8,303	35 50	0.5	3.0%	2.0% 2.0% 2.0%	54 - 68 -	77 167 77 167	359 - 359	50 6,441 50 531 50 6,451	87 66	5 18	148 13 12 1 148 13	0	19 13 2 1 19 13	65.1 74.8	80.0 0.9	51.5 46.7 5	50.3 54.7 48.	6 39.2 40.1	49.6 37.5 37 64.5 52.8 50	7.3 41.0 43.8	36 4 36	9 77	
aparral Drive to Woodglen Vista Drive, Near Term + project aparral Drive to Woodglen Vista Drive, Year 2035 aparral Drive to Woodglen Vista Drive, Year 2035 + project	- 4 4	16 16 16	9,400	50 50 50	0.5	3.0%	2.0% 2.0% 2.0%	68 - 69 -	84 181 96 208	359 390 447	50 6,451 50 7,304 50 8,959	1,194 90	2 247	148 13 168 14 205 17	5	21 15 26 19	71.1 78.8	83.0 0.9	67.3 60.5 6	63.1 69.3 64.	4 53.0 52.9	65.0 53.4 51 65.9 54.3 52	1.1 53.9 57.7	30 39 45	84 96	
partal Drive to woodgien vista Drive, Year 2035 + project aca Street odglen Vista Drive to El Nopal, existing	4	40	4.360	35	0.5	-	2.0%	62 -	- 68	146	50 8,959 0 50 3,388	0 0	0	205 17 0 0 78 7	0	26 19 0 0 10 7	#### ####	#### ####	#### #### #	### #### ###	# #### ####	57 6 45 6 45	## #### ####	45 0 15	96 0 31	
odglen Vista Drive to El Nopal, existing odglen Vista Drive to El Nopal, existing + project odglen Vista Drive to El Nopal. Near Term	4	40 16 40	4,360 11,980 4,472	35 50 35	0.5	3.0%	2.0% 2.0% 2.0%	62 - 69 - 62 -	- 68 99 213 - 69	146 459 149	50 3,388 50 9,308 50 3,475	1,521 1,1	50 314	78 7 213 18 80 7	7	10 7 27 19 10 7	71.1 78.8	83.0 0.9	68.4 61.6 6	64.1 70.4 65.	5 54.0 54.0	57.6 45.6 45 66.1 54.4 52 57.7 45.7 45	2.1 54.9 58.8	15 46 15	31 99 32	:
odgien Vista Drive to El Nopal, Near Term odgien Vista Drive to El Nopal, Near Term + project odgien Vista Drive to El Nopal, Year 2035	4	40 16 16	4,472 12,092 12.600	50 50	0.5	3.0%	2.0% 2.0% 2.0%	62 - 69 - 70 -	99 214 102 220	462		1,536 1,1	61 317	215 18 225 19	7	27 19 28 20	71.1 78.8	83.0 0.9	68.4 61.6 6	64.2 70.4 65.	5 54.1 54.0	66.1 54.5 52 66.3 54.6 52	2.2 54.9 58.8	46	99 102	
odgien Vista Drive to El Nopal, Year 2035 odglen Vista Drive to El Nopal, Year 2035 + project aca Street	4	16	12,600	50	0.5		2.0%	70 53	102 220	474 527		5 1,871 1,4 0 0	14 386	225 19 262 22 0 0	8	28 20 33 24 0 0	71.1 78.8	83.0 0.9	69.3 62.5 6	65.0 71.3 66.	4 54.9 54.9	67.0 55.3 53	3.0 55.8 59.7	47 53 0	102 113 0	1
aca street lopal to Mast Boulevard, existing lopal to Mast Boulevard, existing + project	3	30 16	8,860 16,480	35 50	0.5		2.0% 2.0%	65 - 71 57	- 110 122 263	238 567	50 6,884		1 232	158 13 294 25	5	20 14 37 27	65.1 74.8	80.0 1.0	62.7 58.0 6	61.5 65.9 59.	8 50.4 51.3	60.8 48.8 48 67.5 55.8 53	3.5 52.3 55.0	24 57	51 122	
lopal to Mast Boulevard, existing + project lopal to Mast Boulevard, Near Term lopal to Mast Boulevard. Near Term + project	* 3 1	30 16	9,173 16,793	35 50	0.5	3.0%	2.0% 2.0% 2.0%	71 57 65 - 71 57	- 113 124 267	244 575	50 7,127	5 2,093 1,5 1,165 88 3 2,133 1.6	1 241	294 25 163 14 299 25	5	37 27 21 15 38 27	65.1 74.8	80.0 1.0	62.9 58.1 6	61.7 66.1 60.	0 50.5 51.5	67.5 55.8 53 61.0 48.9 48 67.5 55.9 53	3.7 52.4 55.1	57 24 57	52 124	-
opal to Mast Boulevard, Near Term + project opal to Mast Boulevard, Year 2035 opal to Mast Boulevard, Year 2035 + project	- 4 4	16 16 16	16,500	50 50 50	0.5	3.0%	2.0% 2.0% 2.0%	71 57 71 57 71 62	124 267 122 264 133 286	5/5 568 616	50 12,821	3 2,133 1,6 1 2,096 1,5 3 2,366 1,7	84 433	299 25 294 25 332 28	9	37 27	71.1 78.8	83.0 0.9	69.8 63.0 6	5.5 71.8 66.	9 55.4 55.4	67.5 55.8 53 67.5 56.3 54	3.5 56.3 60.1	57 57 62	124 122 133	
opal to Mast Boulevard, Year 2035 + project aca Street t Boulevard to River Park Drive, existing	4	16	18,630	35	0.5	-	2.0%	68 -	85 184	395	0	0 0 9 2,489 1,8	0	332 28 0 0 349 30	0	42 30 0 0 44 32	##### #####	#### ####	##### ##### #	**** ***** ****	# #### ####	68.0 56.3 54 #### #### ## 64.1 52.1 51	## #### ####	62 0 40	133 0 85	
t Boulevard to River Park Drive, existing t Boulevard to River Park Drive, existing + project t Boulevard to River Park Drive, Near Term	4 4 4	15 15 15	19,600 25,380 20,527	35 35 35	0.5 0.5 0.5	3.0%	2.0% 2.0% 2.0%	68 - 70 - 69 -	85 184 101 218 88 189	395 470 408	50 19,720	9 2,489 1,8 0 3,223 2,4 9 2,607 1,9	36 666	349 30 452 38 366 31	14	44 32 57 41 46 33	65.1 74.8	80.0 0.9	67.1 62.4 6	35.9 70.3 64.	3 54.8 55.8	64.1 52.1 51 65.2 53.2 52 64.3 52.3 52	2.9 56.7 59.4	40 47 41	85 101 88	-
Boulevard to River Park Drive, Near Term Boulevard to River Park Drive, Near Term + project Boulevard to River Park Drive. Year 2035	4 4 4	15 15 15	20,527 26,307 26.600	35 35 35	0.5	3.0%	2.0% 2.0% 2.0%	70 -	88 189 104 223 104 225	408 481 485	50 20,441		25 690	366 31 469 40 474 40	15	46 33 59 42 60 43	65.1 74.8	80.0 0.9	67.3 62.6 6	6.1 70.5 64.	4 55.0 55.9	64.3 52.3 52 65.4 53.3 53 65.4 53.4 53	3.1 56.9 59.6	41 48 48	88 104 104	
t Boulevard to River Park Drive, Year 2035 + project	4 4	15 15	26,600 27,510	35 35	0.5 0.5		2.0% 2.0%	70 - 70 -	104 225 107 230	485 496	50 21,375	5 3,494 2,6	41 722	490 42		60 43 62 44	65.1 74.8	80.0 0.9	67.5 62.7 6	6.3 70.7 64.	6 55.2 56.1	65.4 53.4 53 65.6 53.5 53	3.3 57.0 59.8	48 50	107	2
naca Street er Park Drive to Town Center Parkway, existing an Park Drive to Town Center Parkway, existing	4	15	26,690	35	0.5		2.0%	70 - 74 55	105 225	486		0 0 3 3,390 2,5	62 700	0 0 476 40		0 0 60 43 72 52	65.1 74.8	80.0 0.9	67.4 62.6 6	6.2 70.6 64.	5 55.0 56.0	65.5 53.4 53	3.2 56.9 59.6	0 49	0 105	2
er Park Drive to Town Center Parkway, existing + project er Park Drive to Town Center Parkway, Near Term	4	15 15	32,210 28,084	35 35	0.5	3.0%	2.0%	71 55 70 - 74 57	119 256 108 233	551 503	50 21,821	7 4,091 3,09 1 3,567 2,69	96 737	574 49 500 43	16	73 52 63 45 76 54	65.1 74.8	80.0 0.9	67.6 62.8 6	6.4 70.8 64.	7 55.3 56.2	66.3 54.2 54 65.7 53.6 53	3.4 57.1 59.8	55 50	119 108	1
er Park Drive to Town Center Parkway, Near Term + project er Park Drive to Town Center Parkway, Year 2035	4	15	33,604 31,700	35 35	0.5	3.0%	2.0% 2.0%	71 57 71 54	122 263 117 253	566 545	50 24,631	4,268 3,2 4,026 3,0	43 831	599 51 565 48	18	76 54 72 51	65.1 74.8	80.0 0.9	68.1 63.4 6	6.9 71.3 65.	2 55.8 56.7	66.5 54.4 54 66.2 54.1 53	3.9 57.7 60.4	57 54	122	
er Park Drive to Town Center Parkway, Year 2035 + project aca Street		15	32,670	35	0.5		2.0%	71 56	120 258	556	0	5 4,149 3,13 0 0	0	582 49 0 0	0	74 53 0 0	#### ####	##### #####	*****	**** ***** ***	# #### ####	66.3 54.3 54 #### #### ##	*** ***** *****	56 0	120 0	
vn Center Parkway to Mission Gorge Road, existing vn Center Parkway to Mission Gorge Road, existing + project	6 ct 6	15 15	21,850 26,840	35 35	0.5 0.5	5.0%	3.0% 3.0%	72 68 73 78	147 317 169 364	684 784	50 20,855	7 2,775 2,0 5 3,409 2,5	77 1,173	584 55 717 68	23	82 53 101 65	65.1 74.8	80.0 2.6	68.9 66.6 6	9.7 73.3 66.	2 59.0 59.5	66.8 56.5 56 67.6 57.4 57	7.1 60.4 63.4	68 78	147 169	3
vn Center Parkway to Mission Gorge Road, Near Term vn Center Parkway to Mission Gorge Road, Near Term + pro	6	15 15	24,245 29,235	35 35	0.5 0.5	5.0% 5.0%	3.0% 3.0%	72 73 73 83	158 340 179 385	733 830		3 3,079 2,3 3 3,713 2,8		648 61 781 74		91 59 110 71	65.1 74.8	80.0 2.6	68.5 66.1 6	9.2 72.9 65.	7 58.5 59.0	67.2 56.9 56 68.0 57.8 57	6.7 60.0 62.9	73 83	158 179	3
n Center Parkway to Mission Gorge Road, Year 2035 n Center Parkway to Mission Gorge Road, Year 2035 + pro	6	15 15	30,100 31,640	35 35	0.5 0.5	5.0%	3.0% 3.0%	73 85 74 88	182 393 189 406	846 875	50 23,388	3 3,823 2,8 4 4,018 3,0	90 1,316	805 76 846 80	26	113 73 119 77	65.1 74.8	80.0 2.6	69.4 67.1 7	70.2 73.8 66.	7 59.5 60.0	68.1 57.9 57 68.4 58.1 57	7.6 60.9 63.9	85 88	182 189	3
lia Avenue amaca Street to Princess Joann Road, existing	2	12	DNE	35	0.5			-	#VALUE! #VALUE! #		0	0 0	0	0 0	0	0 0	##### #####	#### ####	#### #### #	### #### ###	# #### ####	#### #### ##		0	0	
amaca Street to Princess Joann Road, existing + project amaca Street to Princess Joann Road, Near Term	2	12	6,310 DNE	35 35	0.5 0.5	3.0%	2.0%	63 -	- 76 #VALUE! #VALUE! #	165	50 4,903	801 60	6 166	112 10	4	14 10	65.1 74.8	80.0 0.1	60.3 55.6 5	59.1 63.5 57.	4 48.0 48.9	58.4 46.3 46		16	35	
amaca Street to Princess Joann Road, Near Term + project amaca Street to Princess Joann Road, Year 2035	t 2 2	12	6,310 4,300	35 35	0.5	3.0%	2.0%	63 - 61 -	- 76 - 59	165		801 60	6 166		4		65.1 74.8	80.0 0.1	60.3 55.6 5	59.1 63.5 57.	4 48.0 48.9	58.4 46.3 46 56.7 44.7 44	5.1 49.9 52.6	16	35	
yamaca Street to Princess Joann Road, Year 2035 + project olia Avenue	t 2	12	7,470	35	0.5		2.0%	63 -	40 85	184	50 5,804 0		7 196	133 11 0 0	4	17 12	65.1 74.8	80.0 0.1	61.0 56.3 5	59.8 64.2 58.	2 48.7 49.7	59.1 47.1 46	6.8 50.6 53.3	18	40	8
iolia Avenue incess Joann Road to Woodglen Vista Drive, existing	4	15	2.020	40	0.5	3.0%	2.0%	60 -		103		257 19		36 3	1	5 3						55.7 43.9 42		10	22	4

River Park Drive to Town Center Parkway, Year 2035	4	15	31,700	35	0.5	3.0%	2.0%	71	54	117	253	545	50		4,026 3,043			48	18	72	51	65.1	74.8 80	0.0 0.9	68.1	63.4 66	.9 71.3	65.2 55	56.7 8.ذ	66.2 54	4.1 53.9 5	7.7 60.4	54	117	253	545
River Park Drive to Town Center Parkway, Year 2035 + project	4	15	32,670	35	0.5	3.0%	2.0%	71	56	120	258	556	50	25,385	4,149 3,136	857	582	49	19	74	53	65.1	74.8 80	0.0 0.9	68.2	63.5 67	.0 71.4	65.4 55	j.9 56.9	66.3 54	4.3 54.0 5	7.8 60.5	56	120	258	556
Cuyamaca Street														0	0 0	0	0	0	0	0	0	####	#### ##	## ####	* ####	¥### ###	######	##### ##	;## ####	* ##### ##	## #### ##	### ####	0	0	0	0
Town Center Parkway to Mission Gorge Road, existing	6	15	21,850	35	0.5	5.0%	3.0%	72	68	147	317	684	50	16,977	2,775 2,098	3 955	584	55	19	82	53	65.1	74.8 80	0.0 2.6	68.0	65.7 68	.8 72.5	65.3 58	3.1 58.6	66.8 56	3.5 56.2 5	/9.5 62.5	68	147	317	684
Town Center Parkway to Mission Gorge Road, existing + project	6	15	26,840	35	0.5	5.0%	3.0%	73	78	169	364	784	50	20,855	3,409 2,57	7 1,17	3 717	68	23	101	65	65.1	74.8 80	0.0 2.6	68.9	66.6 69	.7 73.3	66.2 59	J.0 59.5	67.6 57	7.4 57.1 6	.0.4 63.4	78	169	364	784
Town Center Parkway to Mission Gorge Road, Near Term	6	15	24,245	35	0.5	5.0%	3.0%	72	73	158	340	733	50	18,838	3,079 2,328	3 1,06	0 648	61	21	91	59	65.1	74.8 80	0.0 2.6	68.5	66.1 69	.2 72.9	65.7 58	3.5 59.0	67.2 56	6.9 56.7 6	0.0 62.9	73	158	340	733
Town Center Parkway to Mission Gorge Road, Near Term + proj	6	15	29,235	35	0.5	5.0%	3.0%	73	83	179	385	830	50	22,716	3,713 2,807	7 1,27	8 781	74	25	110	71	65.1	74.8 80	0.0 2.6	69.3	66.9 70	.0 73.7	66.5 59	2.4 59.9	68.0 57	7.8 57.5 6	0.8 63.7	83	179	385	830
Town Center Parkway to Mission Gorge Road, Year 2035	6	15	30,100	35	0.5	5.0%	3.0%	73	85	182	393	846	50	23,388	3,823 2,890	1,31	6 805	76	26	113	73	65.1	74.8 80	0.0 2.6	69.4	67.1 70	2 73.8	66.7 59	∂.5 60.0	68.1 57	7.9 57.6 6	0.9 63.9	85	182	393	846
Town Center Parkway to Mission Gorge Road, Year 2035 + proje	6	15	31,640	35	0.5	5.0%	3.0%	74	88	189	406	875	50	24,584	4,018 3,03	7 1,38	3 846	80	27	119	77	65.1	74.8 80	0.0 2.6	69.7	67.3 70	.4 74.1	66.9 59	3.7 60.2	68.4 58	3.1 57.8 6	1.1 64.1	88	189	406	875
Magnolia Avenue														0	0 0	0	0	0	0	0	0	####	#### ##	## ####	* ####	¥### ###	######	##### ##	;## ####	* ##### ##	## #### ##	### ####	0	0	0	0
Cuyamaca Street to Princess Joann Road, existing	2	12	DNE	35	0.5	3.0%	2.0%	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	50	####### #	****	#####	4# ######	######	######	# ######	* *****	# 65.1	74.8 80	0.0 0.1	####	*### ###	#####	#### ##	.## ####	##### ##	## #### #1	### #### #VA	ALUE! #V/		ALUE! #V	
Cuyamaca Street to Princess Joann Road, existing + project	2	12	6,310	35	0.5	3.0%	2.0%	63	-	-	76	165	50	4,903	801 606	166	112	10	4	14	10	65.1	74.8 80	0.0 0.1	60.3	55.6 59	.1 63.5	57.4 48	3.0 48.9	58.4 46	5.3 46.1 4	9.9 52.6	16	35	76	165
Cuyamaca Street to Princess Joann Road, Near Term	2	12	DNE	35	0.5	3.0%	2.0%	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	50	###### #	****	#####	4# ######	######	######	# ######	* #####	# 65.1	74.8 80	0.0 0.1	####	¥### ###	######	#### ##	## ####	##### ##	## #### #1	### #### #VA	ALUE! #V/	LUE! #V.	ALUE! #V	ALUE!
Cuyamaca Street to Princess Joann Road, Near Term + project	2	12	6,310	35	0.5	3.0%	2.0%	63	-	-	76	165	50		801 606		112	10	4	14	10	65.1	74.8 80	0.0 0.1	60.3	55.6 59	.1 63.5	57.4 48	3.0 48.9	58.4 46	5.3 46.1 4	9.9 52.6	16	35	76	165
Cuyamaca Street to Princess Joann Road, Year 2035	2	12	4,300	35	0.5	3.0%	2.0%	61	-	-	59	127	50	3,341	546 413	113	77	7	2	10	7	65.1	74.8 80	0.0 0.1	58.6	53.9 57	.4 61.8	55.8 46	3.3 47.3	56.7 44	4.7 44.4 4	8.2 50.9	13	27	59	127
Cuyamaca Street to Princess Joann Road, Year 2035 + project	2	12	7,470	35	0.5	3.0%	2.0%	63	-	40	85	184	50	5,804	949 717	196	133	11	4	17	12	65.1	74.8 80	0.0 0.1	61.0	56.3 59	.8 64.2	58.2 48	8.7 49.7	59.1 47	7.1 46.8 5	0.6 53.3	18	40	85	184
Magnolia Avenue														0	0 0	0	0	0	0	0	0	####	#### ##	## ####	* ####	¥### ###	######	#### ##		##### ##	## #### ##	### ####	0	0	0	0
Princess Joann Road to Woodglen Vista Drive, existing	4	15	2,020	40	0.5	3.0%	2.0%	60	-	-	-	103	50		257 194	53	36	3	1	5	3	67.4	76.3 81	.2 0.9	57.8	52.3 55	.5 60.5	54.9 44	4.7 45.3	55.7 43	3.9 42.9 4	6.2 49.3	10	22	48	103
Princess Joann Road to Woodglen Vista Drive, existing + project	4	15	8,330	40	0.5	3.0%	2.0%	66	-	57	123	264	50	6,472	1,058 800	218	148	13	5	19	13	67.4	76.3 81	.2 0.9	64.0	58.5 61	.6 66.7	61.1 50	J.9 51.5	61.9 50	0.0 49.0 5	2.4 55.5	26	57	123	264
Princess Joann Road to Woodglen Vista Drive, Near Term	4	15	2,204	40	0.5	3.0%	2.0%	60	-	-	-	109	50	1,713	280 212	58	39	3	1	5	4	67.4	76.3 81	.2 0.9	58.2	52.7 55	.9 60.9	55.3 45	<i>5.</i> 1 45.7	56.1 44	4.2 43.2 4	6.6 49.7	11	23	51	109
Princess Joann Road to Woodglen Vista Drive, Near Term + proj	4	15	8,514	40	0.5	3.0%	2.0%	66	-	58	125	268	50	6,615	1,081 817	223	152	13	5	19	14	67.4	76.3 81	.2 0.9	64.1	58.6 61	.7 66.8	61.2 51	1.0 51.6	62.0 50	0.1 49.1 5	2.5 55.6	27	58	125	268
Princess Joann Road to Woodglen Vista Drive, Year 2035	4	15	9,500	40	0.5	3.0%	2.0%	66	-	62	134	289	50	7,382	1,207 912	249	169	14	5	21	15	67.4	76.3 81	.2 0.9	64.5	59.0 62	.2 67.2	61.7 51	1.4 52.0	62.5 50	0.6 49.6 5	3.0 56.1	29	62	134	289
Princess Joann Road to Woodglen Vista Drive, Year 2035 + proj	4	15	12,670	40	0.5	3.0%	2.0%	68	-	75	162	350	50	9,845	1,609 1,210	3 332	226	19	7	29	20	67.4	76.3 81	.2 0.9	65.8	60.3 63	.5 68.5	62.9 52	2.7 53.3	63.7 51	1.8 50.8 5	4.2 57.3	35	75	162	350
Magnolia Avenue														0	0 0	0	0	0	0	0	0	####	#### ##	## ####	* ####	¥### ###	######	##### ##	;## ####	* ##### ##	## #### ##	### ####	0	0	0	0
Woodglen Vista Drive to El Nopal, existing	4	15	9,030	40	0.5	3.0%	2.0%	66	-	60	129	279	50	7,016	1,147 867	237	161	14	5	20	15	67.4	76.3 81	.2 0.9	64.3	58.8 62	.0 67.0	61.4 51	1.2 51.8	62.2 50	0.4 49.4 5	2.7 55.8	28	60	129	279
Woodglen Vista Drive to El Nopal, existing + project	4	15	15,340	40	0.5	3.0%	2.0%	69	-	86	184	397	50	11,919	1,948 1,473	3 402	273	23	9	35	25	67.4	76.3 81	.2 0.9	66.6	61.1 64	.3 69.3	63.7 53	3.5 54.1	64.5 52	2.7 51.7 5	5.0 58.1	40	86	184	397
Woodglen Vista Drive to El Nopal, Near Term	4	15	9,415	40	0.5	3.0%	2.0%	66	-	62	133	287	50	7,315	1,196 904	247	168	14	5	21	15	67.4	76.3 81	.2 0.9	64.5	59.0 62	2 67.2	61.6 51	1.4 52.0	62.4 50	0.5 49.5 5	2.9 56.0	29	62	133	287
Woodglen Vista Drive to El Nopal, Near Term + project	4	15	15,725	40	0.5	3.0%	2.0%	69	-	87	187	404	50	12,218	1,997 1,510	0 412	280	24	9	35	25	67.4	76.3 81	.2 0.9	66.7	61.2 64	.4 69.4	63.8 53	3.6 54.2	64.7 52	2.8 51.8 5	5.2 58.2	40	87	187	404
Woodglen Vista Drive to El Nopal, Year 2035	4	15	13,600	40	0.5	3.0%	2.0%	68	-	79	170	367	50	10,567	1,727 1,300	3 357	242	21	8	31	22	67.4	76.3 81	1.2 0.9	66.1	60.6 63	.8 68.8	63.2 53	3.0 53.6	64.0 52	2.1 51.1 5	4.5 57.6	37	79	170	367
Woodglen Vista Drive to El Nopal, Year 2035 + project	4	15	16,770	40	0.5	3.0%	2.0%	69	-	91	196	421	50	13,030	2,130 1,610	440	299	25	10	38	27	67.4	76.3 81	.2 0.9	67.0	61.5 64	.7 69.7	64.1 53	3.9 54.5	64.9 53	3.1 52.0 5	5.4 58.5	42	91	196	421
Magnolia Avenue						-								0	0 0	0	0	0	0	0	0	####	#### ##	## ####	* ####	¥### ###	######	#### ##		##### ##	## #### ##	### ####	0	0	0	0
El Nopal to Mast Boulevard, existing	4	15	13,690	40	0.5	3.0%	2.0%	68	-	79	171	368	50	10,637	1,739 1,314	4 359	244	21	8	31	22	67.4	76.3 81	.2 0.9	66.1	60.6 63	.8 68.8	63.2 53	3.0 53.6	64.1 52	2.2 51.2 5	4.6 57.6	37	79	171	368
El Nopal to Mast Boulevard, existing + project	4	15	17,370	40	0.5	3.0%	2.0%	69	-	93	200	431	50	13,496	2,206 1,668	3 456	310	26	10	39	28	67.4	76.3 81	.2 0.9	67.2	61.7 64	.8 69.9	64.3 54	4.1 54.7	65.1 53	3.2 52.2 5	5.6 58.7	43	93	200	431
El Nopal to Mast Boulevard, Near Term	4	15	14,291	40	0.5	3.0%	2.0%	68	-	82	176	379	50	11,104	1,815 1,372	2 375	255	22	8	32	23	67.4	76.3 81	.2 0.9	66.3	60.8 64	.0 69.0	63.4 53	3.2 53.8	64.2 52	2.4 51.4 5	4.7 57.8	38	82	176	379
El Nopal to Mast Boulevard, Near Term + project	4	15	17,971	40	0.5	3.0%	2.0%	69	-	95	205	441	50	13,963	2,282 1,72	5 471	320	27	10	41	29	67.4	76.3 81	.2 0.9	67.3	61.8 65	.0 70.0	64.4 54	4.2 54.8	65.2 53	3.4 52.3 5	5.7 58.8	44	95	205	441
El Nopal to Mast Boulevard, Year 2035	4	15	27,300	40	0.5	3.0%	2.0%	71	58	126	271	583	50	21,212	3,467 2,62	1 716	486	41	16	62	44	67.4	76.3 81	.2 0.9	69.1	63.6 66	.8 71.8	66.2 56	ô.0 56.6	67.0 55	5.2 54.2 5	7.5 60.6	58	126	271	583
El Nopal to Mast Boulevard, Year 2035 + project	4	15	28,310	40	0.5	3.0%	2.0%	71	60	129	277	598	50	21,997	3,595 2,718	3 743	504	43	16	64	46	67.4	76.3 81	.2 0.9	69.3	63.8 66	.9 72.0	66.4 56	ô.2 56.8	67.2 55	5.3 54.3 5	7.7 60.8	60	129	277	598
State Route 52						-		-						0	0 0	0	0	0	0	0	0	####	#### ##	## ####	* ####	¥### ###	######	#### ##		##### ##	## #### ##	### ####	0	0	0	0
Santo Road to Mast Boulevard, existing	6	60	96,000	65	0.5	2.0%	0.6%	76	246	531	1,143	2,462	100	74,592 1	2,192 9,210	5 1,67		97	16	144	46	75.5	81.7 85	5.2 -3.2	76.7	66.6 64	.9 77.4	73.8 59	J.0 54.7	74.0 61	1.1 57.1 5	5.7 63.3	246	531	1143	2462
Santo Road to Mast Boulevard, existing + project	6	60	106,531	65	0.5	2.0%	0.6%	76	264	569	1,225	2,639	100	82,775 1	3,529 10,22	7 1,86	3 570	108	18	160	52	75.5	81.7 85	5.2 -3.2	77.2	67.0 65	.4 77.8	74.2 59	J.4 55.2	74.4 61	1.5 57.6 5	6.1 63.8	264	569	1225	2639
Santo Road to Mast Boulevard, Near Term	6	60	104,092	65	0.5	2.0%	0.6%	76	260	560	1,206	2,599	100	80,879 1	3,220 9,993	3 1,82	0 556	105	18	157	50	75.5	81.7 85	5.2 -3.2	77.1	66.9 65	.3 77.7	74.1 59	J.3 55.1	74.3 61	1.4 57.5 5	6.0 63.7	260	560	1206	2599
Santo Road to Mast Boulevard, Near Term + project	6	60	114,066	65	0.5	2.0%	0.6%	77	276	595	1,282	2,762	100	88,629 1	4,486 10,95	0 1,99	5 610	115	19	172	55	75.5	81.7 85	5.2 -3.2	77.5	67.3 65	.7 78.1	74.5 59	J.7 55.5	74.7 61	1.8 57.9 5	6.4 64.1	276	595	1282	2762
Santo Road to Mast Boulevard, Year 2035	6	60	129,451	65	0.5	2.0%	0.6%	77	301	648	1,395	3,006	100	###### 1	6,440 12,42	7 2,26	4 692	131	22	195	63	75.5	81.7 85	5.2 -3.2	78.0	67.9 66	.2 78.7	75.1 60	J.3 56.0	75.3 62	2.4 58.4 5	7.0 64.6	301	648	1395	3006
Santo Road to Mast Boulevard, Year 2035 + project	6	60	133,589	65	0.5	2.0%	0.6%	77	307	661	1,425	3,069	100	####### 1	6,966 12,82	5 2,33	6 714	135	23	201	65	75.5	81.7 85	5.2 -3.2	78.2	68.0 66	.3 78.8	75.2 60	J.4 56.2	75.4 62	2.5 58.5 5	7.1 64.8	307	661	1425	3069

Appendix C. FHWA Noise Prediction Model Results – Land Use Plan Without School

TRAFFIC NOISE LEVELS AND NOISE CONTOURS

Project Number: 1501144001 Project Name: Fanita Ranch - No School Option

round Information												-									
Description: of Traffic Volumes: unity Noise Descriptor:	Linscott	Highway Nois , Law, and G _{dn} : X	reenspan, J	January 20		7-108) with	n California	Vehicle Noise	(CALVENO)	Emission Le	evels.										
24-Hour Traffic Distribution: Volumes		Day 77.70%	Evening 12.70%	Night 9.60%	-	Distance		ed within the re centerline of th on.													
y Trucks Trucks		87.43% 89.10%	5.05% 2.84%	7.52% 8.06%								_	Traffic Volu	imes					Ref. Energy Leve Dist Ld Le	Ln	DIST
n dition , Segment	Lanes	Median Width	ADT Volume	Design Speed (mph)	Alpha Factor	Vehi Medium Trucks	cle Mix Heavy Trucks	Ldn at	Dis	enterline of F stance to Cor 5 Ldn 60 I	ntour		c Day Eve t	e Night	MTd HT				n A MT HT Adj A MT HT Total A MT	HT Total A MT HT Total	
r ard West Hills Parkway, existing West Hills Parkway, existing + project	4 4	25 25	26,440 33,050	40 40	0.5 0.5	3.0% 3.0%	2.0% 2.0%	71 72	72	134 28 155 33	34 719	50 50	20,544 3, 25,680 4,		693 4 867 5	0 0 71 40 89 50	0 15 19	60 4 75 5	0 ##### ####	57.0 67.4 55.6 54.6 57.9 61.0 58.0 68.4 56.5 55.5 58.9 62.0	0 62 72
ast Hills Parkway, Near Term ast Hills Parkway, Near Term + project ast Hills Parkway, Year 2035	4 4 4	25 25	30,730 37,340	40	0.5	3.0%	2.0% 2.0% 2.0%	72 73 73	78	168 36	18 685 62 780	50 50	29,013 4,	,903 2,950 ,742 3,585	979 6	48 47 65 57 44 46	17 21 17	84 6	50 67.4 76.3 81.2 1.4 70.2 64.7 67.8 72.9 67.3 57.1 60 67.4 76.3 81.2 1.4 71.0 65.5 68.7 73.7 68.1 57.9 49 67.4 76.3 81.2 1.4 70.1 64.6 67.8 72.8 67.3 57.0	58.5 68.9 57.1 56.1 59.4 62.5	69 78 68
Hills Parkway, Year 2035 Hills Parkway, Year 2035 + project	4	25 25	30,500 33,970	40 40	0.5 0.5	3.0%	2.0%	72 72		147 31 158 34		50 50	26,395 4,		891 6	44 46 05 51 0 0	17 19 0		49 67.4 76.3 81.2 1.4 70.1 64.6 67.8 72.8 67.3 57.0 55 67.4 76.3 81.2 1.4 70.6 65.1 68.3 73.3 67.7 57.5 0 #### #### #### #### #### #### #### #	58.1 68.5 56.7 55.6 59.0 62.1	7
I arkway to Medina Drive, existing arkway to Medina Drive, existing + project	4 4	15 15	19,540 29,060	40 40	0.5 0.5	3.0% 3.0%	2.0% 2.0%	70 71		101 21 131 28	17 467 82 608	50 50	15,183 2,		513 3	48 30 18 44			31 67.4 76.3 81.2 0.9 67.7 62.2 65.3 70.4 64.8 54.6 47 67.4 76.3 81.2 0.9 69.4 63.9 67.1 72.1 66.5 56.3	55.2 65.6 53.7 52.7 56.1 59.2	4
kway to Medina Drive, Near Term kway to Medina Drive, Near Term + project	4 4	15 15	22,962 32,482	40 40	0.5 0.5	3.0% 3.0%	2.0% 2.0%	70 72	65	112 24 141 30	04 655	50 50	25,239 4,	,916 2,204 ,125 3,118	852 5	09 35 79 49	13 18		52 67.4 76.3 81.2 0.9 69.9 64.4 67.5 72.6 67.0 56.8	57.4 67.8 55.9 54.9 58.3 61.4	5
rkway to Medina Drive, Year 2035 rkway to Medina Drive, Year 2035 + project	4	15 15	29,000 34,600	40 40	0.5 0.5	3.0% 3.0%	2.0% 2.0%	71 72		131 28 147 31		50 50	26,884 4,	,683 2,784 ,394 3,322 0 0	908 6	17 44 17 52 0 0	16 20 0		47 67.4 76.3 81.2 0.9 69.4 63.9 67.0 72.1 66.5 56.3 56 67.4 76.3 81.2 0.9 70.2 64.6 67.8 72.9 67.3 57.1 0 ##### ##### ##### ##### ##### ##### ##### ##### #####<	57.6 68.1 56.2 55.2 58.6 61.7	6
h Drive to Fanita Parkway, existing h Drive to Fanita Parkway, existing + project	4 4	15 15	19,590 29,110	40 40	0.5 0.5	3.0% 3.0%	2.0% 2.0%	70 71		101 21 131 28	17 467 83 609	50 50	15,221 2,		514 3		11		32 67.4 76.3 81.2 0.9 67.7 62.2 65.3 70.4 64.8 54.6 47 67.4 76.3 81.2 0.9 69.4 63.9 67.1 72.1 66.5 56.3	55.2 65.6 53.7 52.7 56.1 59.2	í
ch Drive to Fanita Parkway, Near Term ch Drive to Fanita Parkway, Near Term + project	4 4	15 15	21,361 30,881	40 40	0.5 0.5	3.0%	2.0% 2.0%	70 72	63	136 29		50 50	23,995 3,		810 5	81 32 50 47	18	70 5	34 67.4 76.3 81.2 0.9 68.1 62.6 65.7 70.8 65.2 55.0 50 67.4 76.3 81.2 0.9 69.7 64.2 67.3 72.4 66.8 56.6	57.2 67.6 55.7 54.7 58.1 61.2	
Drive to Fanita Parkway, Year 2035 Drive to Fanita Parkway, Year 2035 + project Dad	4 4	15 15	29,000 34,440	40 40	0.5 0.5	3.0% 3.0%	2.0% 2.0%	71 72		131 28 147 31	82 607 16 681	50 50	26,760 4,	,683 2,784 ,374 3,306 0 0	903 6	17 44 14 52 0 0	16 20 0		47 67.4 76.3 81.2 0.9 69.4 63.9 67.0 72.1 66.5 56.3 56 67.4 76.3 81.2 0.9 70.1 64.6 67.8 72.8 67.3 57.0 0 #### ##### ##### #### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ####################################	57.6 68.1 56.2 55.2 58.6 61.6	
nita Drive, existing nita Drive, existing + project	6 6	15 15	45,440 51,260	45 45	0.5 0.5	5.0% 5.0%	3.0% 3.0%	77 78		325 69 352 75		50 50	35,307 5,	,771 4,362	1,986 1,3	215 115	39	171 1	110 69.3 77.6 82.1 2.6 74.4 70.6 72.9 77.7 71.6 63.0 124 69.3 77.6 82.1 2.6 74.9 71.1 73.5 78.2 72.1 63.5	62.8 72.6 62.8 61.1 63.7 67.4	
nita Drive, Near Term nita Drive, Near Term + project	6	15 15	48,026 53,846	45 45	0.5	5.0%	3.0% 3.0%	77 78	169	364 78		50	41,838 6,	838 5,169	2,354 1,4		46	202 13	116 69.3 77.6 82.1 2.6 74.6 70.8 73.2 77.9 71.8 63.2 130 69.3 77.6 82.1 2.6 75.1 71.3 73.7 78.4 72.3 63.7	63.5 73.4 63.6 61.8 64.4 68.2	
anita Drive, Year 2035 Fanita Drive, Year 2035 + project	6 6	15 15	49,200 52,670	45 45	0.5 0.5	5.0% 5.0%	3.0% 3.0%	78 78		342 73 358 77	37 1,589 72 1,663	50 50	40,925 6,		2,151 1,3 2,302 1,4 0			198 12	119 69.3 77.6 82.1 2.6 74.7 70.9 73.3 78.0 71.9 63.3 127 69.3 77.6 82.1 2.6 75.0 71.2 73.6 78.3 72.2 63.6 0 ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##	63.4 73.3 63.5 61.7 64.3 68.1	
e to Carlton Hills Boulevard, existing to Carlton Hills Boulevard, existing + project	6 6	15 15	41,100 47,710	45 45	0.5 0.5	5.0% 5.0%	3.0% 3.0%	77 77		304 65 335 72	54 1,409 22 1,557	50 50			1,797 1,0	099 104	35		99 69.3 77.6 82.1 2.6 73.9 70.1 72.5 77.2 71.2 62.5 115 69.3 77.6 82.1 2.6 74.6 70.8 73.2 77.9 71.8 63.2	62.3 72.2 62.4 60.7 63.3 67.0	
ve to Carlton Hills Boulevard, Near Term ve to Carlton Hills Boulevard, Near Term + project	6	15 15	43,029 49,639	45 45	0.5 0.5	5.0% 5.0%	3.0% 3.0%	77 78	145 160	313 67 344 74	74 1,453 42 1,598	50 50	33,434 5, 38,570 6,	465 4,131 304 4,765			42	162 10 187 12	104 69.3 77.6 82.1 2.6 74.1 70.3 72.7 77.4 71.4 62.7 120 69.3 77.6 82.1 2.6 74.8 70.9 73.3 78.0 72.0 63.4	62.5 72.4 62.6 60.9 63.5 67.2 63.2 73.0 63.2 61.5 64.1 67.8	
e to Carlton Hills Boulevard, Year 2035 e to Carlton Hills Boulevard, Year 2035 + project y	6 6	15 15	48,700 52,670	45 45	0.5 0.5	5.0% 5.0%	3.0% 3.0%	77 78		340 73 358 77	32 1,578 72 1,663		40,925 6,		2,302 1,	302 123 408 133 0 0		198 12	118 69.3 77.6 82.1 2.6 74.7 70.9 73.2 78.0 71.9 63.3 127 69.3 77.6 82.1 2.6 75.0 71.2 73.6 78.3 72.2 63.6 0 ##### ##### ##### ##### ##### ##### ##### ##### ##### ####################################	63.4 73.3 63.5 61.7 64.3 68.1	
to Ganley Drive, existing to Ganley Drive, existing + project	2	15 15	DNE 12,430	40 40	0.5 0.5	2.0% 2.0%	2.0% 2.0%	66	-	62 13	LUE! #VALUE 35 290	50	####### ### 9,658 1,	#### ###### 579 1,193	####### ### 217 2	22 13	## ###### 7	19 2	#### 67.4 76.3 81.2 0.1 #### #### #### #### #### #### 20 67.4 76.3 81.2 0.1 65.0 57.7 62.6 67.5 62.1 50.1	52.5 62.8 49.1 48.2 53.4 55.6	
to Ganley Drive, Near Term to Ganley Drive, Near Term + project to Ganley Drive, Year 2035	2 2 2	15 15 15	DNE 12,430 7,380	40 40 40	0.5 0.5 0.5	2.0% 2.0% 2.0%	2.0% 2.0% 2.0%	#VALUE! # 66 64		ALUE! #VAL 62 13 44 9		1 50 50 50	9,658 1,	#### ###### 579 1,193 937 708	217 2			19 2	#### 67.4 76.3 81.2 0.1 ##### ###### ##### ##### <	52.5 62.8 49.1 48.2 53.4 55.6	#VAL
to Ganley Drive, Year 2035 to Ganley Drive, Year 2035 + project y	2	15 15	7,380 12,430	40 40	0.5	2.0%	2.0%	64 66	-		35 205 35 290	50 50	9,658 1,	337 708 579 1,193 0 0	217 2	32 7 22 13 0 0	4 7 0	19 2	12 67.4 76.3 81.2 0.1 62.8 55.4 60.4 65.2 59.8 47.9 20 67.4 76.3 81.2 0.1 65.0 57.7 62.6 67.5 62.1 50.1 0 #### #### #### #### #### #### #### #	52.5 62.8 49.1 48.2 53.4 55.6	
e to Lake Canyon Road, existing e to Lake Canyon Road, existing + project	2	0 14	2,610 15,040	40 50	0.5	2.0%	2.0%	59 70	-	- 4 107 23	30 495	50 50	2,028 3 11,686 1,	331 251 ,910 1,444	46 4 263 2	47 3 68 15	1 9	4 4 23 2	4 67.4 76.3 81.2 -0.1 58.0 50.7 55.7 60.5 55.1 43.1 24 71.1 78.8 83.0 0.8 69.3 60.7 65.0 71.1 66.4 53.1	45.5 55.8 42.1 41.3 46.4 48.7 54.9 66.9 53.4 51.3 55.8 58.7	
e to Lake Canyon Road, Near Term e to Lake Canyon Road, Near Term + project e to Lake Canyon Road, Year 2035	2 4 2	0 14 0	2,782 15,212 9,920	40 50 40	0.5 0.5 0.5	2.0% 2.0% 2.0%	2.0% 2.0% 2.0%	60 70 65		- 4 107 23 52 11		50 50 50	11,820 1,	353 267 ,932 1,460 ,260 952	266 2	50 3 71 15 77 10	2 9 6	23 2	4 67.4 76.3 81.2 -0.1 58.3 51.0 55.9 60.8 55.4 43.4 25 71.1 78.8 83.0 0.8 69.4 60.8 65.1 71.2 66.5 53.2 16 67.4 76.3 81.2 -0.1 63.8 56.5 61.5 66.3 60.9 48.9	54.9 66.9 53.5 51.3 55.9 58.7	
ve to Lake Canyon Road, Year 2035 + project	4	14	15,210	50	0.5	2.0%	2.0%	70		107 23	31 499	50	11,818 1, 0	932 1,460 0 0	266 2 0	71 15 0 0	9		25 71.1 78.8 83.0 0.8 69.4 60.8 65.1 71.2 66.5 53.2 0 #### #### #### #### #### #### #### #	54.9 66.9 53.5 51.3 55.9 58.7	
n Road to Mast Boulevard, existing n Road to Mast Boulevard, existing + project n Road to Mast Boulevard, Near Term	2 4 2	0 14 0	3,860 15,230 4,158	40 50 40	0.5 0.5 0.5	2.0% 2.0% 2.0%	2.0% 2.0% 2.0%	61 70 61	-	- 6 107 23 - 6	32 499	50 50 50	11,834 1,	490 371 ,934 1,462 528 399	266 2	59 4 71 15 74 4	2 9 2		6 67.4 76.3 81.2 -0.1 59.7 52.4 57.4 62.2 56.8 44.8 25 71.1 78.8 83.0 0.8 69.4 60.8 65.1 71.2 66.5 53.2 7 67.4 76.3 81.2 -0.1 60.1 52.7 57.7 62.5 57.2 45.2	54.9 67.0 53.5 51.3 55.9 58.7	
n Road to Mast Boulevard, Near Term + project n Road to Mast Boulevard, Year 2035	4	14 0	15,528 10,910	50 40	0.5	2.0%	2.0%	70 66		109 23 56 12	35 505	50 50	12,065 1,	972 1,491	272 2	77 16 94 11	9	23 2	7 67.4 76.3 61.2 -0.1 60.1 52.7 51.7 52.3 51.2 43.2 25 71.1 78.8 83.0 0.8 69.5 60.9 65.2 71.3 66.6 53.3 18 67.4 76.3 81.2 -0.1 64.3 56.9 61.9 66.7 61.3 49.4	55.0 67.0 53.5 51.4 55.9 58.8	
n Road to Mast Boulevard, Year 2035 + project	4	14	15,530	50	0.5	2.0%	2.0%	70	-	109 23		50 50	0	972 1,491 0 0	0	77 16 0 0 30 3	9	0 0	25 71.1 78.8 83.0 0.8 69.5 60.9 65.2 71.3 66.6 53.3 0 #### #### #### #### #### #### #### #	****	
ard to Carlton Oaks Drive, existing ard to Carlton Oaks Drive, existing + project ard to Carlton Oaks Drive, Near Term	2 2 2	0 0 0	3,330 6,770 3,713	35 35 35	0.5 0.5 0.5	2.0% 2.0% 2.0%	1.0% 1.0% 1.0%	58 61 59	-	- 3 - 6 - 4		50 50 50	5,260 8	423 320 360 650 472 356	118 6	30 3 50 7 33 4	1 2 1	10 5	3 65.1 74.8 80.0 -0.1 57.5 50.9 53.2 59.5 54.5 43.3 5 65.1 74.8 80.0 -0.1 60.6 54.0 56.2 62.6 57.6 46.4 3 65.1 74.8 80.0 -0.1 58.0 51.4 53.6 60.0 55.0 43.8	46.1 58.2 44.8 44.5 47.0 50.4	
ward to Carlton Oaks Drive, Near Term + project ward to Carlton Oaks Drive, Year 2035	2	0	7,153 6,000	35 35	0.5	2.0%	1.0%	62 61	-	- 6 - 5	58 124	50 50	4,662 7	008 <u>687</u> 762 576	105 5	54 7 53 6	2	11 0 9 5	6 65.1 74.8 80.0 -0.1 60.8 54.2 56.5 62.8 57.8 46.6 5 65.1 74.8 80.0 -0.1 60.0 53.4 55.7 62.1 57.1 45.9	45.6 57.7 44.3 44.0 46.5 49.8	
vard to Carlton Oaks Drive, Year 2035 + project soulevard to Drive to Mission Gorge Road, existing	2	0	7,400	35	0.5	2.0%	2.0%	62		- 6 92 19		50 50	0	0 710 0 0 170 2 396	0	6 7 0 0 45 38	2 0 14	11 0 0 0 56 4	6 65.1 74.8 80.0 -0.1 61.0 54.3 56.6 63.0 58.0 46.8 0 ##### ##### ##### ##### ##### ##### ##### ##### ##### #### ##### ##### ##### ##### ##### ##### ####################################	**** **** **** **** ****	
s Drive to Mission Gorge Road, existing + project s Drive to Mission Gorge Road, Near Term	4	0 0	29,460 25,993	35 35	0.5	3.0%	2.0% 2.0%	70 69	48	103 22 95 20	22 478 04 440	50 50	22,890 3, 20,197 3,	741 2,828 301 2,495	773 5 682 4	25 45 63 39	17 15	66 4	47 65.1 74.8 80.0 0.3 67.3 62.5 66.1 70.5 64.4 54.9 42 65.1 74.8 80.0 0.3 66.7 62.0 65.5 69.9 63.8 54.4	55.9 65.4 53.3 53.1 56.8 59.5 55.3 64.8 52.8 52.5 56.3 59.0	
Drive to Mission Gorge Road, Near Term + project Drive to Mission Gorge Road, Year 2035 Drive to Mission Gorge Road, Year 2035 + project	4	0	30,493 32,800 33,850	35 35 35	0.5 0.5 0.5	3.0% 3.0% 3.0%	2.0% 2.0% 2.0%	70 70 70	51	105 22 111 23 113 24	38 514	50 50 50	25,486 4,	166 3,149	860 5	43 46 84 50 03 51		74 5	49 65.1 74.8 80.0 0.3 67.4 62.7 66.2 70.6 64.5 55.1 53 65.1 74.8 80.0 0.3 67.7 63.0 66.5 70.9 64.8 55.4 55 65.1 74.8 80.0 0.3 67.9 63.1 66.7 71.1 65.0 55.5	56.4 65.8 53.8 53.5 57.3 60.0	
eet to Magnolia Avenue, existing	2	10	33,850 DNE	40	0.5	2.0%	2.0%	-			LUE! #VALUE			299 3,250 0 0 #### #####		0 0	0		0 ##### ##### #### #### #### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ####################################	****	#VAL
to Magnolia Avenue, existing + project to Magnolia Avenue, Near Term	2 2	10 10	14,020 DNE	40 40	0.5 0.5	2.0% 2.0%	2.0% 2.0%	67 #VALUE! #	VALUE! #V		LUE! #VALUE		*****	,781 1,346 #### ######	* ******		*# ######		23 67.4 76.3 81.2 0.1 65.5 58.1 63.1 67.9 62.5 50.6 #### 67.4 76.3 81.2 0.1 #### #### #### #### #### ####	****	#VAL
Magnolia Avenue, Near Term + project Magnolia Avenue, Year 2035 Magnolia Avenue, Year 2035 + project	2	10 10 10	14,020 8,630 14,020	40 40 40	0.5 0.5 0.5	2.0% 2.0% 2.0%	2.0% 2.0% 2.0%	67 65 67	-	48 10	44 310 04 224 44 310	50 50 50	6,706 1,		151 1	50 14 54 9 50 14	8 5 8	13 1	23 67.4 76.3 81.2 0.1 65.5 58.1 63.1 67.9 62.5 50.6 14 67.4 76.3 81.2 0.1 63.4 56.0 61.0 65.8 60.4 48.4 23 67.4 76.3 81.2 0.1 63.5 58.1 63.1 67.9 62.5 50.6 23 67.4 76.3 81.2 0.1 65.5 58.1 63.1 67.9 62.5 50.6	50.8 61.1 47.4 46.6 51.7 54.0	
et enue to Princess Joann Road, existing	2	10	DNE	40	0.5	2.0%	2.0%	-		ALUE! #VAL	LUE! #VALUE		0 ####### ###	0 0 #### ######	0 # ###### ###	0 0 #### #####	0 ## ######	0 (0	****	#VAL
Avenue to Princess Joann Road, existing + project Avenue to Princess Joann Road, Near Term Avenue to Princess Joann Road, Near Term + project	2	10 10 10	7,670 DNE 7,670	40 40 40	0.5 0.5 0.5	2.0% 2.0% 2.0%	2.0% 2.0% 2.0%	64 #VALUE! # 64	- VALUE! #V	45 9 ALUE! #VAL 45 9	LUE! #VALUE	50 E! 50 50	####### ###	974 736 #### ###### 974 736	* ###### ###	37 8 #### ##### 37 8	4 ## ###### 4	****	12 67.4 76.3 81.2 0.1 62.8 55.5 60.4 65.3 59.9 47.9 #### 67.4 76.3 81.2 0.1 #### #### #### #### #### 12 67.4 76.3 81.2 0.1 62.8 55.5 60.4 65.3 59.9 47.9	****	#VAL
enue to Princess Joann Road, Year 2035 enue to Princess Joann Road, Year 2035 enue to Princess Joann Road, Year 2035 + project	2	10 10	6,800 8,980	40 40	0.5	2.0%	2.0%	64 65		41 8		50 50	5,284 8	364 653	119 1	21 7 60 9	4	10 1	11 67.4 76.3 81.2 0.1 62.3 55.0 59.9 64.8 59.4 47.4 14 67.4 76.3 81.2 0.1 63.5 56.2 61.1 66.0 60.6 48.6	49.8 60.1 46.4 45.5 50.7 52.9	
eet ann Road to Chaparral Drive, existing	2	10	DNE	40	0.5	2.0%	2.0%				LUE! #VALUE		####### ###		* ###### ###			****	0 #### #### #### #### #### #### #### #	**** **** **** **** ****	#VAL
ann Road to Chaparral Drive, existing + project ann Road to Chaparral Drive, Near Term ann Road to Chaparral Drive, Near Term + project	2 2 2	10 10 10	7,670 DNE 7.670	40 40 40	0.5 0.5 0.5	2.0% 2.0% 2.0%	2.0% 2.0% 2.0%	64 #VALUE! # 64	VALUE! #V	45 9 ALUE! #VAL 45 9	LUE! #VALUE	50 E! 50 50	####### ###	974 736 #### ###### 974 736	* ###### ###	37 8 #### ##### 37 8	4 ## ###### 4	****	12 67.4 76.3 81.2 0.1 62.8 55.5 60.4 65.3 59.9 47.9 #### 67.4 76.3 81.2 0.1 #### #### #### #### #### 12 67.4 76.3 81.2 0.1 62.8 55.5 60.4 65.3 59.9 47.9	****	#VAI
ann Road to Chaparral Drive, Year 2035 ann Road to Chaparral Drive, Year 2035 + project	2 2	10 10	9,400 11,580	40 40	0.5 0.5	2.0% 2.0%	2.0% 2.0%	65 66	-	51 11	10 237 27 273	50 50	7,304 1, 8,998 1,	,194 902 ,471 1,112	202 2	68 9 06 12	5 7	14 1 17 1	15 67.4 76.3 81.2 0.1 63.7 56.4 61.3 66.2 60.8 48.8 19 67.4 76.3 81.2 0.1 64.6 57.3 62.2 67.1 61.7 49.7	51.2 61.5 47.8 46.9 52.1 54.3 52.1 62.4 48.7 47.9 53.0 55.2	
t ve to Woodglen Vista Drive, existing ve to Woodglen Vista Drive, existing + project	2 4	40 16	670 8,340	35 50	0.5 0.5	3.0% 3.0%	2.0% 2.0%	54 68	-	 78 16	 67 360	50 50	521 8	0 0 85 64 .059 801	18 1	0 0 12 1 49 13	0 0 5	2	0 #### #### #### #### #### #### #### #	40.0 49.5 37.4 37.2 41.0 43.7	
e to Woodglen Vista Drive, Near Term e to Woodglen Vista Drive, Near Term + project	2	40 16	683 8,353	35 50	0.5 0.5	3.0% 3.0%	2.0% 2.0%	54 68	-	 78 16	 67 361	50 50	531 8 6,490 1,	87 66 061 802	18 1 219 1	12 1 49 13	0 5	2 19 1	1 65.1 74.8 80.0 0.9 51.5 46.7 50.3 54.7 48.6 39.2 13 71.1 78.8 83.0 0.9 66.8 60.0 62.6 68.8 63.9 52.4	40.1 49.6 37.5 37.3 41.0 43.8 52.4 64.5 52.9 50.6 53.3 57.2	
to Woodglen Vista Drive, Year 2035 to Woodglen Vista Drive, Year 2035 + project	4 4	16 16	9,400 11,580	50 50	0.5 0.5	3.0% 3.0%	2.0% 2.0%	68 69	-	84 18 97 20		50 50	8,998 1,	,194 902 ,471 1,112 0 0	304 2	68 14 06 18 0 0	5 7 0		15 71.1 78.8 83.0 0.9 67.3 60.5 63.1 69.3 64.4 53.0 19 71.1 78.8 83.0 0.9 68.2 61.4 64.0 70.2 65.4 53.9 0 ##### #### #### #### ##### ##### ##### ##### ##### <td>53.8 65.9 54.3 52.0 54.8 58.6</td> <td></td>	53.8 65.9 54.3 52.0 54.8 58.6	
Drive to El Nopal, existing Drive to El Nopal, existing + project	2 4	40 16	4,360 12,030	35 50	0.5 0.5	3.0% 3.0%	2.0% 2.0%	62 69	-	- 6 99 21	14 460	50 50	3,388 5	0 0 554 419 ,528 1,155	114 7	0 0 78 7 14 18	0 2 7	10 7	0 #### #### #### #### #### #### 7 65.1 74.8 80.0 0.9 59.5 54.8 58.3 62.7 56.6 47.2 19 71.1 78.8 83.0 0.9 68.4 61.6 64.2 70.4 65.5 54.0	48.2 57.6 45.6 45.3 49.1 51.8	
Drive to El Nopal, Near Term Drive to El Nopal, Near Term + project	2	40 16	4,472 12,142	35 50	0.5 0.5	3.0% 3.0%	2.0% 2.0%	62 69	-	- 6 100 21	i9 149 15 463	50 50	3,475 5 9,434 1,	568 429 542 1,166	117 8 318 2	30 7 16 18	3 7	10 7 27 2	7 65.1 74.8 80.0 0.9 59.6 54.9 58.4 62.9 56.8 47.3 20 71.1 78.8 83.0 0.9 68.4 61.7 64.2 70.4 65.6 54.1	48.3 57.7 45.7 45.4 49.2 51.9 54.0 66.1 54.5 52.2 55.0 58.8	
brive to El Nopal, Year 2035 brive to El Nopal, Year 2035 + project	4 4	16 16	12,600 14,780	50 50	0.5 0.5	3.0% 3.0%	2.0% 2.0%	70 70		102 22 114 24		50 50	11,484 1,	,600 1,210 ,877 1,419 0 0	388 2	25 19 63 22 0 0	7 8 0		20 71.1 78.8 83.0 0.9 68.6 61.8 64.4 70.6 65.7 54.2 24 71.1 78.8 83.0 0.9 69.3 62.5 65.1 71.3 66.4 54.9 0 ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ###### ####################################	54.9 67.0 55.3 53.1 55.8 59.7	
Boulevard, existing Boulevard, existing + project	3 4	30 16	8,860 16,530	35 50	0.5 0.5	3.0% 3.0%	2.0% 2.0%	65 71	- 57		64 569	50 50	6,884 1, 12,844 2,	125 851 099 1,587	232 1 434 2	58 13 95 25	5 9	37 2	14 65.1 74.8 80.0 1.0 62.7 58.0 61.5 65.9 59.8 50.4 27 71.1 78.8 83.0 0.9 69.8 63.0 65.5 71.8 66.9 55.4	51.3 60.8 48.8 48.5 52.3 55.0 55.4 67.5 55.8 53.5 56.3 60.2	
loulevard, Near Term loulevard, Near Term + project loulevard, Year 2035	3 4 4	30 16 16	9,173 16,843 16,500	35 50 50	0.5 0.5 0.5	3.0% 3.0% 3.0%	2.0% 2.0% 2.0%	65 71 71		- 11 124 26 122 26		50 50 50	13,087 2,	,165 881 ,139 1,617 ,096 1,584	442 3	63 14 00 26 94 25	5 10 9	38 2	15 65.1 74.8 80.0 1.0 62.9 58.1 61.7 66.1 60.0 50.5 27 71.1 78.8 83.0 0.9 69.9 63.1 65.6 71.9 67.0 55.5 27 71.1 78.8 83.0 0.9 69.8 63.0 65.5 71.8 66.9 55.4	55.5 67.6 55.9 53.6 56.4 60.2	
t Boulevard, Year 2035 + project	4	16	18,680	50	0.5	3.0%	2.0%	71		133 28	86 617	50	14,514 2, 0	372 1,793 0 0	490 3 0	33 <u>28</u> 0 0	11 0	42 3	30 71.1 78.8 83.0 0.9 70.3 63.5 66.1 72.3 67.4 55.9 0 #### #### #### #### #### #### #### #	55.9 68.0 56.4 54.1 56.8 60.7	
to River Park Drive, existing to River Park Drive, existing + project	4	15 15	19,600 25,420	35 35	0.5	3.0% 3.0%	2.0%	68 70		85 18 101 21	18 470	50 50	19,751 3,	228 2,440	667 4	49 30 53 39	11 14	57 4	32 65.1 74.8 80.0 0.9 66.0 61.3 64.8 69.2 63.1 53.7 41 65.1 74.8 80.0 0.9 67.1 62.4 65.9 70.4 64.3 54.8 <td>55.8 65.2 53.2 52.9 56.7 59.4</td> <td></td>	55.8 65.2 53.2 52.9 56.7 59.4	
to River Park Drive, Near Term to River Park Drive, Near Term + project to River Park Drive, Year 2035	4 4 4	15 15 15	20,527 26,347 26,600	35 35 35	0.5 0.5 0.5	3.0% 3.0% 3.0%	2.0% 2.0% 2.0%	69 70 70	-	104 22	89 408 24 482 25 485	50 50 50	20,472 3,	346 2,529	691 4	66 31 70 40 74 40	12 15 15	59 4	33 65.1 74.8 80.0 0.9 66.2 61.5 65.0 69.4 63.3 53.9 42 65.1 74.8 80.0 0.9 67.3 62.6 66.1 70.5 64.4 55.0 43 65.1 74.8 80.0 0.9 67.3 62.6 66.1 70.5 64.4 55.0	55.9 65.4 53.3 53.1 56.9 59.6	
River Park Drive, Year 2035 + project	4	15	27,550	35	0.5	3.0%	2.0%	70	-	107 23	30 496	50	21,406 3, 0	499 2,645 0 0	723 4 0	91 42 0 0	16 0	62 4 0 0	44 65.1 74.8 80.0 0.9 67.5 62.8 66.3 70.7 64.6 55.2 0 ##### #### #### ##### #### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ####################################	56.1 65.6 53.5 53.3 57.1 59.8	
Town Center Parkway, existing Town Center Parkway, existing + project Town Center Parkway, Near Term	4	15 15 15	26,690 32,240 28.084	35 35 35	0.5 0.5 0.5	3.0% 3.0% 3.0%	2.0% 2.0% 2.0%	70 71 70	55	105 22 119 25 108 23	56 551	50 50 50	25,050 4,		846 5	76 40 75 49 00 43	15 18 16	73 5	43 65.1 74.8 80.0 0.9 67.4 62.6 66.2 70.6 64.5 55.0 52 65.1 74.8 80.0 0.9 68.2 63.4 67.0 71.4 65.3 55.8 45 65.1 74.8 80.0 0.9 67.6 62.8 66.4 70.8 64.7 55.3	56.8 66.3 54.2 54.0 57.7 60.4	
to Town Center Parkway, Near Term to Town Center Parkway, Near Term + project to Town Center Parkway, Year 2035	4 1 4 4	15 15 15	28,084 33,634 31,700	35 35 35	0.5 0.5 0.5	3.0% 3.0% 3.0%	2.0% 2.0% 2.0%	70 71 71	57		63 567	50 50 50	26,134 4,	,567 2,696 ,272 3,229 ,026 3,043	882 5	00 43 99 51 65 48	19	76 5	45 65.1 74.8 80.0 0.9 67.6 62.8 66.4 70.8 64.7 55.3 54 65.1 74.8 80.0 0.9 68.4 63.6 67.2 71.6 65.5 56.0 51 65.1 74.8 80.0 0.9 68.1 63.4 66.9 71.3 65.2 55.8	57.0 66.5 54.4 54.2 57.9 60.6	
to Town Center Parkway, Year 2035 + project	4	15	32,700	35	0.5	3.0%	2.0%	71	56	120 25	58 556	50	25,408 4, 0	153 3,139 0 0	858 5 0	83 <u>50</u> 0 0	19 0	74 5	53 65.1 74.8 80.0 0.9 68.2 63.5 67.0 71.4 65.4 55.9 0 ##### ###### ####################################	56.9 66.3 54.3 54.0 57.8 60.5	
arkway to Mission Gorge Road, existing arkway to Mission Gorge Road, existing + projec arkway to Mission Gorge Road, Near Term	6 ct 6 6	15 15 15	21,850 26,870 24,245	35 35 35	0.5 0.5 0.5	5.0% 5.0% 5.0%	3.0% 3.0% 3.0%	72 73 72	78	147 31 169 36 158 34	64 785	50 50 50	20,878 3,	,775 2,098 ,412 2,580 ,079 2,328	1,175 7	84 55 18 68 48 61	19 23 21	101 6	53 65.1 74.8 80.0 2.6 68.0 65.7 68.8 72.5 65.3 58.1 65 65.1 74.8 80.0 2.6 68.9 66.6 69.7 73.3 66.2 59.0 59 65.1 74.8 80.0 2.6 68.5 66.1 69.2 72.9 65.7 58.5	59.5 67.7 57.4 57.1 60.4 63.4	
arkway to Mission Gorge Road, Near Term + pro arkway to Mission Gorge Road, Year 2035	6	15 15	29,265 30,100	35 35	0.5	5.0% 5.0%	3.0% 3.0%	73 73	83 85	179 38 182 39	86 831 93 846	50 50	22,739 3, 23,388 3,	717 2,809 823 2,890	1,279 7 1,316 8	82 74 05 76	25 26	110 7 113 7	71 65.1 74.8 80.0 2.6 69.3 66.9 70.0 73.7 66.5 59.4 73 65.1 74.8 80.0 2.6 69.4 67.1 70.2 73.8 66.7 59.5	59.9 68.0 57.8 57.5 60.8 63.7 60.0 68.1 57.9 57.6 60.9 63.9	
Parkway to Mission Gorge Road, Year 2035 + pro ue	oj∉ 6 2	15	31,670	35	0.5	5.0%	3.0%	74	88	189 40		50	24,608 4, 0	022 3,040 0 0	0	47 80 0 0	27	119 7 0 (77 65.1 74.8 80.0 2.6 69.7 67.3 70.4 74.1 66.9 59.7 0 ##### ##### #### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ##### ####################################	****	#\/*'
treet to Princess Joann Road, existing treet to Princess Joann Road, existing + project treet to Princess Joann Road, Near Term	2 2 2	12 12 12	DNE 6,350 DNE	35 35 35	0.5 0.5 0.5	3.0% 3.0% 3.0%	2.0% 2.0% 2.0%	63	-	- 7	LUE! #VALUE 77 165 LUE! #VALUE	50	4,934 8	306 610	167 1	13 10	4	14 1	10 65.1 74.8 80.0 0.1 60.3 55.6 59.1 63.5 57.4 48.0 #### 65.1 74.8 80.0 0.1 #### #### #### #### ####	49.0 58.4 46.4 46.1 49.9 52.6	
treet to Princess Joann Road, Near Term + project treet to Princess Joann Road, Year 2035	t 2 2	12 12	6,350 4,300	35 35	0.5	3.0%	2.0% 2.0%	63 61	-	- 7	77 165 59 127	50 50	4,934 8 3,341 5	30 <u>6 610</u> 546 413	167 1 113 7	1 <u>3</u> 10 77 7	4	14 1 10 7	10 65.1 74.8 80.0 0.1 60.3 55.6 59.1 63.5 57.4 48.0 7 65.1 74.8 80.0 0.1 58.6 53.9 57.4 61.8 55.8 46.3	49.0 58.4 46.4 46.1 49.9 52.6 47.3 56.7 44.7 44.4 48.2 50.9	_
treet to Princess Joann Road, Year 2035 + project ue Inn Road to Woodglen Vista Drive, existing	4	12	7,510 2,020	35 40	0.5	3.0%	2.0% 2.0%	64	-	40 8	- 103	50 50	0	054 721 0 0 257 194	0	34 11 0 0 36 3	4 0 1	0 0	12 65.1 74.8 80.0 0.1 61.1 56.3 59.9 64.3 58.2 48.7 0 ##### #### #### ###### ##### ###### ##### ##### ####################################	****	
ann Road to Woodglen Vista Drive, existing + projet ann Road to Woodglen Vista Drive, Near Term		15 15	8,370 2,204	40 40	0.5 0.5	3.0% 3.0%	2.0% 2.0%	66 60	-		23 265 - 109	50 50	6,503 1, 1,713 2	063 804 280 212	220 1 58 3	49 13 39 3	5 1	19 1 5 4	13 67.4 76.3 81.2 0.9 64.0 58.5 61.6 66.7 61.1 50.9 4 67.4 76.3 81.2 0.9 58.2 52.7 55.9 60.9 55.3 45.1	51.5 61.9 50.0 49.0 52.4 55.5 45.7 56.1 44.2 43.2 46.6 49.7	
n Road to Woodglen Vista Drive, Near Term + pr n Road to Woodglen Vista Drive, Year 2035	oj 4 4	15 15	8,554 9,500	40	0.5	3.0%	2.0%	66 66		62 13		50 50	7,382 1,		249 1	52 13 69 14		21 1	14 67.4 76.3 81.2 0.9 64.1 58.6 61.7 66.8 61.2 51.0 15 67.4 76.3 81.2 0.9 64.5 59.0 62.2 67.2 61.7 51.4 0 74 70.3 81.2 0.9 64.5 59.0 62.2 67.2 61.7 51.4	52.0 62.5 50.6 49.6 53.0 56.1	
n Road to Woodglen Vista Drive, Year 2035 + pro	oji 4	15	12,710	40	0.5	3.0%	2.0%	68	-	75 16	63 350	50	9,876 1,	,614 1,220	333 2	26 19	7	29 2	20 67.4 76.3 81.2 0.9 65.8 60.3 63.5 68.5 62.9 52.7	53.3 63.7 51.8 50.8 54.2 57.3	

Princess Joann Road to Woodglen Vista Drive, Year 2035	4	15	9,500	40	0.5	3.0%	2.0%	66	-	62	134	289	50	7,38	2 1,207	912	249	169	14	5	21	15	67.4 76.3	81.2 0.9	9 64.5	59.0 62.	2 67.2 6	1.7 51.4	52.0 62	.5 50.6 49.6 53.	0 56.1	29	62	134	289
Princess Joann Road to Woodglen Vista Drive, Year 2035 + proj-	4	15	12,710	40	0.5	3.0%	2.0%	68	-	75	163	350	50	9,87	6 1,614	1,220	333	226	19	7	29	20	67.4 76.3	81.2 0.9	65.8	60.3 63.	5 68.5 6	2.9 52.7	53.3 63	7 51.8 50.8 54.	2 57.3	35	75	163	350
Magnolia Avenue														0	0	0	0	0	0	0	0	0	#### ####	#### ###	# #### 1	4### ###	# #### #	*## ####	##### ###	III	# ####	0	0	0	0
Woodglen Vista Drive to El Nopal, existing	4	15	9,030	40	0.5	3.0%	2.0%	66	-	60	129	279	50	7,01	6 1,147	867	237	161	14	5	20	15	67.4 76.3	81.2 0.9	64.3	58.8 62.	0 67.0 6	1.4 51.2	51.8 62	2 50.4 49.4 52.	7 55.8	28	60	129	279
Woodglen Vista Drive to El Nopal, existing + project	4	15	15,380	40	0.5	3.0%	2.0%	69	-	86	185	398	50	11,95	50 1,953	3 1,476	403	274	23	9	35	25	67.4 76.3	81.2 0.9	9 66.6	61.1 64.	3 69.3 6	3.7 53.5	54.1 64	.6 52.7 51.7 55.	1 58.1	40	86	185	398
Woodglen Vista Drive to El Nopal, Near Term	4	15	9,415	40	0.5	3.0%	2.0%	66	-	62	133	287	50	7,31	5 1,196	904	247	168	14	5	21	15	67.4 76.3	81.2 0.9	64.5	59.0 62.	2 67.2 6	1.6 51.4	52.0 62	4 50.5 49.5 52.	9 56.0	29	62	133	287
Woodglen Vista Drive to El Nopal, Near Term + project	4	15	15,765	40	0.5	3.0%	2.0%	69	-	87	188	404	50	12,24	9 2,002	2 1,513	414	281	24	9	36	25	67.4 76.3	81.2 0.9	9 66.7	61.2 64.	4 69.4 6	3.9 53.6	54.2 64	.7 52.8 51.8 55.	2 58.3	40	87	188	404
Woodglen Vista Drive to El Nopal, Year 2035	4	15	13,600	40	0.5	3.0%	2.0%	68	-	79	170	367	50	10,56	67 1,727	7 1,306	357	242	21	8	31	22	67.4 76.3	81.2 0.9	9 66.1	60.6 63.	8 68.8 6	3.2 53.0	53.6 64	.0 52.1 51.1 54.	5 57.6	37	79	170	367
Woodglen Vista Drive to El Nopal, Year 2035 + project	4	15	16,810	40	0.5	3.0%	2.0%	69	-	91	196	422	50	13,06	61 2,135	5 1,614	441	300	25	10	38	27	67.4 76.3	81.2 0.9	9 67.0	61.5 64.	7 69.7 6	4.1 53.9	54.5 64	.9 53.1 52.1 55.	4 58.5	42	91	196	422
Magnolia Avenue														0	0	0	0	0	0	0	0	0	#### ####	#### ###	# #### 1	¥### ###	# #### ##	*## ####	##### ###	IH #### #### ###	# ####	0	0	0	0
El Nopal to Mast Boulevard, existing	4	15	13,690	40	0.5	3.0%	2.0%	68	-	79	171	368	50	10,63	37 1,739	1,314	359	244	21	8	31	22	67.4 76.3	81.2 0.9	9 66.1	60.6 63.	8 68.8 6	3.2 53.0	53.6 64	1 52.2 51.2 54.	6 57.6	37	79	171	368
El Nopal to Mast Boulevard, existing + project	4	15	17,390	40	0.5	3.0%	2.0%	69	-	93	200	432	50	13,51	2,209	1,669	456	310	26	10	39	28	67.4 76.3	81.2 0.9	67.2	61.7 64.	8 69.9 6	4.3 54.1	54.7 65	.1 53.2 52.2 55.	6 58.7	43	93	200	432
El Nopal to Mast Boulevard, Near Term	4	15	14,291	40	0.5	3.0%	2.0%	68	-	82	176	379	50	11,10	04 1,815	5 1,372	375	255	22	8	32	23	67.4 76.3	81.2 0.9	66.3	60.8 64.	0 69.0 6	3.4 53.2	53.8 64	2 52.4 51.4 54.	7 57.8	38	82	176	379
El Nopal to Mast Boulevard, Near Term + project	4	15	17,991	40	0.5	3.0%	2.0%	69		95	205	442	50	13,97	9 2,285	5 1,727	472	321	27	10	41	29	67.4 76.3	81.2 0.9	67.3	61.8 65.	0 70.0 6	4.4 54.2	54.8 65	2 53.4 52.4 55.	7 58.8	44	95	205	442
El Nopal to Mast Boulevard, Year 2035	4	15	27,300	40	0.5	3.0%	2.0%	71	58	126	271	583	50	21,21	2 3,467	2,621	716	486	41	16	62	44	67.4 76.3	81.2 0.9	9 69.1	63.6 66.	8 71.8 6	6.2 56.0	56.6 67	.0 55.2 54.2 57.	5 60.6	58	126	271	583
El Nopal to Mast Boulevard, Year 2035 + project	4	15	28,330	40	0.5	3.0%	2.0%	71	60	129	277	598	50	22,01	2 3,598	3 2,720	743	505	43	16	64	46	67.4 76.3							2 55.3 54.3 57.		60	129	277	598
State Route 52														0	0	0	0	0	0	0	0	0								III		0	0	0	0
Santo Road to Mast Boulevard, existing	6	60	96,000	65	0.5	2.0%	0.6%	76	246	531	1,143	2,462	100				1,679	513	97	16	144	46								.0 61.1 57.1 55.		246	531	1143	2462
Santo Road to Mast Boulevard, existing + project	6	60	103,669	65	0.5	2.0%	0.6%	76	259	558	1,203	2,592	100	80,55		,	1,813	554	105	18	156	50								.3 61.4 57.4 56.		259	558	1203	2592
Santo Road to Mast Boulevard, Near Term	6	60	104,092	65	0.5	2.0%	0.6%	76	260	560	1,206	2,599	100	80,87	79 13,22		1,820	556	105	18	157	50								.3 61.4 57.5 56.		260	560	1206	2599
Santo Road to Mast Boulevard, Near Term + project	6	60	111,761	65	0.5	2.0%	0.6%	77	273	587	1,265	2,725	100	86,83	14,10		1,954	597	113	19	168	54	75.5 81.7	85.2 -3.	2 77.4	67.2 65.	6 78.1 7	4.4 59.6	55.4 74	.6 61.7 57.8 56.	3 64.0	273	587	1265	2725
Santo Road to Mast Boulevard, Year 2035	6	60	129,451	65	0.5	2.0%	0.6%	77	301	648	1,395	3,006	100	####	## 16,44	0 12,427	2,264	692	131	22	195	63	75.5 81.7	85.2 -3.	2 78.0	67.9 66.	2 78.7 7	5.1 60.3	56.0 75	.3 62.4 58.4 57.	0 64.6	301	648	1395	3006
Santo Road to Mast Boulevard, Year 2035 + project	6	60	137,120	65	0.5	2.0%	0.6%	77	312	673	1,450	3,123	100	####	## 17,41	4 13,164	2,398	733	138	23	206	66	75.5 81.7	85.2 -3.	2 78.3	68.1 66.	5 78.9 7	5.3 60.5	56.3 75	.5 62.6 58.7 57.	2 64.9	312	673	1450	3123
Proposed Project Trip % on SR-52	29%																																		
	26445																																		
No School Scenarion Trips on SR-52	7669																																		

Appendix D. FHWA Noise Prediction Model Results – Average Construction Volumes

TRAFFIC NOISE LEVELS AND NOISE CONTOURS

Project Number: 1501144001 posed Project (with school)

Project Number: 15 Project Name: Fa			sed Project	t (with scho	ool)							_																		
ackground Information	HWA Higt	hway Noise	e Prediction	n Model (Fl	HWA-RD-7	7-108) with	ı California	Vehicle Noise (CA	LVENO) Emi	ssion Level	ls.	_																		
ource of Traffic Volumes: Lin community Noise Descriptor:		aw, and Gro X	eenspan, Ja CNEL:	anuary 20'	_	"-" = conto	our is locate	ed within the roadw	av right-of-wa	av.																				
sumed 24-Hour Traffic Distribution: tal ADT Volumes		77.70%	Evening 12.70%	9.60%	_		s from the	centerline of the ro																						
adium-Duty Trucks avy-Duty Trucks			5.05% 2.84%	7.52% 8.06%								_																		
alysis Condition		Median	ADT	Design Speed	Alpha	Medium		Ldn at		e to Contou	Jr		Traffic Vo		MTd	HTd M	ITe HTe	e MTn		Ref. Energy Leve		мт нт	Le Total A	мт нт	Ln Total A	мт н	T Total		NCE TO CO 5 Ldn 6	
Roadway, Segment L ast Boulevard SR-52 to West Hills Parkway, existing	Lanes 4	Width 25	Volume 26,440	(mph) 40	Factor 0.5	Trucks	Trucks 2.0%	50 Feet 70 L		1 60 Ldn 288	1 55 Ldn 620	Dis	0	0 0	0	0 471		0 0		*### #### #### 67.4 76.3 81.2								0	0 134	0 288
SR-52 to West Hills Parkway, existing + construction SR-52 to West Hills Parkway, Near Term	4	25 25	26,590 30,730	40 40	0.5	3.0%	2.0%	71 62 72 69	134	289 318	622 685	50 50	20,660	3,377 2,55	3 697	474	40 1	15 60 17 69	43	67.4 76.3 81.2 67.4 76.3 81.2	1.4 69.5	64.0 67.2	72.3 66.7	56.5 57.	0 67.5 55	.6 54.6 5	8.0 61.1	62 69	134 148	289 318
SR-52 to West Hills Parkway, Near Term + 50 % project SR-52 to West Hills Parkway, Near Term + project	4	25 25	34,015 37,300	40 40	0.5	3.0% 3.0%	2.0% 2.0%	72 73 73 78	168	340 362	733 780	50 50		4,320 3,26 4,737 3,58		606 665	52 1 57 2	19 77 21 84		67.4 76.3 81.2 67.4 76.3 81.2								73 78	158 168	340 362
st Boulevard	4	25	34,165	40	0.5	3.0%	2.0%	73 74		341	735	50	0	0 0	0	0	0	1 <u>9 77</u> 0 0	0 #		#### ####	****	#### ####	#### ###	# #### ###	## #### #	#### #####	74	158	341
West Hills Parkway to Medina Drive, existing West Hills Parkway to Medina Drive, existing + construction West Hills Parkway to Medina Drive. Near Term	4	15 15 15	19,540 19,690 22,962	40 40 40	0.5 0.5 0.5	3.0% 3.0% 3.0%	2.0% 2.0% 2.0%	70 - 70 - 70 52	101 101 112	217 218 241	467 469 520	50 50 50	15,299	2,501 1,89	0 516	351	30 1	11 44 11 44 13 52	32	67.4 76.3 81.2 67.4 76.3 81.2 67.4 76.3 81.2	0.9 67.7	62.2 65.4	70.4 64.8	54.6 55.	2 65.6 53	.8 52.7 5	6.1 59.2	47 47 52	101 101 112	217 218 241
West Hills Parkway to Medina Drive, Near Term + 50 % project West Hills Parkway to Medina Drive, Near Term + project	4 4	15	27,692 32,422	40 40 40	0.5	3.0%	2.0%	70 52 71 59 72 65	127	241 273 304	589	50 50	21,517	3,517 2,65	8 726	493	42 1	16 62 18 73	45	67.4 76.3 81.2 67.4 76.3 81.2 67.4 76.3 81.2	0.9 69.2	63.7 66.8	71.9 66.3	56.1 56.	7 67.1 55	.2 54.2 5	7.6 60.7	59 65	127	273
West Hills Parkway to Medina Driv, Near Term + 50% project + c st Boulevard	4	15	27,842	40	0.5	3.0%	2.0%	71 59		274	591		21,633 0					16 63 0 0		67.4 76.3 81.2								59 0	127 0	274
Pebble Beach Drive to Fanita Parkway, existing Pebble Beach Drive to Fanita Parkway, existing + construction	4 4	15 15	19,590 19,740	40 40	0.5 0.5	3.0% 3.0%	2.0% 2.0%	70 - 70 -	101 101	217 218	467 470	50 50	15,338	2,507 1,89	5 518	352	30 1	11 44 11 45	32	67.4 76.3 81.2 67.4 76.3 81.2	0.9 67.7	62.2 65.4	70.4 64.8	54.6 55.	2 65.6 53	.8 52.8 5	6.1 59.2	47 47	101 101	217 218
Pebble Beach Drive to Fanita Parkway, Near Term Pebble Beach Drive to Fanita Parkway, Near Term + 50 % projec	4 4	15 15	21,361 26,091	40 40	0.5 0.5	3.0% 3.0%	2.0% 2.0%	70 - 71 57		230 263	495 566	50 50	20,273	2,713 2,05 3,314 2,50	5 684	465	40 1	12 48 15 59	42	67.4 76.3 81.2 67.4 76.3 81.2	0.9 68.9	63.4 66.6		55.8 56.	4 66.9 55	.0 54.0 5	7.4 60.4	50 57	107 122	230 263
Pebble Beach Drive to Fanita Parkway, Near Term + project Pebble Beach Drive to Fanita Parkway, Near Term + 50% projec sion Gorge Road	4	15 15	30,821 26,241	40 40	0.5	3.0% 3.0%	2.0% 2.0%	72 63 71 57		294 264	632 568	50 50		3,914 2,95 3,333 2,51 0 0		549 468 0	40 1	18 70 15 59 0 0	42	67.4 76.3 81.2 67.4 76.3 81.2	0.9 69.0	63.4 66.6	71.7 66.1	55.9 56.	4 66.9 55	.0 54.0 5	7.4 60.5	63 57 0	136 122 0	294 264
ston Gorge Road SR-125 to Fanita Drive, existing SR-125 to Fanita Drive, existing + construction	6	15 15	45,440 45,590	45 45	0.5 0.5	5.0% 5.0%	3.0% 3.0%	77 15 77 15		699 701	1,507 1,510	50 50	35,307	5,771 4,36 5,790 4.37	2 1,986	1,215	115 3	39 171 39 171	110	69.3 77.6 82.1 69.3 77.6 82.1	2.6 74.4	70.6 72.9	77.7 71.6	63.0 62.	8 72.6 62	.8 61.1 6	3.7 67.4	151 151	325 325	699 701
SR-125 to Fanita Drive, Near Term SR-125 to Fanita Drive, Near Term + 50 % project	6	15 15	48,026 50,916	45 45	0.5	5.0% 5.0%	3.0% 3.0%	77 15 78 16	337	726 755	1,563 1,626	50 50	37,316	6,099 4,61 6,466 4,88	0 2,099	1,284	121 4		116	69.3 77.6 82.1 69.3 77.6 82.1	2.6 74.6	70.8 73.2	77.9 71.8	63.2 63.	0 72.9 63	.1 61.3 6	3.9 67.7	156 163	337 350	726 755
SR-125 to Fanita Drive, Near Term + project SR-125 to Fanita Drive, Near Term + 50% project + construction	6 6	15 15	53,806 51,066	45 45	0.5 0.5	5.0% 5.0%	3.0% 3.0%	78 16 78 16		783 756	1,686 1,629	50 50	41,807 39,678	6,485 4,90	2 2,232			46 202 44 192	123	69.3 77.6 82.1 69.3 77.6 82.1	2.6 74.9	71.1 73.4	78.2 72.1	63.5 63.	3 73.1 63	.3 61.6 6	4.2 68.0	169 163	363 351	783 756
ssion Gorge Road Fanita Drive to Carlton Hills Boulevard, existing	6	15	41,100	45	0.5	5.0%	3.0%	77 14		654	1,409	50		0 0 0 5,220 3,94			104 3	0 0 35 155	99	69.3 77.6 82.1	2.6 73.9	70.1 72.5	77.2 71.2	62.5 62.	3 72.2 62	.4 60.7 6		0 141	0 304	0 654
Fanita Drive to Carlton Hills Boulevard, existing + construction Fanita Drive to Carlton Hills Boulevard, Near Term	6 6 6	15 15	41,250 43,029	45 45	0.5	5.0% 5.0%	3.0% 3.0%	77 14 77 14 77 15	5 313	656 674 708	1,413 1,453	50 50	33,434	5,465 4,13		1,150	109 3	35 155 37 162 39 174	104	69.3 77.6 82.1 69.3 77.6 82.1	2.6 74.1	70.3 72.7	77.4 71.4	62.7 62.	5 72.4 62	.6 60.9 6	3.5 67.2	141 145	304 313 329	656 674 708
Fanita Drive to Carlton Hills Boulevard, Near Term + 50 % projec Fanita Drive to Carlton Hills Boulevard, Near Term + project Fanita Drive to Carlton Hills Boulevard, Near Term + 50% project	6 6	15 15 15	46,314 49,599 46,464	45 45 45	0.5	5.0% 5.0% 5.0%	3.0% 3.0% 3.0%	77 15 78 16 77 15) 344	708 741 710	1,526 1,597 1,529	50 50 50	38,538	5,882 4,44 6,299 4,76 5,901 4,46	2 2,168	1,326	125 4	39 174 42 186 40 175	120	69.3 77.6 82.1 69.3 77.6 82.1 69.3 77.6 82.1	2.6 74.7	70.9 73.3	78.0 72.0	63.4 63.	2 73.0 63	.2 61.5 6	4.1 67.8	153 160 153	329 344 329	708 741 710
roject site to Ganley Drive, existing	2	15	DNE	40	0.5	2.0%	2.0%	#VALUE! #VAL					0	0 0	0	0	0	0 0	0 #	67.4 76.3 81.2	****	****	#### ####	#### ###	# #### ###	## #### #	#### #####	0	0	0
Project site to Ganley Drive, existing + construction Project site to Ganley Drive, Near Term	2	15 15	150 DNE	40 40	0.5 0.5	2.0% 2.0%	2.0% 2.0%	47 - #VALUE! #VAL	-	- E! #VALUE	- E! #VALUE	50 ! 50	####### #	19 14 ##### ####	un nnnnn	, """""""""	****		¥ ######	67.4 76.3 81.2 67.4 76.3 81.2	0.1 #####	<i></i>	#### ####	#### ###	# #### ###	## #### #	### #### #			
troject site to Ganley Drive, Near Term + 50 % project troject site to Ganley Drive, Near Term + project	2	15 15	6,175 12,350 6.325	40 40 40	0.5	2.0%	2.0% 2.0% 2.0%	63 - 66 - 64 -	- 62 40	84 134 86	182 289 185	50 50 50	9,596	784 593 1,568 1,18 803 607	6 216	110 220 113	6 4 12	4 9 7 19 4 10	20	67.4 76.3 81.2 67.4 76.3 81.2 67.4 76.3 81.2	0.1 65.0	57.7 62.6	67.5 62.1	50.1 52.	4 62.8 49	.1 48.2 5	3.4 55.6	18 29 18	39 62 40	84 134 86
roject site to Ganley Drive, Near Term + 50% project + construc ta Parkway ianley Drive to Lake Canyon Road, existing	2	15	2.610	40	0.5	2.0%	2.0%	59 -	40	46	99	50	0	803 607 0 0 331 251	0	113 0 47	0 1	4 10 0 0	0 #	67.4 76.3 81.2 #### #### #### 67.4 76.3 81.2	#### ####	****	#### ####	#### ###	# #### ###	## #### #	### ####	18 0 10	40 0 21	86 0 46
anley Drive to Lake Canyon Road, existing anley Drive to Lake Canyon Road, existing + construction anley Drive to Lake Canyon Road, Near Term	3	14 0	2,760	40 50 40	0.5	2.0%	2.0%	62 - 60 -	-	40 69 48	150 104	50 50	2,145	351 265 353 267	48	47 49 50		2 4	4	71.1 78.8 83.0 67.4 76.3 81.2	0.4 61.5	52.9 57.2	63.3 58.6	45.4 47.	1 59.1 45	6 43.5 4	8.0 50.9	15 10	32 22	40 69 48
anley Drive to Lake Canyon Road, Near Term + 50 % project anley Drive to Lake Canyon Road, Near Term + project	3	14	8,957	50	0.5	2.0%	2.0%	67 - 70 47	71	152	328	50		1,138 860	157	160 270	9	5 13 9 23	14	71.1 78.8 83.0 71.1 78.8 83.0	0.4 66.7	58.1 62.4	68.4 63.7	50.5 52.	2 64.2 50	.7 48.6 5	3.1 56.0	33	71	152
anley Drive to Lake Canyon Road, Near Term + 50% project + a Parkway	3	14	9,107	50	0.5	2.0%	2.0%	67 -	71	154	332	50	7,076 0	1,157 874 0 0	159 0	162 0	9	5 14 0 0		71.1 78.8 83.0								33 0	71 0	154 0
ike Canyon Road to Mast Boulevard, existing ike Canyon Road to Mast Boulevard, existing + construction	2 4	0 14	3,860 4,010	40 50	0.5 0.5	2.0% 2.0%	2.0% 2.0%	61 - 64 -	-	60 95	129 205	50 50	3,116	490 371 509 385	70	69 71	4	26 26	6	67.4 76.3 81.2 71.1 78.8 83.0	0.8 63.6	55.0 59.3	65.4 60.7	47.4 49.	1 61.2 47	.7 45.5 5	0.1 52.9	13 20	28 44	60 95
ke Canyon Road to Mast Boulevard, Near Term ke Canyon Road to Mast Boulevard, Near Term + 50 % projec	2	0 14 14	4,158 9,808	40 50	0.5	2.0%	2.0%	61 - 68 -	- 80	63 173	135 372 504	50 50	7,621	528 399 1,246 942 1,963 1,48	172	74 175 275	4 : 10 1	2 6 6 15 9 23	16	67.4 76.3 81.2 71.1 78.8 83.0 71.1 78.8 83.0	0.8 67.5	58.9 63.2	69.3 64.6	51.3 53.	0 65.0 51	.6 49.4 5	3.9 56.8	14 37 50	29 80	63 173
ake Canyon Road to Mast Boulevard, Near Term + project ake Canyon Road to Mast Boulevard, Near Term + 50% project a Parkway	4	14	15,458 9,958	50 50	0.5 0.5	2.0% 2.0%	2.0% 2.0%	70 - 68 -	109 81	234 174	376	50 50				177	10 1	9 23 6 15 0 0	16	71.1 78.8 83.0 71.1 78.8 83.0	0.8 67.5	58.9 63.3	69.3 64.6	51.4 53.	1 65.1 51	.6 49.5 5	64.0 56.9	38	109 81	234 174 0
last Boulevard to Carlton Oaks Drive, existing last Boulevard to Carlton Oaks Drive, existing + construction	2 2	0	3,330 3.480	35 35	0.5 0.5	2.0% 2.0%	1.0% 1.0%	58 - 59 -	-	39 40	84 86	50 50	2,587	423 320 442 334		30 31	3 4	1 5 1 5	3	65.1 74.8 80.0 65.1 74.8 80.0	-0.1 57.5	50.9 53.2	59.5 54.5	43.3 43.	0 55.1 41	.7 41.4 4	3.9 47.3	8	18 19	39 40
last Boulevard to Carlton Oaks Drive, Near Term last Boulevard to Carlton Oaks Drive, Near Term + 50 % projec	2	0	3,713 5,423	35 35	0.5	2.0%	1.0% 1.0%	59 - 60 -	-	42 54	90 116	50 50	2,885	472 356 689 521	65	33 48	4 5	1 6 2 8	3		-0.1 58.0	51.4 53.6	60.0 55.0	43.8 43.	5 55.6 42	.2 41.9 4	4.4 47.8	9 12	19 25	42 54
Mast Boulevard to Carlton Oaks Drive, Near Term + project Mast Boulevard to Carlton Oaks Drive, Near Term + 50% project	2	0	7,133 5,573	35 35	0.5 0.5	2.0% 2.0%	1.0%	62 - 61 -	-	65 55	139 118	50 50		906 685 708 535	97	64 50	7 : 6 :	2 11 2 8	4	65.1 74.8 80.0 65.1 74.8 80.0	-0.1 59.7	53.1 55.4	61.7 56.8	45.5 45.	2 57.4 44	.0 43.7 4	6.2 49.5	14 12	30 25	65 55
Iton Hills Boulevard Carlton Oaks Drive to Mission Gorge Road, existing	4	0	24,960 25,110	35 35	0.5 0.5	3.0% 3.0%	2.0% 2.0%	69 -	92 93	199 200	428 430	50 50		0 0 3,170 2,39 3.189 2.41				0 0 14 56 14 57	40	#### #### #### 65.1 74.8 80.0 65.1 74.8 80.0	0.3 66.5	61.8 65.3	69.7 63.7	54.2 55.	2 64.6 52	.6 52.3 5	6.1 58.8	0 43 43	0 92 93	0 199 200
Carlton Oaks Drive to Mission Gorge Road, existing + constructic Carlton Oaks Drive to Mission Gorge Road, Near Term Carlton Oaks Drive to Mission Gorge Road, Near Term + 50 % p	4	0 0 0	25,993 28,228	35 35 35	0.5	3.0% 3.0% 3.0%	2.0% 2.0% 2.0%	69 - 69 - 70 46	93 95 100	200 204 216	430 440 465	50 50	20,197		5 682	463	39 1	14 57 15 59 16 64	42	65.1 74.8 80.0 65.1 74.8 80.0 65.1 74.8 80.0	0.3 66.7	62.0 65.5	69.9 63.8	54.4 55.	3 64.8 52	.8 52.5 5	6.3 59.0	43 44 46	93 95 100	200 204 216
	4 4	0	30,463	35	0.5	3.0%	2.0%	70 49 70 49		210	489	50 50		3,869 2,92 3,604 2,72				17 69 16 64		65.1 74.8 80.0 65.1 74.8 80.0								49	105	210
te Route 52 Santo Road to Mast Boulevard, existing	6	60	96,000	65	0.5	2.0%	0.6%	76 24		1,143		100	,	0 0	,			0 0 16 144	46	75.5 81.7 85.2	-3.2 76.7	66.6 64.9	77.4 73.8	59.0 54.	7 74.0 61	.1 57.1 5	5.7 63.3	0 246	0 531	0 1143
Santo Road to Mast Boulevard, existing + construction Santo Road to Mast Boulevard, Near Term	6	60 60	96,150 104,092	65 65	0.5	2.0%	0.6%	76 24 76 26	560	1,144 1,206	2,599	100	80,879 1	2,211 9,23 3,220 9,99	3 1,820	556	105 1	16 145 18 157	50	75.5 81.7 85.2 75.5 81.7 85.2	-3.2 77.1	66.9 65.3	77.7 74.1	59.3 55.	1 74.3 61	.4 57.5 5	6.0 63.7	247 260	531 560	1144 1206
anto Road to Mast Boulevard, Near Term + 50 % project anto Road to Mast Boulevard, Near Term + project anto Road to Mast Boulevard. Near Term + 50% project + cons	6	60 60 60	109,079 114,066 109,229	65 65 65	0.5	2.0% 2.0% 2.0%	0.6% 0.6% 0.6%	76 26 77 27 76 26	595	1,245 1,282 1,246	2,762	100		3,853 10,47 4,486 10,95	50 1,995	610	115 1	19 164 19 172 19 164	55	75.5 81.7 85.2 75.5 81.7 85.2 75.5 81.7 85.2	-3.2 77.5	67.3 65.7	78.1 74.5	59.7 55.	5 74.7 61	.8 57.9 5	6.4 64.1	268 276 268	578 595 578	1245 1282 1246
amaca Street roject Site to Magnolia Avenue, existing	2	10	DNE	40	0.5	2.0%	2.0%	#VALUE! #VAL					0	0 0	0	0	0	0 0	0 #	73.5 81.7 85.2 #### #### #### 67.4 76.3 81.2	****	****	#### ####	#### ###	# #### ###	## #### #	#### #####	0	0	0
roject Site to Magnolia Avenue, existing + project Project Site to Magnolia Avenue, Near Term	2	10 10	13,920 DNE	40 40	0.5	2.0%	2.0% 2.0%	67 - #VALUE! #VAL	66	143	309	50	10,816	1,768 1,33 ##### ####				8 21	22	67.4 76.3 81.2 67.4 76.3 81.2	0.1 65.4	58.1 63.0	67.9 62.5	50.5 52.	9 63.2 49	.5 48.7 5	3.8 56.0	31	66	143
roject Site to Magnolia Avenue, Near Term + 50% project roject Site to Magnolia Avenue, Near Term + Project	2 2	10 10	6,960 13,920	40 40	0.5	2.0% 2.0%	2.0% 2.0%	<u>64</u> - 67 -	42 66	90 143	194 309	50 50	10,816		6 243	248		4 10 8 21	22	67.4 76.3 81.2 67.4 76.3 81.2	0.1 65.4	58.1 63.0	67.9 62.5	50.5 52.	9 63.2 49	.5 48.7 5	3.8 56.0	19 31	42 66	90 143
roject Site to Magnolia Avenue, Near Term + 50% project + con maca Street	2	10	7,110	40	0.5	2.0%	2.0%	64 -	42	92	197	50	0	0 0	0	0	0 0	4 11 0 0	0 #	67.4 76.3 81.2	#### ####	****	#### ####	#### ###	# ##### ###	## #### #	#### #####	20	42 0	92 0
lagnolia Avenue to Princess Joann Road, existing lagnolia Avenue to Princess Joann Road, existing + project lagnolia Avenue to Princess Joann Road, Near Term	2	10 10 10	DNE 7,620 DNE	40 40 40	0.5 0.5 0.5	2.0% 2.0% 2.0%	2.0% 2.0% 2.0%	#VALUE! #VAL 64 - #VALUE! #VAL	44	96	206	50	5,921	968 732	133	136	8	4 11	12	67.4 76.3 81.2 67.4 76.3 81.2 67.4 76.3 81.2	0.1 62.8	55.5 60.4	65.3 59.9	47.9 50.	3 60.6 46	.9 46.0 5	1.2 53.4	21	44	96
lagnolia Avenue to Princess Joann Road, Near Term + 50% prc lagnolia Avenue to Princess Joann Road, Near Term + Project	2	10 10	3,810	40 40	0.5	2.0%	2.0%	<u>61</u> - 64 -	- 44	60 96	130	50 50	2,960	484 366	67		4	2 <u>6</u> 4 11	6	67.4 76.3 81.2 67.4 76.3 81.2 67.4 76.3 81.2	0.1 59.8	52.5 57.4	62.3 56.9	44.9 47.	2 57.6 43	.9 43.0 4	8.2 50.4	13 21	28	60 96
lagnolia Avenue to Princess Joann Road, Near Term + 50% pro	2	10	3,960	40	0.5	2.0%	2.0%	61 -	-	62	133	50	3,077	503 380 0 0		71	4	2 6 0 0	6	67.4 76.3 81.2	0.1 60.0	52.6 57.6	62.4 57.1	45.1 47.	4 57.7 44	.0 43.2 4	8.3 50.6	13	29	62
rincess Joann Road to Chaparral Drive, existing rincess Joann Road to Chaparral Drive, existing + project	2 2	10 10	DNE 7,620	40 40	0.5 0.5	2.0% 2.0%	2.0% 2.0%	#VALUE! #VAL 64 -	44	96	206	50	5,921	968 732	133	136		4 11	12	67.4 76.3 81.2 67.4 76.3 81.2	0.1 62.8	55.5 60.4	65.3 59.9	47.9 50.	3 60.6 46	.9 46.0 5	51.2 53.4	21	44	96
rincess Joann Road to Chaparral Drive, Near Term rincess Joann Road to Chaparral Drive, Near Term + 50% proje	2	10 10	DNE 3,810	40 40	0.5	2.0% 2.0%	2.0% 2.0% 2.0%	#VALUE! #VAL 61 -	-	60	130	50	2,960	484 366	67	68	4	26	6	67.4 76.3 81.2 67.4 76.3 81.2	0.1 59.8	52.5 57.4	62.3 56.9	44.9 47.	2 57.6 43	.9 43.0 4	8.2 50.4	13	28	60
rincess Joann Road to Chaparral Drive, Near Term + Project rincess Joann Road to Chaparral Drive, Near Term + 50% proje maca Street	2	10 10	7,620 3,960	40 40	0.5 0.5	2.0%	2.0%	64 - 61 -	44	96 62	206 133	50 50		968 732 503 380 0 0	69	136 71 0	4	4 11 2 6 0 0	6	67.4 76.3 81.2 67.4 76.3 81.2	0.1 60.0	52.6 57.6	62.4 57.1	45.1 47.	4 57.7 44	.0 43.2 4	8.3 50.6	21 13 0	44 29 0	96 62 0
ihaparral Drive to Woodglen Vista Drive, existing haparral Drive to Woodglen Vista Drive, existing + project	2	40 16	670 8.290	35 50	0.5 0.5	3.0% 3.0%	2.0% 2.0%	54 - 68 -	- 77	- 167	- 359	50 50	521	85 64 1.053 796	18	12 148	1 0	0 0 0 2 5 19	1	65.1 74.8 80.0 71.1 78.8 83.0	0.9 51.4	46.7 50.2	54.6 48.5	39.1 40.	0 49.5 37	.4 37.2 4	1.0 43.7	4	9 77	19 167
haparral Drive to Woodglen Vista Drive, Near Term haparral Drive to Woodglen Vista Drive, Near Term + 50% proj	2	40 16	683 4,493	35 50	0.5	3.0% 3.0%	2.0% 2.0%	54 - 65 -	-	111	239	50 50	531	87 66 571 431	18	12 80		0 2 3 10	1	65.1 74.8 80.0 71.1 78.8 83.0	0.9 51.5	46.7 50.3	54.7 48.6	39.2 40.	1 49.6 37	.5 37.3 4	1.0 43.8	4 24	9 51	20 111
haparral Drive to Woodglen Vista Drive, Near Term + Project haparral Drive to Woodglen Vista Drive, Near Term + 50% proj	4 4	16 16	8,303 4,643	50 50	0.5 0.5	3.0% 3.0%	2.0% 2.0%	68 - 65 -	77 53	167 113	359 244	50 50		1,054 797 590 446		148 83	13 : 7 :	5 19 3 10	7	71.1 78.8 83.0 71.1 78.8 83.0	0.9 64.3	57.5 60.0	66.3 61.4	49.9 49.	9 62.0 50	.3 48.0 5	0.8 54.6	36 24	77 53	167 113
imaca Street /oodglen Vista Drive to El Nopal, existing	2	40	4,360	35	0.5	3.0%	2.0%	62 -		68	146	50		0 0 554 419		0 78		0 0 2 10	7	65.1 74.8 80.0	0.9 59.5	54.8 58.3	62.7 56.6	47.2 48.	2 57.6 45	.6 45.3 4	9.1 51.8	0 15	0 31	0 68
oodglen Vista Drive to El Nopal, existing + project oodglen Vista Drive to El Nopal, Near Term oodglen Vista Drive to El Nopal, Near Term + 50% project	4 2 4	16 40 16	11,980 4,472 8,282	50 35 50	0.5 0.5 0.5	3.0% 3.0% 3.0%	2.0% 2.0% 2.0%	69 - 62 - 68 -	99 - 77	213 69 166	459 149 359	50 50 50	3,475	1,521 1,15 568 429 1.052 795	117	213 80 148	18 7 13	7 27 3 10 5 19	7	71.1 78.8 83.0 65.1 74.8 80.0 71.1 78.8 83.0		54.9 58.4	62.9 56.8	47.3 48.	3 57.7 45	.7 45.4 4	9.2 51.9	46 15 36	99 32 77	213 69 166
oodglen Vista Drive to El Nopal, Near Term + 50% project oodglen Vista Drive to El Nopal, Near Term + Project oodglen Vista Drive to El Nopal, Near Term + 50% project + cc	4	16 16 16	8,282 12,092 8,432	50 50 50	0.5	3.0% 3.0%	2.0% 2.0% 2.0%	69 - 68 -	99 78	214	462 363	50 50	9,395	1,536 1,16	1 317	215	18	5 19 7 27 5 19	19		0.9 68.4	61.6 64.2	70.4 65.5	54.1 54.	0 66.1 54	.5 52.2 5	64.9 58.8	46 36	99 78	214
Imaca Street I Nopal to Mast Boulevard, existing	3	30	8,860	35	0.5	3.0%	2.0%	65 -	-	110	238	50	0	0 0 1,125 851	0	0	0	0 0 5 20	0 #	#### #### #### 65.1 74.8 80.0	#### ####	****	#### ####	#### ###	# #### ###	## #### #	### ####	0 24	0 51	0
Nopal to Mast Boulevard, existing + project Nopal to Mast Boulevard, Near Term	4 3	16 30	16,480 9,173	50 35	0.5 0.5	3.0% 3.0%	2.0% 2.0%	71 57 65 -	-	263 113	567 244	50 50	12,805 7,127	2,093 1,58 1,165 881	2 432 241	294 163	25 14	9 37 5 21	27 15	71.1 78.8 83.0 65.1 74.8 80.0	0.9 69.8 1.0 62.9	63.0 65.5 58.1 61.7	71.8 66.9 66.1 60.0	55.4 55. 50.5 51	4 67.5 55 5 61.0 48	.8 53.5 5 .9 48.7 5	6.3 60.1 2.4 55.1	57 24	122 52	263 113
Nopal to Mast Boulevard, Near Term + 50% project Nopal to Mast Boulevard, Near Term + Project	4	16 16	12,983 16,793	50 50	0.5	3.0% 3.0%	2.0% 2.0%	70 - 71 57		225 267	484 575	50 50	13,048		2 440	299		7 29	27	71.1 78.8 83.0 71.1 78.8 83.0	0.9 69.9	63.1 65.6	71.9 67.0	55.5 55.	4 67.5 55	.9 53.6 5	6.4 60.2	48	104 124	225 267
I Nopal to Mast Boulevard, Near Term + 50% project + construc amaca Street	4	16	13,133	50	0.5	3.0%	2.0%	- 70 -	105	226	488	50	0	0 0	0	0		7 <u>30</u> 0 0	0 #	71.1 78.8 83.0	#### ####	****	#### ####	#### ###	# #### ###	## #### #	### ####	49 0 40	105 0	226 0
last Boulevard to River Park Drive, existing last Boulevard to River Park Drive, existing + project last Boulevard to River Park Drive. Near Term	4	15 15 15	19,600 25,380 20,527	35 35 35	0.5 0.5 0.5	3.0% 3.0% 3.0%	2.0% 2.0% 2.0%	68 - 70 - 69 -	85 101 88	184 218 189	395 470 408	50 50 50	19,720	3,223 2,43	6 666	452	38 1	11 44 14 57 12 46	41	65.1 74.8 80.0 65.1 74.8 80.0 65.1 74.8 80.0	0.9 67.1	62.4 65.9	70.3 64.3	54.8 55.	8 65.2 53	.2 52.9 5	6.7 59.4	40 47 41	85 101 88	184 218 189
ast Boulevard to River Park Drive, Near Term ast Boulevard to River Park Drive, Near Term + 50% project ast Boulevard to River Park Drive, Near Term + Project	4 4	15 15 15	20,527 23,417 26,307	35 35 35	0.5	3.0% 3.0% 3.0%	2.0% 2.0% 2.0%	69 - 69 - 70 -	96 104	189 207 223	408 445 481	50 50 50	18,195		8 614	417	35 1	12 46 13 53 15 59	38	65.1 74.8 80.0 65.1 74.8 80.0 65.1 74.8 80.0	0.9 66.8	62.0 65.6	70.0 63.9	54.5 55.	4 64.9 52	.8 52.6 5	6.3 59.1	41 45 48	96 104	189 207 223
Mast Boulevard to River Park Drive, Near Term + 50% project +	4	15	23,567	35	0.5	3.0%	2.0%	69 -	96	208	447	50					36 1	13 53 0 0	38	65.1 74.8 80.0	0.9 66.8	62.1 65.6	70.0 63.9	54.5 55.	4 64.9 52	.9 52.6 5	6.4 59.1	45	96	208
River Park Drive to Town Center Parkway, existing River Park Drive to Town Center Parkway, existing + project	4 4	15 15	26,690 32,210	35 35	0.5 0.5	3.0% 3.0%	2.0% 2.0%	70 - 71 55	105 119	225 256	486 551	50 50	20,738 25,027	3,390 2,56 4,091 3,09	2 700 2 845	476 574	40 1 49 1	15 60 18 73	43 52	65.1 74.8 80.0 65.1 74.8 80.0	0.9 67.4 0.9 68.2	62.6 66.2 63.4 67.0	70.6 64.5 71.4 65.3	55.0 56. 55.8 56.	0 65.5 53 8 66.3 54	.4 53.2 5 .2 54.0 5	6.9 59.6 7.7 60.4	49 55	105 119	225 256
River Park Drive to Town Center Parkway, Near Term River Park Drive to Town Center Parkway, Near Term + 50% pro	4	15 15	28,084 30,844	35 35	0.5 0.5	3.0% 3.0%	2.0% 2.0%	70 - 70 53	108 115	233 248	503 535	50 50	23,966	3,917 2,96	1 809	550	47 1	16 63 18 70	50	65.1 74.8 80.0 65.1 74.8 80.0	0.9 68.0	63.2 66.8	71.2 65.1	55.7 56.	6 66.1 54	.0 53.8 5	7.5 60.3	50 53	108 115	233 248
iver Park Drive to Town Center Parkway, Near Term + Project iver Park Drive to Town Center Parkway, Near Term + 50% pro	4 4	15 15	33,604 30,994	35 35	0.5 0.5	3.0% 3.0%	2.0% 2.0%	71 57 70 54		263 249	566 537	50 50		4,268 3,22 3,936 2,97	5 813		47 1	19 76 18 70	50	65.1 74.8 80.0 65.1 74.8 80.0	0.9 68.0	63.3 66.8	71.2 65.1	55.7 56.	6 66.1 54	.1 53.8 5	7.6 60.3	57 54	122	263 249
ramaca Street Town Center Parkway to Mission Gorge Road, existing	6	15	21,850	35	0.5	5.0%	3.0%	72 68	147	317	684	50	U 16,977	0 0 2,775 2,09	0 8 955	U 584	0 (55 1	0 0 19 82		#### #### #### 65.1 74.8 80.0								0 68	0 147	0 317

 P1
 F1
 F2
 F2
 F3
 F3<
 uyanaca Street
 5

 Town Center Parkway to Mission Gorge Road, existing
 6

 Town Center Parkway to Mission Gorge Road, existing + projet
 6

 Town Center Parkway to Mission Gorge Road, Near Term
 6

 Town Center Parkway to Mission Gorge Road, Near Term
 5

 Town Center Parkway to Mission Gorge Road, Near Term + 50%
 6

 Town Center Parkway to Mission Gorge Road, Near Term + 50%
 6

 Agnola Avenue
 1

 Cuyamaca Street to Princes Joann Road, existing project
 2

 Cuyamaca Street to Princes Joann Road, existing project
 2

 Cuyamaca Street to Princes Joann Road, Near Term + 50% pr
 2

 Cuyamaca Street to Princes Joann Road, Near Term + 50% pr
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 Cuyamaca Street to Princes Joann Road, Near Term + 50% pr
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 Cuyamaca Street to Princes Joann Road, Near Term + 50% pr
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 Cuyamaca Street to Princes Joann Road, Near Term + 50% pr
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 Cuyamaca Street to Princes Joann Road, Near Term + Project
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 Cuyamaca Street to Princes Joann Road, Near Term + Project
 2
 0.5 0.5 0.5 0.5 0.5 0.5 0.5 21,850 26,840 24,245 26,740 29,235 5.0% 5.0% 5.0% 5.0% 5.0% 5.0% 15 15 15 15 35 35 35 35 26,890 DNE 6,310 DNE 3,155 6,310 3.0% 3.0% 3.0% 3.0% 3.0% 15 15 15 35 35 35 0.5 0.5 0.5 0.5

Cuyamaca Street to Princess Joann Road, Near Term + Project	:t· 2	15	3,305	35	0.5	3.0%	2.0%	60	-	-	50	108	50	2,568	420	317	87	59	5	2	7	5	65.1 74.4	8 80.0	D.1 57.	6 52.8	56.3 60.	8 54.7	45.2 46.	2 55.7	43.6 43.4 4	47.1 49.8	11	23	50	108
Magnolia Avenue														0	0	0	0	0	0	0	0										#### #### #		0	0	0	0
Princess Joann Road to Woodglen Vista Drive, existing	4	15	2,020	40	0.5	3.0%	2.0%	60	-	-	-	103	50	1,570	257	194	53	36	3	1	5	3	67.4 76.3	3 81.2	0.9 57.	8 52.3	55.5 60.	5 54.9	44.7 45.	.3 55.7	43.9 42.9 4	46.2 49.3	10	22	48	103
Princess Joann Road to Woodglen Vista Drive, existing + proje	ct 4	15	8,330	40	0.5	3.0%	2.0%	66	-	57	123	264	50	6,472	1,058	800	218	148	13	5	19										50.0 49.0 5		26	57	123	264
Princess Joann Road to Woodglen Vista Drive, Near Term	4	15	2,204	40	0.5	3.0%	2.0%	60	-	-	-	109	50	1,713	280	212	58	39	3	1	5	4	67.4 76.3	3 81.2	0.9 58.	2 52.7	55.9 60.	9 55.3	45.1 45.	.7 56.1	44.2 43.2 4	46.6 49.7	11	23	51	109
Princess Joann Road to Woodglen Vista Drive, Near Term + 5	09 4	15	5,359	40	0.5	3.0%	2.0%	64	-	-	91	197	50	4,164	681	514	141	95	8	3	12	9	67.4 76.3	3 81.2	0.9 62.	1 56.5	59.7 64.	8 59.2	49.0 49.	.5 60.0	48.1 47.1 5	50.5 53.6	20	42	91	197
Princess Joann Road to Woodglen Vista Drive, Near Term + P	roj 4	15	8,514	40	0.5	3.0%	2.0%	66	-	58	125	268	50	6,615	1,081	817	223	152	13	5	19	14	67.4 76.3	3 81.2	0.9 64.	1 58.6	61.7 66.	8 61.2	51.0 51.	.6 62.0	50.1 49.1 5	52.5 55.6	27	58	125	268
Princess Joann Road to Woodglen Vista Drive, Near Term + 5	09 4	15	5,509	40	0.5	3.0%	2.0%	64	-	-	93	201	50	4,280	700	529	144	98	8	3	12	9	67.4 76.3	3 81.2	0.9 62.	2 56.7	59.8 64.	9 59.3	49.1 49.	.7 60.1	48.2 47.2 5	50.6 53.7	20	43	93	201
Magnolia Avenue														0	0	0	0	0	0	0	0										#### #### #		0	0	0	0
Woodglen Vista Drive to El Nopal, existing	4	15	9,030	40	0.5	3.0%	2.0%	66	-	60	129	279	50	7,016	1,147	867	237	161	14	5	20	15	67.4 76.3	3 81.2	0.9 64.	3 58.8	62.0 67.	0 61.4	51.2 51.	.8 62.2	50.4 49.4 5	52.7 55.8	28	60	129	279
Woodglen Vista Drive to El Nopal, existing + project	4	15	15,340	40	0.5	3.0%	2.0%	69	-	86	184	397	50	11,919	1,948	1,473	402	273	23	9	35	25	67.4 76.3	3 81.2	0.9 66.	6 61.1	64.3 69.	3 63.7	53.5 54.	.1 64.5	52.7 51.7 5	55.0 58.1	40	86	184	397
Woodglen Vista Drive to El Nopal, Near Term	4	15	9,415	40	0.5	3.0%	2.0%	66	-	62	133	287	50	7,315	1,196	904	247	168	14	5	21	15	67.4 76.3	3 81.2	0.9 64.	5 59.0	62.2 67.	2 61.6	51.4 52.	.0 62.4	50.5 49.5 5	52.9 56.0	29	62	133	287
Woodglen Vista Drive to El Nopal, Near Term + 50% project	4	15	12,570	40	0.5	3.0%	2.0%	68	-	75	161	348	50	9,767	1,596	1,207	330	224	19	7	28	20	67.4 76.3	3 81.2	0.9 65.	8 60.2	63.4 68.	5 62.9	52.7 53.	2 63.7	51.8 50.8 5	54.2 57.3	35	75	161	348
Woodglen Vista Drive to El Nopal, Near Term + Project	4	15	15,725	40	0.5	3.0%	2.0%	69	-	87	187	404	50	12,218	1,997	1,510	412	280	24	9	35	25	67.4 76.3	3 81.2	0.9 66.	7 61.2	64.4 69.	4 63.8	53.6 54.	.2 64.7	52.8 51.8 5	55.2 58.2	40	87	187	404
Woodglen Vista Drive to El Nopal, Near Term + 50% project +	cc 4	15	12,720	40	0.5	3.0%	2.0%	68	-	76	163	351	50	9,883	1,615	1,221	334	227	19	7	29	21	67.4 76.3	3 81.2	0.9 65.	8 60.3	63.5 68.	5 62.9	52.7 53.	.3 63.7	51.9 50.8 5	54.2 57.3	35	76	163	351
Magnolia Avenue														0	0	0	0	0	0	0	0	0	#### ###	# #### #	### ###	# #### :	****	# #### 1	*### ###	######	****	<i>+####</i> #####	0	0	0	0
El Nopal to Mast Boulevard, existing	4	15	13,690	40	0.5	3.0%	2.0%	68	-	79	171	368	50	10,637	1,739	1,314	359	244	21	8	31	22	67.4 76.3	3 81.2	0.9 66.	1 60.6	63.8 68.	8 63.2	53.0 53.	.6 64.1	52.2 51.2 5	54.6 57.6	37	79	171	368
El Nopal to Mast Boulevard, existing + project	4	15	17,370	40	0.5	3.0%	2.0%	69	-	93	200	431	50	13,496	2,206	1,668	456	310	26	10	39	28	67.4 76.3	3 81.2	0.9 67.	2 61.7	64.8 69.	9 64.3	54.1 54.	.7 65.1	53.2 52.2 5	55.6 58.7	43	93	200	431
El Nopal to Mast Boulevard, Near Term	4	15	14,291	40	0.5	3.0%	2.0%	68	-	82	176	379	50	11,104	1,815	1,372	375	255	22	8	32	23	67.4 76.3	3 81.2	0.9 66.	3 60.8	64.0 69.	0 63.4	53.2 53.	.8 64.2	52.4 51.4 5	54.7 57.8	38	82	176	379
El Nopal to Mast Boulevard, Near Term + 50% project	4	15	16,131	40	0.5	3.0%	2.0%	69	-	88	191	411	50	12,534	2,049	1,549	423	287	24	9	36	26	67.4 76.3	3 81.2	0.9 66.	8 61.3	64.5 69.	5 64.0	53.7 54.	.3 64.8	52.9 51.9 5	55.3 58.4	41	88	191	411
El Nopal to Mast Boulevard, Near Term + Project	4	15	17,971	40	0.5	3.0%	2.0%	69	-	95	205	441	50	13,963	2,282	1,725	471	320	27	10	41	29	67.4 76.3	3 81.2	0.9 67.	3 61.8	65.0 70.	0 64.4	54.2 54.	.8 65.2	53.4 52.3 5	55.7 58.8	44	95	205	441
El Nopal to Mast Boulevard, Near Term + 50% project + constr	uc 4	15	16,281	40	0.5	3.0%	2.0%	69	-	89	192	413	50	12,650	2,068	1,563	427	290	25	9	37	26	67.4 76.3	3 81.2	D.9 66.	9 61.4	64.5 69.	6 64.0	53.8 54.	.4 64.8	52.9 51.9 5	55.3 58.4	41	89	192	413

Appendix E. FHWA Noise Prediction Model Results – Building Construction Worst-Case Scenario

TRAFFIC NOISE LEVELS AND NOISE CONTOURS

Project Number: 1501144001

Project Numb Project Nar	er: 150114 e: Fanita I		posed Proje	ct (with sch	ool)						
Background Information											
Model Description: Source of Traffic Volumes: Community Noise Descriptor:	Linscot	Highway Noi t, Law, and C L _m : X	Greenspan,	January 20		7-108) with	n California	Vehicle Noise (CA	ALVENO) Emit	ssion Leve	ls.
Assumed 24-Hour Traffic Distribution: Total ADT Volumes Medium-Duty Trucks		Day 77.70%	Evening 6 12.70% 6 5.05%	Night 9.60% 7.52%	-	Distance		ted within the road centerline of the ro ion.			
Heavy-Duty Trucks		ຮ 9.10%	⊍ ∠.84%			v	cle Mix	0:	from Centeri	ino of P	duc
Analysis Condition Roadway, Segment Mast Boulevard	Lane	Median s Width		Design Speed (mph)	Alpha Factor	Vehi Medium Trucks		Ldn at	Distance	ine of Ro e to Conto 60 Ld	Jr
Mast Boulevard SR-52 to West Hills Parkway, existing SR-52 to West Hills Parkway, existing + construction	4 4	25 25	26,440 27,851	40 40	0.5 0.5	3.0% 3.0%	2.0% 3.1%	71 63 72 73		288 335	620 723
SR-52 to West Hills Parkway, Near Term SR-52 to West Hills Parkway, Near Term + 50 % project SR-52 to West Hills Parkway, Near Term + project	4	25 25 25	30,730 34,015 37,300	40	0.5 0.5 0.5	3.0% 3.0% 3.0%	2.0% 2.0% 2.0%	72 69 72 73 73 74	3 158	318 340 362	685 733 780
SR-52 to West Hills Parkway, Near Term + 50% project + co Mast Boulevard		25	35,088	40	0.5	3.0%	2.7%	73 8	1 174	374	806
West Hills Parkway to Medina Drive, existing West Hills Parkway to Medina Drive, existing + construction West Hills Parkway to Medina Drive, Near Term	4 4 4	15 15 15	19,540 20,951 22,962	40 40 40	0.5 0.5 0.5	3.0% 3.0% 3.0%	2.0% 3.5% 2.0%	70 - 71 5 70 5		217 265 241	467 570 520
West Hills Parkway to Medina Driv, Near Term + 50 % proje- West Hills Parkway to Medina Drive, Near Term + project West Hills Parkway to Medina Driv, Near Term + 50% projec	4	15 15 15	27,692 32,422 28,765	40 40 40	0.5 0.5 0.5	3.0% 3.0% 3.0%	2.0% 2.0% 2.8%	71 55 72 65 72 66	9 127 5 141	273 304 306	589 654 660
Mast Boulevard Pebble Beach Drive to Fanita Parkway, existing	4	15	19,590	40	0.5	3.0%	2.0%	70 -	101	217	467
Pebble Beach Drive to Fanita Parkway, existing + construction Pebble Beach Drive to Fanita Parkway, Near Term Pebble Beach Drive to Fanita Parkway, Near Term + 50 % p	4	15 15 15	21,001 21,361 26.091	40 40 40	0.5 0.5 0.5	3.0% 3.0% 3.0%	3.5% 2.0% 2.0%	71 5 70 - 71 5	107	265 230 263	571 495 566
Pebble Beach Drive to Fanita Parkway, Near Term + project Pebble Beach Drive to Fanita Parkway, Near Term + 50% pr	4	15 15	30,821 27,164	40 40	0.5 0.5	3.0% 3.0%	2.0% 2.9%	72 63 72 64	3 136	294 296	632 638
Mission Gorge Road SR-125 to Fanita Drive, existing SR-125 to Fanita Drive, existing + construction	6 6	15 15	45,440 46,851	45 45	0.5 0.5	5.0% 5.0%	3.0% 3.7%	77 15 78 16	1 348	699 749	1,507 1,615
SR-125 to Fanita Drive, Near Term SR-125 to Fanita Drive, Near Term + 50 % project SR-125 to Fanita Drive, Near Term + project	6	15 15 15	48,026 50,916 53,806	45 45 45	0.5 0.5 0.5	5.0% 5.0% 5.0%	3.0% 3.0% 3.0%	77 15 78 16 78 16	3 350	726 755 783	1,563 1,626 1.686
SR-125 to Fanita Drive, Near Term + 50% project + construc Mission Gorge Road	ion 6	15	51,989	45	0.5	5.0%	3.5%	78 17	0 367	791	1,704
Fanita Drive to Carlton Hills Boulevard, existing Fanita Drive to Carlton Hills Boulevard, existing + construction Fanita Drive to Carlton Hills Boulevard, Near Term	6 1 6 6	15 15 15	41,100 42,511 43,029		0.5 0.5 0.5	5.0% 5.0% 5.0%	3.0% 3.7% 3.0%	77 14 77 15 77 14	2 328	654 706 674	1,409 1,521 1,453
Fanita Drive to Carlton Hills Boulevard, Near Term + 50 % p Fanita Drive to Carlton Hills Boulevard, Near Term + project	6	15 15	46,314 49,599	45 45	0.5	5.0% 5.0%	3.0% 3.0% 3.5%	77 15 78 16	3 329 0 344	708 741	1,526
Fanita Drive to Carlton Hills Boulevard, Near Term + 50% pr Fanita Parkway Project site to Ganley Drive, existing	2	15 15	47,387 DNE	45 40	0.5	5.0% 2.0%	2.0%		.UE! #VALUE		
Project site to Ganley Drive, existing + construction Project site to Ganley Drive, Near Term Project site to Ganley Drive, Near Term + 50 % project	2 2 2	15 15 15	1,411 DNE 6,175	40 40 40	0.5 0.5 0.5	2.0% 2.0% 2.0%	24.1% 2.0% 2.0%	64 - #VALUE! #VAL 63 -	41 .UE! #VALUE	87 E! #VALU 84	188 E! #VALU 182
Project site to Ganley Drive, Near Term + project Project site to Ganley Drive, Near Term + 50% project + con	2 truc 2	15 15 15	6,175 12,350 7,248		0.5	2.0% 2.0% 2.0%	2.0% 2.0% 5.2%	63 - 66 - 66 -	62 60	84 134 129	289 279
Fanita Parkway Ganley Drive to Lake Canyon Road, existing Ganley Drive to Lake Canyon Road, existing + construction	2	0 14	2,610 4,021	40 50	0.5 0.5	2.0% 2.0%	2.0% 9.8%	59 - 67 -	- 69	46 148	99 318
Ganley Drive to Lake Canyon Road, Near Term Ganley Drive to Lake Canyon Road, Near Term + 50 % proje	2 2 2 2	0 14	2,782 8,957	40 50	0.5 0.5	2.0% 2.0%	2.0% 2.0%	60 - 67 -	- 71	48 152	104 328
Ganley Drive to Lake Canyon Road, Near Term + project Ganley Drive to Lake Canyon Road, Near Term + 50% proje Fanita Parkway		14 14	15,132 10,030	50 50	0.5	2.0% 2.0%	2.0% 4.3%	70 4 69 -	7 100 93	216 200	465 430
Lake Canyon Road to Mast Boulevard, existing Lake Canyon Road to Mast Boulevard, existing + construction Lake Canyon Road to Mast Boulevard, Near Term	2 4 2	0 14 0	3,860 5,271 4,158	40 50 40	0.5 0.5 0.5	2.0% 2.0% 2.0%	2.0% 7.9% 2.0%	61 - 68 - 61 -	- 80 -	60 173 63	129 372 135
Lake Canyon Road to Mast Boulevard, Near Term + 50 % pr Lake Canyon Road to Mast Boulevard, Near Term + project	4	14 14	9,808 15,458	50 50	0.5 0.5	2.0% 2.0%	2.0% 2.0%	68 - 70 -	80 109	173 234	372 504
Lake Canyon Road to Mast Boulevard, Near Term + 50% pn Fanita Parkway Mast Boulevard to Carlton Oaks Drive, existing	2	14 0	10,881 3,330	50 35	0.5	2.0%	4.2% 1.0%	<u> </u>	- 103	222 39	478 84
Mast Boulevard to Carlton Oaks Drive, existing + constructio Mast Boulevard to Carlton Oaks Drive, Near Term Mast Boulevard to Carlton Oaks Drive, Near Term + 50 % pr	2	0	4,741 3,713 5,423	35 35 35	0.5 0.5 0.5	2.0% 2.0% 2.0%	7.6% 1.0% 1.0%	64 - 59 - 60 -	46	99 42 54	213 90 116
Mast Boulevard to Carlton Oaks Drive, Near Term + project Mast Boulevard to Carlton Oaks Drive, Near Term + 50% pro	2	0	7,133	35 35	0.5	2.0%	1.0%	62 - 64 -	45	65 97	139
Carlton Hills Boulevard Carlton Oaks Drive to Mission Gorge Road, existing Carlton Oaks Drive to Mission Gorge Road, existing + constr	4 Ictic 4	0	24,960 26,371	35 35	0.5 0.5	3.0% 3.0%	2.0% 3.2%	69 - 70 5	92 1 110	199 238	428 512
Carlton Oaks Drive to Mission Gorge Road, Near Term Carlton Oaks Drive to Mission Gorge Road, Near Term + 50	4 6p 4	0	25,993 28,228	35 35	0.5 0.5	3.0% 3.0%	2.0% 2.0%	69 - 70 44	95 6 100	204 216	440 465
Carlton Oaks Drive to Mission Gorge Road, Near Term + pro Carlton Oaks Drive to Mission Gorge Road, Near Term + 50 ate Route 52	ect 4 pr 4	0	30,463 29,301	35 35	0.5 0.5	3.0% 3.0%	2.0% 2.8%	70 49 70 53	3 113	227 244	489 526
Santo Road to Mast Boulevard, existing Santo Road to Mast Boulevard, existing + construction Santo Road to Mast Boulevard, Near Term	6 6	60 60 60	96,000 97,411 104.092	65 65 65	0.5 0.5 0.5	2.0% 2.0% 2.0%	0.6% 0.9% 0.6%	76 24 76 25 76 26	5 549	1,143 1,182 1,206	2,547
Santo Road to Mast Boulevard, Near Term + 50 % project Santo Road to Mast Boulevard, Near Term + project	6	60 60	109,079	65 65	0.5 0.5	2.0% 2.0%	0.6% 0.6%	76 26 77 27	8 578 6 595	1,245 1,282	2,681
nto Road to Mast Boulevard, Near Term + 50% project + (naca Street oject Site to Magnolia Avenue, Near Term	<u>2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 </u>	60 10	110,152 DNE	40	0.5	2.0%	0.8% 2.0%	77 27		1,273 ! #VALU	
roject Site to Magnolia Avenue, Near Term + 50% project roject Site to Magnolia Avenue, Near Term + Project roject Site to Magnolia Avenue, Near Term + 50% project +	2 2 con 2	10 10 10	6,960 13,920 8.033	40 40 40	0.5	2.0% 2.0% 2.0%	2.0% 2.0% 4.9%	64 - 67 - 66 -	42 66 62	90 143 133	194
uyamaca Street Magnolia Avenue to Princess Joann Road, Near Term	2	10	DNE	40	0.5	2.0%	2.0%	#VALUE! #VAL		! #VALU	E! #VALU
Magnolia Avenue to Princess Joann Road, Near Term + 50% Magnolia Avenue to Princess Joann Road, Near Term + Pro Magnolia Avenue to Princess Joann Road, Near Term + 50%	ect 2	10 10 10	3,810 7,620 4,883	40 40 40	0.5 0.5 0.5	2.0% 2.0% 2.0%	2.0% 2.0% 6.8%	61 - 64 - 65 -	- 44 51	60 96 110	130 206 237
uyamaca Street Princess Joann Road to Chaparral Drive, Near Term Princess Joann Road to Chaparral Drive, Near Term + 50%	2	10 10	DNE 3.810	40	0.5	2.0%	2.0%	#VALUE! #VAL			
Princess Joann Road to Chaparral Drive, Near Term + Proje Princess Joann Road to Chaparral Drive, Near Term + 50%	t 2	10 10 10	3,810 7,620 4,883	40 40 40	0.5 0.5 0.5	2.0% 2.0% 2.0%	2.0% 2.0% 6.8%	61 - 64 - 65 -	- 44 51	60 96 110	130 206 237
uyamaca Street Chaparral Drive to Woodglen Vista Drive, Near Term Chaparral Drive to Woodglen Vista Drive, Near Term + 50%	2 roji 4	40 16	683 4,493	35 50	0.5 0.5	3.0% 3.0%	2.0% 2.0%	54 - 65 -	-	111	- 239
Chaparral Drive to Woodglen Vista Drive, Near Term + Proje Chaparral Drive to Woodglen Vista Drive, Near Term + 50%	:t 4	16 16	8,303 5,566	50 50	0.5 0.5	3.0%	2.0% 6.2%	68 - 68 -	77 80	167 172	359 370
Cuyamaca Street Woodglen Vista Drive to El Nopal, Near Term Woodglen Vista Drive to El Nopal, Near Term + 50% project	2	40 16	4,472 8,282	35 50	0.5 0.5	3.0% 3.0%	2.0% 2.0%	62 - 68 -	- 77	69 166	149 359
Woodglen Vista Drive to El Nopal, Near Term + Project Woodglen Vista Drive to El Nopal, Near Term + 50% project uvamaca Street	4 cc 4	16 16	12,092 9,355	50 50	0.5 0.5	3.0% 3.0%	2.0% 4.5%	69 - 70 -	99 102	214 219	462 471
El Nopal to Mast Boulevard, Near Term El Nopal to Mast Boulevard, Near Term + 50% project	3 4	30 16	9,173	35 50	0.5	3.0%	2.0%	65 - 70 -	- 104	113 225	244 484
El Nopal to Mast Boulevard, Near Term + Project El Nopal to Mast Boulevard, Near Term + 50% project + con Cuyamaca Street	4 truc 4	16 16	16,792 13,133	50 50	0.5 0.5	3.0% 3.0%	2.0% 3.8%	71 5 71 5		267 261	575 562
Mast Boulevard to River Park Drive, Near Term Mast Boulevard to River Park Drive, Near Term + 50% proje Mast Boulevard to River Park Drive. Near Term + Project	4	15 15 15	20,527 23,417 26,307	35 35 35	0.5 0.5 0.5	3.0% 3.0% 3.0%	2.0% 2.0% 2.0%	69 - 69 - 70 -	88 96 104	189 207 223	408 445 481
Mast Boulevard to River Park Drive, Near Term + 50% proje Cuyamaca Street		15	24,490	35	0.5	3.0%	3.0%	70 53	2 111	239	516
River Park Drive to Town Center Parkway, Near Term River Park Drive to Town Center Parkway, Near Term + 50% River Park Drive to Town Center Parkway, Near Term + Proj		15 15 15	28,084 30,844 33,604	35 35 35	0.5	3.0% 3.0% 3.0%	2.0% 2.0% 2.0%	70 - 70 55 71 55		233 248 263	503 535 566
River Park Drive to Town Center Parkway, Near Term + 50% Cuyamaca Street	pra 4	15	31,917	35	0.5	3.0%	2.7%	71 6) 129	278	600
Town Center Parkway to Mission Gorge Road, Near Term Town Center Parkway to Mission Gorge Road, Near Term + Town Center Parkway to Mission Gorge Road, Near Term +	6 0% 6 Proj 6	15 15 15	24,245 26,740 29,235	35 35 35	0.5 0.5 0.5	5.0% 5.0% 5.0%	3.0% 3.0% 3.0%	72 73 73 74 73 83	3 169	340 363 385	733 782 830
Town Center Parkway to Mission Gorge Road, Near Term + Magnolia Avenue Cuvamaca Street to Princess Joann Road. Near Term		15	27,813 DNE	35	0.5	5.0%	3.8%	74 8	7 187	403	868
Cuyamaca Street to Princess Joann Road, Near Term + 50% Cuyamaca Street to Princess Joann Road, Near Term + Pro	prc 2 ect 2	12 12	3,155 6,310	35 35	0.5	3.0%	2.0% 2.0%	<u>60</u> - 63 -		48 76	104 165
Cuyamaca Street to Princess Joann Road, Near Term + 50% Magnolia Avenue Princess Joann Road to Woodglen Vista Drive. Near Term		12	4,228	35 40	0.5	3.0%	7.6% 2.0%	<u>64</u> -	45	96	207
Princess Joann Road to Woodglen Vista Drive, Near Term + Princess Joann Road to Woodglen Vista Drive, Near Term +	Proj 4	15 15	5,359 8,514	40 40	0.5	3.0%	2.0% 2.0%	<u>64</u> - 66 -	58	91 125	197 268
Princess Joann Road to Woodglen Vista Drive, Near Term + Magnolia Avenue Woodglen Vista Drive to El Nopal, Near Term	4	15	6,432 9,415	40	0.5	3.0%	5.7% 2.0%	67 -	67	143	309
Woodglen Vista Drive to El Nopal, Near Term + 50% project Woodglen Vista Drive to El Nopal, Near Term + Project	4	15 15	12,570 15,725	40 40	0.5	3.0%	2.0% 2.0%	<u>68</u> - 69 -	75 87	161 187	348 404
Woodglen Vista Drive to El Nopal, Near Term + 50% project Magnolia Avenue El Nopal to Mast Boulevard, Near Term	- cc 4 4	15	13,643 14,291	40 40	0.5	3.0%	3.7% 2.0%	<u>69</u> -	94	203	437
El Nopal to Mast Boulevard, Near Term + 50% project El Nopal to Mast Boulevard, Near Term + Project El Nopal to Mast Boulevard, Near Term + 50% project + con	4 4 true 4	15 15 15	16,131 17,971 17,204	40 40 40	0.5	3.0% 3.0% 3.0%	2.0% 2.0% 3.4%	<u>69</u> -	88 95 106	191 205 229	411 441 494
Magnolia Avenue (Mitigated) Princess Joann Road to Woodglen Vista Drive, Near Term	4	15	2,204	40	0.5	3.0%	2.0%	<u> </u>	- 106	-	109
Princess Joann Road to Woodglen Vista Drive, Near Term + Princess Joann Road to Woodglen Vista Drive, Year 2035 Princess Joann Road to Woodglen Vista Drive, Year 2035 +	4	15 15 15	5,359 8,514 6,197	40 40 40	0.5 0.5 0.5	3.0% 3.0% 3.0%	2.0% 2.0% 2.0%	64 - 66 - 65 -	- 58	91 125 101	197 268 217
Magnolia Avenue (Mitigated) Woodglen Vista Drive to El Nopal, Near Term	4	15	9,415	40	0.5	3.0%	2.0%		62	133	287

Woodglen Vista Drive to El Nopal, Near Term + 50% project	4	15	12,570	40	0.5	3.0%	2.0%	68	-	75	161	348	50	9,767	1,596	1,207	330	224	19	7	28	20	67.4 76.3 81.3	2 0.9	65.8 60.	2 63.4 1	8.5 62.9	52.7 53	3.2 63.7	51.8 50.8 5	54.2 57.3	35	75	161	348
Woodglen Vista Drive to El Nopal, Near Term + Project	4	15	15,725	40	0.5	3.0%	2.0%	69	-	87	187	404	50	12,218	1,997	1,510	412	280	24	9	35	25	67.4 76.3 81.3	2 0.9	66.7 61	2 64.4	9.4 63.8	53.6 5/	4.2 64.7	52.8 51.8 5	55.2 58.2	40	87	187	404
Woodglen Vista Drive to El Nopal, Near Term + 50% project + cc	4	15	13,643	40	0.5	3.0%	3.7%	69		94	203	437	50	10,601	1,733	1,310	358	453	21	14	31	41	67.4 76.3 81.2	2 0.9	66.0 60.	6 66.5	9.8 63.2	53.0 56	3.3 64.3	51.9 51.1 5	57.2 59.1	44	94	203	437
Magnolia Avenue														0	0	0	0	0	0	0	0	0	#### #### ###	# ####	¥### ##A	# #### +	### ####	. ##### ##	;## ####	****	****	0	0	0	0
El Nopal to Mast Boulevard, Near Term	4	15	14,291	40	0.5	3.0%	2.0%	68	-	82	176	379	50	11,104	1,815	1,372	375	255	22	8	32	23	67.4 76.3 81.2	2 0.9	66.3 60	8 64.0	9.0 63.4	53.2 57	3.8 64.2	52.4 51.4 5	54.7 57.8	38	82	176	379
El Nopal to Mast Boulevard, Near Term + 50% project	4	15	16,131	40	0.5	3.0%	2.0%	69	-	88	191	411	50	12,534	2,049	1,549	423	287	24	9	36	26	67.4 76.3 81.2	2 0.9	66.8 61	3 64.5 1	9.5 64.0	53.7 5/	4.3 64.8	52.9 51.9 5	55.3 58.4	41	88	191	411
El Nopal to Mast Boulevard, Near Term + Project	4	15	17,971	40	0.5	3.0%	2.0%	69	-	95	205	441	50	13,963	2,282	1,725	471	320	27	10	41	29	67.4 76.3 81.2	2 0.9	67.3 61	8 65.0	0.0 64.4	54.2 54	4.8 65.2	53.4 52.3 5	55.7 58.8	44	95	205	441
El Nopal to Mast Boulevard, Near Term + 50% project + construc	4	15	17,204	40	0.5	3.0%	3.4%	70		106	229	494	50	13,368	2,185	1,652	451	516	26	16	39	47	67.4 76.3 81.2	2 0.9	67.0 61.	6 67.0	0.6 64.2	54.0 56	ô.9 65.3	52.9 52.2 5	57.8 59.8	49	106	229	494
Magnolia Avenue (Mitigated)														0	0	0	0	0	0	0	0	0	#### #### ###	# ####	¥### ##A	W ##### +	### ####	. ##### ##	;## ####	****	****	0	0	0	0
Princess Joann Road to Woodglen Vista Drive, Near Term	4	15	2,204	40	0.5	3.0%	2.0%	60	-	-	-	109	50	1,713	280	212	58	39	3	1	5	4								44.2 43.2 4		11	23	51	109
Princess Joann Road to Woodglen Vista Drive, Near Term + 50%	4	15	5,359	40	0.5	3.0%	2.0%	64		-	91	197	50	4,164	681	514	141	95	8	3	12	9	67.4 76.3 81.3	2 0.9	62.1 56	5 59.7	4.8 59.2	49.0 49	9.5 60.0	48.1 47.1 5	50.5 53.6	20	42	91	197
Princess Joann Road to Woodglen Vista Drive, Year 2035	4	15	8,514	40	0.5	3.0%	2.0%	66	-	58	125	268	50	6,615	1,081	817	223	152	13	5	19	14	67.4 76.3 81.3	2 0.9	64.1 58	6 61.7	6.8 61.2	51.0 51	1.6 62.0	50.1 49.1 5	52.5 55.6	27	58	125	268
Princess Joann Road to Woodglen Vista Drive, Year 2035 + 50%	4	15	6,197	40	0.5	3.0%	2.0%	65	-	-	101	217	50	4,815	787	595	163	110	9	4	14	10	67.4 76.3 81.3	2 0.9	62.7 57	2 60.3	5.4 59.8	49.6 50	0.2 60.6	48.7 47.7 5	51.1 54.2	22	47	101	217
Magnolia Avenue (Mitigated)								-						0	0	0	0	0	0	0	0	0	#### #### ###	# ####	¥### ###A	# #### #	### ####	##### ##	<i>i## ####</i>	##### ##### #	<i>### ####</i>	0	0	0	0
Woodglen Vista Drive to El Nopal, Near Term	4	15	9,415	40	0.5	3.0%	2.0%	66	-	62	133	287	50	7,315	1,196	904	247	168	14	5	21	15	67.4 76.3 81.3	2 0.9	64.5 59	0 62.2	7.2 61.6	51.4 52	2.0 62.4	50.5 49.5 5	52.9 56.0	29	62	133	287
Woodglen Vista Drive to El Nopal, Near Term + 50% project	4	15	12,570	40	0.5	3.0%	2.0%	68	-	75	161	348	50	9,767	1,596	1,207	330	224	19	7	28	20	67.4 76.3 81.3	2 0.9	65.8 60	2 63.4	8.5 62.9	52.7 5	3.2 63.7	51.8 50.8 5	54.2 57.3	35	75	161	348
Woodglen Vista Drive to El Nopal, Near Term + Project	4	15	15,725	40	0.5	3.0%	2.0%	69	-	87	187	404	50	12,218	1,997	1,510	412	280	24	9	35	25	67.4 76.3 81.3	2 0.9	66.7 61.	2 64.4	9.4 63.8	53.6 5/	4.2 64.7	52.8 51.8 5	55.2 58.2	40	87	187	404
Woodglen Vista Drive to El Nopal, Near Term + 50% project + cc	4	15	13,408	40	0.5	3.0%	2.0%	68	-	78	169	363	50	10,418	1,703	1,287	352	239	20	8	30	22	67.4 76.3 81.3	2 0.9	66.0 60.	5 63.7	8.7 63.2	52.9 5	3.5 64.0	52.1 51.1 5	54.5 57.5	36	78	169	363
Fanita Parkway (Mitigated)														0	0	0	0	0	0	0	0	0	##### ##### ####	# ####	4### ##K	W ##### +	### ####	##### ##	;## ####	#### #### #	### ####	0	0	0	0
Ganley Drive to Lake Canyon Road, existing	2	0	2,610	40	0.5	2.0%	2.0%	59	-	-	46	99	50	2,028	331	251	46	47	3	1	4	4	67.4 76.3 81.3	2 -0.1	58.0 50	7 55.7	0.5 55.1	43.1 45	5.5 55.8	42.1 41.3 4	46.4 48.7	10	21	46	99
Ganley Drive to Lake Canyon Road, existing + construction	3	14	4,021	40	0.5	2.0%	6.2%	64	-	45	98	211	50	3,124	511	386	70	223	4	7	6	20	67.4 76.3 81.3	2 0.4	60.2 53	1 62.9	5.1 57.4	45.5 52	2.8 58.9	43.3 43.6 5	53.7 54.4	21	45	98	211
Fanita Parkway (Mitigated)														0	0	0	0	0	0	0	0	0	#### #### ###	# ####	¥### ###A	# #### *	### ####	##### ##	<i>:## ####</i>	#### #### #	<i>### ####</i>	0	0	0	0
Lake Canyon Road to Mast Boulevard, existing	2	0	3,860	40	0.5	2.0%	2.0%	61	-	-	60	129	50	2,999	490	371	67	69	4	2	6	6	67.4 76.3 81.3	2 -0.1	59.7 52	4 57.4	2.2 56.8	44.8 4	7.2 57.5	43.8 43.0 4	48.1 50.4	13	28	60	129
Lake Canyon Road to Mast Boulevard, existing + construction	4	14	5,271	40	0.5	2.0%	5.2%	65	-	54	116	250	50	4,096	669	506	92	245	5	8	8	22	67.4 76.3 81.3	2 0.8	61.8 54	7 63.8	6.2 59.0	47.1 5	3.6 60.3	45.2 45.2 5	54.5 55.4	25	54	116	250
Fanita Parkway (Mitigated)														0	0	0	0	0	0	0	0	0	#### #### ###	# ####	¥### ###A	# #### *	### ####	##### ##	<i>:## ####</i>	#### #### #	<i>### ####</i>	0	0	0	0
Project site to Ganley Drive, Near Term	2	15	DNE	40	0.5	2.0%	2.0%	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	50	######	* ######	####### #	*##### #	##### #	##### #	###### A	*#####	*****	67.4 76.3 81.3	2 0.1 ;	¥### ##A	# #### #	### ####	#### ##	;## ####	#### #### #	### #### #V	ALUE! #V	ALUE! #\	ALUE! #V	ALUE!
Project site to Ganley Drive, Near Term + 50 % project	2	15	6,175	40	0.5	2.0%	2.0%	63	-	-	84	182	50	4,798	784	593	108	110	6	4	9	10	67.4 76.3 81.3	2 0.1	62.0 54	7 59.6	4.4 59.1	47.1 49	9.4 59.8	46.1 45.2 5	50.4 52.6	18	39	84	182
Project site to Ganley Drive, Near Term + project	2	15	12,350	40	0.5	2.0%	2.0%	66	-	62	134	289	50	9,596	1,568	1,186	216	220	12	7	19	20	67.4 76.3 81.3	2 0.1	65.0 57	7 62.6	7.5 62.1	50.1 52	2.4 62.8	49.1 48.2 5	53.4 55.6	29	62	134	289
Project site to Ganley Drive, Near Term + 50% project + construct	2	15	7,248	40	0.5	2.0%	3.9%	65		54	116	249	50	5,632	920	696	127	254	7	8	11	23	67.4 76.3 81.2	2 0.1	62.6 55	4 63.2	6.3 59.7	47.8 53	3.1 60.8	46.3 45.9 5	54.0 55.2	25	54	116	249

TRAFFIC NOISE LEVELS AND NOISE CONTOURS

Project Number: 1501144001 Project Name: Fanita Ranch - Proposed Project (with school)

	A Highway Noise Prediction Model (FHWA-F htt. Law, and Greenspan. January 2019	RD-77-108) with California Vehicle Noise (CALVENO) Emission Levels.	Trucks 'assenger Building Construction 312.0 1099.0 Other Building Construction 235.0 838.0
Community Noise Descriptor:	L _{dn} : X CNEL:	"-" = contour is located within the roadway right-of-way.	NTOverlap 312.0 124.0 LT Overlap 235.0 988.0
Assumed 24-Hour Traffic Distribution: Total ADT Volumes Medium-Duty Trucks	Day Evening Night 77.70% 12.70% 9.60% 87.43% 5.05% 7.52%	Distance is from the centerline of the roadway segment to the receptor location.	
Heavy-Duty Trucks	89.10% 2.84% 8.06%		Traffic-Volumes Ref. Energy Leve Dist. Ld Le Ln DISTANCE TO CONTOUR (2)
Analysis Condition Roadway, Segment Lan	Design Median ADT Speed Alp es Width Volume (mph) Fac		Calc Day Eve Night MTd HTd MTe HTe MTn HTn A MT HT Adj A MT HT Total A MT HT Total A MT HT Total 70 Ldn 65 Ldn 60 Ldn 55 Ldn
Mast Boulevard SR-52 to West Hills Parkway, existing 4	25 26,440 40 0.		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
SR-52 to West Hills Parkway, existing + construction 4 SR-52 to West Hills Parkway, Near Term 4	25 28,001 40 0. 25 30,730 40 0.	5 3.0% 2.0% 72 69 148 318 685	50 23,877 3,903 2,950 806 548 47 17 69 50 67.4 76.3 81.2 1.4 70.2 64.7 67.8 72.9 67.3 57.1 57.7 68.1 56.2 55.2 58.6 61.7 69 148 318 685
SR-52 to West Hills Parkway, Near Term + 50 % project 4 SR-52 to West Hills Parkway, Near Term + project 4	25 34,015 40 0. 25 37,300 40 0.	5 3.0% 2.0% 73 78 168 362 780	50 28,982 4,737 3,581 978 665 57 21 84 60 67.4 76.3 81.2 1.4 71.0 65.5 68.7 73.7 68.1 57.9 58.5 68.9 57.1 56.1 59.4 62.5 78 168 362 780
SR-52 to West Hills Parkway, Near Term + 50% project + constri 4 Mast Boulevard West Hills Parkway to Medina Drive existing 4	25 35,238 40 0. 15 19.540 40 0.		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
West Hills Parkway to Medina Drive, existing + construction 4 West Hills Parkway to Medina Drive, Near Term 4	15 21,101 40 0. 15 22,962 40 0.	5 3.0% 3.5% 71 57 123 266 572	50 16,395 2,680 2,026 553 654 32 21 48 59 67.4 76.3 81.2 0.9 67.9 62.5 68.1 71.6 65.1 54.9 57.9 66.2 53.8 53.0 58.8 60.8 57 123 266 572
West Hills Parkway to Medina Driv, Near Term + 50 % project 4 West Hills Parkway to Medina Drive, Near Term + project 4	15 27,692 40 0. 15 32,422 40 0.	5 3.0% 2.0% 72 65 141 304 654	50 25,192 4,118 3,113 850 578 49 18 73 52 67.4 76.3 81.2 0.9 69.9 64.4 67.5 72.6 67.0 56.8 57.4 67.8 55.9 54.9 58.3 61.4 65 141 304 654
West Hills Parkway to Medina Driv, Near Term + 50% project + c 4 Mast Boulevard Pebble Beach Drive to Fanita Parkway, existing 4	15 28,915 40 0. 15 19,590 40 0.		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Pebble Beach Drive to Fanita Parkway, existing + construction 4 Pebble Beach Drive to Fanita Parkway, Near Term 4	15 21,151 40 0. 15 21,361 40 0.	5 3.0% 3.5% 71 57 123 266 573 5 3.0% 2.0% 70 - 107 230 495	50 16,434 2,688 2,030 555 655 32 21 48 59 67.4 76.3 81.2 0.9 67.9 62.5 68.1 71.6 65.1 54.9 57.9 66.2 53.8 53.1 58.8 60.8 57 12.3 266 573 50 16,597 2,713 2,051 560 381 32 12 48 34 67.4 76.3 81.2 0.9 68.1 62.6 65.7 70.8 65.2 55.0 55.6 66.0 54.1 53.1 56.5 59.6 50 107 230 495
Pebble Beach Drive to Fanita Parkway, Near Term + 50 % project 4 Pebble Beach Drive to Fanita Parkway, Near Term + project 4 Pebble Beach Drive to Fanita Parkway, Near Term + 50% project 4		5 3.0% 2.0% 72 63 136 294 632	50 23.948 3.914 2.959 808 549 47 18 70 50 67.4 76.3 81.2 0.9 69.7 64.1 67.3 72.4 66.8 56.6 57.1 67.6 55.7 54.7 58.1 61.2 63 136 294 632
Pebble Beach Drive to Fanita Parkway, Near Term + 50% projec 4 Mission Gorge Road SR-125 to Fanita Drive, existing 6	15 27,314 40 0. 15 45.440 45 0.		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
SR-125 to Fanita Drive, existing + construction 6 SR-125 to Fanita Drive, Near Term 6	15 47,001 45 0. 15 48,026 45 0.	5 5.0% 3.0% 77 156 337 726 1,563	3 50 37,316 6,099 4,610 2,099 1,284 121 41 181 116 69.3 77.6 82.1 2.6 74.6 70.8 73.2 77.9 71.8 63.2 63.0 72.9 63.1 61.3 63.9 67.7 156 337 726 1563
SR-125 to Fanita Drive, Near Term + 50 % project 6 SR-125 to Fanita Drive, Near Term + project 6 OP 105 For the New York Construction of the State Sta	15 50,916 45 0. 15 53,806 45 0. 15 52,139 45 0.	5 5.0% 3.0% 78 169 363 783 1,686	3 50 41,807 6,833 5,165 2,352 1,438 136 46 202 130 69.3 77.6 82.1 2.6 75.1 71.3 73.7 78.4 72.3 63.7 63.5 73.4 63.6 61.8 64.4 68.2 169 363 783 1686
SR-125 to Fanita Drive, Near Term + 50% project + construction 6 Mission Gorge Road Fanita Drive to Carlton Hills Boulevard, existing 6	· · · · · · · · · · · · · · · · · · ·		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Fanita Drive to Carlton Hills Boulevard, existing + construction 6 Fanita Drive to Carlton Hills Boulevard, Near Term 6	15 42,661 45 0. 15 43,029 45 0.	5 5.0% 3.7% 77 152 328 707 1,524 5 5.0% 3.0% 77 145 313 674 1,453	4 50 33,148 5,418 4,095 1,865 1,418 108 45 160 128 69.3 77.6 82.1 2.6 74.1 70.3 73.6 77.7 71.3 62.7 63.5 72.5 62.5 60.8 64.4 67.6 152 328 707 1524 3 50 33,434 5,465 4,131 1,881 1,150 109 37 162 104 69.3 77.6 82.1 2.6 74.1 70.3 72.7 77.4 71.4 62.7 62.5 72.4 62.6 60.9 63.5 67.2 145 313 674 1453
Fanita Drive to Carlton Hills Boulevard, Near Term + 50 % projec 6 Fanita Drive to Carlton Hills Boulevard, Near Term + project 6 Fanita Drive to Carlton Hills Boulevard. Near Term + 50% project 6	15 46,314 45 0. 15 49,599 45 0. 15 47.537 45 0.	5 5.0% 3.0% 78 160 344 741 1,597	7 50 38,538 6,299 4,762 2,168 1,326 125 42 186 120 69.3 77.6 82.1 2.6 74.7 70.9 73.3 78.0 72.0 63.4 63.2 73.0 63.2 61.5 64.1 67.8 160 344 741 1597
Fanita Parkway Project site to Ganley Drive, existing 2	15 DNE 40 0.	5 2.0% 2.0% #VALUE ! #VALUE! #VALUE! #VALUE! #VALUE!	
Project site to Ganley Drive, existing + construction 2 Project site to Ganley Drive, Near Term 2 Project site to Ganley Drive, Near Term + 50 % project 2	15 1,561 40 0. 15 DNE 40 0. 15 6,175 40 0.	5 2.0% 2.0% #VALUE! #VALUE! #VALUE! #VALUE! #VALUE!	IEI 50 ####### ####### ####### ####### ######
Project site to Ganley Drive, Near Term + project 2 Project site to Ganley Drive, Near Term + 50% project + construct 2	15 12,350 40 0. 15 7,398 40 0.	5 2.0% 2.0% 66 - 62 134 289	50 9,596 1,568 1,186 216 220 12 7 19 20 67.4 76.3 81.2 0.1 65.0 57.7 62.6 67.5 62.1 50.1 52.4 62.8 49.1 48.2 53.4 55.6 29 62 134 289 50 5,748 940 710 129 341 7 11 11 31 67.4 76.3 81.2 0.1 62.6 55.4 64.5 67.0 59.8 47.9 54.3 61.1 46.0 46.0 55.3 56.2 28 61 131 281
Fanita Parkway Ganley Drive to Lake Canyon Road, existing 2 Ganley Drive to Lake Canyon Road, existing + construction 3	0 2,610 40 0. 14 4,171 50 0.		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Ganley Drive to Lake Canyon Road, existing + Construction 3 Ganley Drive to Lake Canyon Road, Near Term 2 Ganley Drive to Lake Canyon Road, Near Term + 50 % project 3	0 2,782 40 0. 14 8,957 50 0.	5 2.0% 2.0% 60 48 104	50 2,162 353 267 49 50 3 2 4 4 67.4 76.3 81.2 -0.1 58.3 51.0 55.9 60.8 55.4 43.4 45.8 56.1 42.4 41.5 46.7 48.9 10 22 48 104
Ganley Drive to Lake Canyon Road, Near Term + project 3 Ganley Drive to Lake Canyon Road, Near Term + 50% project + 3	14 15,132 50 0. 14 10,180 50 0.		50 7,910 1,293 977 178 391 10 12 15 35 71.1 78.8 83.0 0.4 67.1 58.6 66.3 70.0 64.3 51.0 56.1 65.1 50.7 49.2 57.0 58.5 43 93 201 433
Fanita Parkway Lake Canyon Road to Mast Boulevard, existing 2 Lake Canyon Road to Mast Boulevard, existing + construction 4	0 3,860 40 0. 14 5,421 50 0.		
Lake Canyon Road to Mast Boulevard, Near Term 2 Lake Canyon Road to Mast Boulevard, Near Term + 50 % projec 4	0 4,158 40 0. 14 9,808 50 0.	5 2.0% 2.0% 61 63 135 5 2.0% 2.0% 68 - 80 173 372	50 3,231 528 399 73 74 4 2 6 7 67.4 76.3 81.2 -0.1 60.1 52.7 57.7 62.5 57.2 45.2 47.5 57.8 44.1 43.3 48.4 50.7 14 29 63 135 50 7,621 1,246 942 172 175 10 6 15 16 71.1 78.8 83.0 0.8 67.5 58.9 63.2 69.3 64.6 51.3 53.0 65.0 51.6 49.4 53.9 56.8 37 80 173 372
Lake Canyon Road to Mast Boulevard, Near Term + project 4 Lake Canyon Road to Mast Boulevard, Near Term + 50% project 4 Fanita Parkway			
Mast Boulevard to Carlton Oaks Drive, existing 2 Mast Boulevard to Carlton Oaks Drive, existing + construction 2	0 3,330 35 0. 0 4,891 35 0.		50 2,587 423 320 58 30 3 1 5 3 65.1 74.8 80.0 -0.1 57.5 50.9 53.2 59.5 54.5 43.3 43.0 55.1 41.7 41.4 43.9 47.3 8 18 39 84
Mast Boulevard to Carlton Oaks Drive, Near Term 2 Mast Boulevard to Carlton Oaks Drive, Near Term + 50 % projec 2 Mast Boulevard to Carlton Oaks Drive, Near Term + project 2	0 3,713 35 0. 0 5,423 35 0. 0 7,133 35 0.	5 2.0% 1.0% 60 54 116	
Mast Boulevard to Cariton Oaks Drive, Near Term + project 2 Mast Boulevard to Cariton Oaks Drive, Near Term + 50% project 2 Cariton Hills Boulevard	0 7,133 35 0. 0 6,646 35 0.		
Carlton Oaks Drive to Mission Gorge Road, existing 4 Carlton Oaks Drive to Mission Gorge Road, existing + constructic 4	0 24,960 35 0. 0 26,521 35 0.	5 3.0% 3.2% 70 51 111 238 513	50 20.607 3.368 2.546 696 751 40 24 60 68 65.1 74.8 80.0 0.3 66.7 62.1 67.6 70.8 63.9 54.5 57.4 65.2 52.7 52.6 58.4 60.2 51 111 238 513
Carlton Oaks Drive to Mission Gorge Road, Near Term 4 Carlton Oaks Drive to Mission Gorge Road, Near Term + 50 % p Carlton Oaks Drive to Mission Gorge Road, Near Term + project 4	0 25,993 35 0. 0 28,228 35 0. 0 30,463 35 0.	5 3.0% 2.0% 70 46 100 216 465	50 21,933 3,585 2,710 740 503 43 16 64 46 65.1 74.8 80.0 0.3 67.1 62.3 65.9 70.3 64.2 54.7 55.7 65.2 53.1 52.9 56.6 59.3 46 100 216 465
Carlton Oaks Drive to Mission Gorge Road, Near Term + 50% pr 4 State Route 52	0 29,451 35 0. 60 96.000 65 0.	5 3.0% 2.8% 70 53 114 245 528	50 22.883 3.740 2.827 772 734 45 23 66 66 65.1 74.8 80.0 0.3 672 62.5 0 75 7.1 0.64 4 54.9 57.3 65.5 53.2 53.1 58.3 60.3 53 114 245 528 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Santo Road to Mast Boulevard, existing 6 Santo Road to Mast Boulevard, existing + construction 6 Santo Road to Mast Boulevard, Near Term 6	60 96,000 65 0. 60 97,561 65 0. 60 104,092 65 0.	5 2.0% 0.9% 76 255 549 1,183 2,549	9 100 75.805 12,390 9,366 1,706 800 99 25 147 72 75.5 81.7 85.2 -3.2 76.8 66.6 66.8 77.6 73.8 59.0 56.7 74.1 61.1 57.2 57.6 63.8 255 549 1183 2549
Santo Road to Mast Boulevard, Near Term + 50 % project 6 Santo Road to Mast Boulevard, Near Term + project 6	60 109,079 65 0. 60 114,066 65 0.	5 2.0% 0.6% 77 276 595 1,282 2,762	2 100 88,629 14,486 10,950 1,995 610 115 19 172 55 75.5 81.7 85.2 -3.2 77.5 67.3 65.7 78.1 74.5 59.7 55.5 74.7 61.8 57.9 56.4 64.1 276 595 1282 2762
Santo Road to Mast Boulevard, Near Term + 50% project + cons 6 Cuyamaca Street Project Site to Magnolia Avenue, Near Term 2	60 110,302 65 0. 10 DNE 40 0.		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Project Site to Magnolia Avenue, Near Term + 50% project 2 Project Site to Magnolia Avenue, Near Term + Project 2	10 <u>6,960 40 0.</u> 10 13,920 40 0.	5 2.0% 2.0% 64 - 42 90 194 5 2.0% 2.0% 67 - 66 143 309	50 5,408 884 668 122 124 7 4 10 11 67.4 76.3 81.2 0.1 62.4 55.1 60.0 64.9 59.5 47.5 49.9 60.2 46.5 50.8 53.0 19 42 90 194 50 10,816 1,788 1,336 243 248 14 8 21 22 67.4 76.3 81.2 0.1 65.4 58.1 63.0 67.9 62.5 50.5 52.9 63.2 49.5 48.7 53.8 56.0 31 66 143 309
Project Site to Magnolia Avenue, Near Term + 50% project + con 2 Cuyamaca Street Magnolia Avenue to Princess Joann Road. Near Term 2	10 <u>8,183 40 0.</u>		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Magnolia Avenue to Princess Joann Road, Near Term + 50% prc 2 Magnolia Avenue to Princess Joann Road, Near Term + Project 2	10 <u>3,810 40 0.</u> 10 7,620 40 0.	5 2.0% 2.0% 61 60 130	50 2,960 484 366 67 68 4 2 6 6 67.4 76.3 81.2 0.1 59.8 52.5 57.4 62.3 56.9 44.9 47.2 57.6 43.9 43.0 48.2 50.4 13 28 60 130
Magnolia Avenue to Princess Joann Road, Near Term + 50% prc 2 Cuyamaca Street Princess Joann Road to Chaparral Drive. Near Term 2	10 <u>5,033 40 0.</u>		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Princess Joann Road to Chaparral Drive, Near Term + 50% proje 2 Princess Joann Road to Chaparral Drive, Near Term + Project 2	10 3,810 40 0.	5 2.0% 2.0% 61 - 60 130 5 2.0% 2.0% 64 - 44 96 206	50 2,960 484 366 67 68 4 2 6 6 67.4 76.3 81.2 0.1 59.8 52.5 57.4 62.3 56.9 44.9 47.2 57.6 43.9 43.0 48.2 50.4 13 28 60 130
Princess Joann Road to Chaparral Drive, Near Term + 50% proje 2 Cuyamaca Street Chaparral Drive to Mondrates Vista Drive, Near Term 2	10 <u>5,033 40 0.</u>	5 2.0% 6.7% 65 - 52 111 239	50 3,911 639 483 88 299 5 10 8 27 67.4 76.3 91.2 0.1 60.8 53.7 63.9 65.9 58.0 46.1 53.7 59.6 43.8 44.2 54.6 55.3 24 52 111 239 0 <td< td=""></td<>
Chaparral Drive to Woodglen Vista Drive, Near Term 2 Chaparral Drive to Woodglen Vista Drive, Near Term + 50% proj Chaparral Drive to Woodglen Vista Drive, Near Term + Project 4		5 3.0% 2.0% 65 111 239	
Chaparral Drive to Woodglen Vista Drive, Near Term + 50% proje 4 Cuyamaca Street	16 5,716 50 0.	5 3.0% 6.1% 68 - 81 174 374	50 4,441 726 549 150 311 9 10 13 28 71.1 78.8 83.0 0.9 64.9 58.4 65.8 68.8 62.2 50.8 55.6 63.3 50.5 48.9 56.5 58.1 37 81 174 374 0 <
Woodglen Vista Drive to El Nopal, Near Term 2 Woodglen Vista Drive to El Nopal, Near Term + 50% project 4 Woodglen Vista Drive to El Nopal, Near Term + Project 4	40 4,472 35 0. 16 8,282 50 0. 16 12,092 50 0.	5 3.0% 2.0% 68 - 77 166 359	50 6,435 1,052 795 217 148 13 5 19 13 71.1 78.8 83.0 0.9 66.8 60.0 62.5 68.8 63.9 52.4 52.4 64.5 52.8 50.5 53.3 57.2 36 77 166 359
Woodglen Vista Drive to El Nopal, Near Term + 50% project + cc 4 Cuyamaca Street 4	16 9,505 50 0.	5 3.0% 4.5% 70 - 102 220 475	50 7,385 1,207 912 249 379 14 12 21 34 71.1 78.8 83.0 0.9 67.2 60.6 66.6 70.4 64.5 53.0 56.5 65.4 53.0 51.1 57.4 59.4 47 102 220 475 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
El Nopal to Mast Boulevard, Near Term 3 El Nopal to Mast Boulevard, Near Term + 50% project 4 El Nopal to Mast Boulevard, Near Term + Project 4	30 9,173 35 0. 16 12,983 50 0. 16 16,793 50 0.	5 3.0% 2.0% 70 - 104 225 484	50 10,088 1,649 1,246 341 231 20 7 29 21 71.1 78.8 83.0 0.9 68.7 61.9 64.5 70.7 65.9 54.4 54.3 66.4 54.8 52.5 55.3 59.1 48 104 225 484
El Nopal to Mast Boulevard, Near Term + 50% project + construc 4 Cuyamaca Street	16 14,206 50 0.	5 3.0% 3.7% 71 59 126 272 587	50 11,038 1,804 1,364 373 463 22 15 32 42 71.1 78.8 83.0 0.9 69.0 62.3 67.5 71.9 66.2 54.8 57.3 67.0 54.9 52.9 58.3 60.7 59 126 272 587 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Mast Boulevard to River Park Drive, Near Term 4 Mast Boulevard to River Park Drive, Near Term + 50% project 4 Mast Boulevard to River Park Drive, Near Term + Project 4		5 3.0% 2.0% 69 - 96 207 445	50 18,195 2,974 2,248 614 417 35 13 53 38 65.1 74.8 80.0 0.9 66.8 62.0 65.6 70.0 63.9 54.5 55.4 64.9 52.8 52.6 56.3 59.1 45 96 207 445
Mast Boulevard to River Park Drive, Near Term + 50% project + 4 Cuyamaca Street	15 24,640 35 0.	5 3.0% 3.0% 70 52 111 240 517	50 19,145 3,129 2,365 646 648 37 21 56 59 65.1 74.8 80.0 0.9 67.0 62.3 67.5 70.9 64.1 54.7 57.3 65.3 52.9 52.8 58.3 60.2 52 111 240 517 0
River Park Drive to Town Center Parkway, Near Term 4 River Park Drive to Town Center Parkway, Near Term + 50% pro 4 River Park Drive to Town Center Parkway, Near Term + Project 4	15 28,084 35 0. 15 30,844 35 0. 15 33,604 35 0.	5 3.0% 2.0% 70 53 115 248 535	50 23,966 3,917 2,961 809 550 47 18 70 50 65.1 74.8 80.0 0.9 68.0 63.2 66.8 71.2 65.1 55.7 56.6 66.1 54.0 53.8 57.5 60.3 53 115 248 535
River Park Drive to Town Center Parkway, Near Term + 50% pro 4 Cuyamaca Street	15 32,067 35 0.	5 3.0% 2.7% 71 60 130 279 601	50 24.916 4.073 3.078 841 781 49 25 72 71 65.1 74.8 80.0 9.8:1 63.4 63.3 71.9 65.3 55.8 58.1 64.4 54.1 54.0 59.1 61.2 60 130 279 6011 0 0 0 0 0 0 0 ##### #### #### #### #### #### #### ##### #### #### ##### ##### ##### ##### #####<
Town Center Parkway to Mission Gorge Road, Near Term 6 Town Center Parkway to Mission Gorge Road, Near Term + 50% 6	15 26,740 35 0.	5 5.0% 3.0% 73 78 169 363 782	50 20,777 3,396 2,567 1,169 715 68 23 101 65 65.1 74.8 80.0 2.6 68.9 66.6 69.6 73.3 66.2 59.0 59.5 67.6 57.4 57.1 60.4 63.3 78 169 363 782
Town Center Parkway to Mission Gorge Road, Near Term + Proj 6 Town Center Parkway to Mission Gorge Road, Near Term + 50% 6 Magnolia Avenue	i 15 29,235 35 0. i 15 27,963 35 0.		
Cuyamaca Street to Princess Joann Road, Near Term 2 Cuyamaca Street to Princess Joann Road, Near Term + 50% prc 2	15 3,155 35 0.	5 3.0% 2.0% 60 49 105	EI 50 ####### ####### ####### ####### ######
Cuyamaca Street to Princess Joann Road, Near Term + Project 2 Cuyamaca Street to Princess Joann Road, Near Term + Project 2 Magnolia Avenue	15 6,310 35 0. 15 4,378 35 0.		50 4,903 801 606 166 112 10 4 14 10 65.1 74.8 80.0 0.1 80.4 56.6 59.2 63.8 57.5 48.0 49.0 58.5 64.4 62.4 94.9 52.6 17 36 77 166 50 3,402 556 420 115 287 7 9 10 26 65.1 74.8 80.0 0.1 58.5 54.0 45.3 58.0 43.9 46.5 54.8 21 46 98 211 0 </td
Princess Joann Road to Woodglen Vista Drive, Near Term 4 Princess Joann Road to Woodglen Vista Drive, Near Term + 50% 4	15 2,204 40 0. 15 5,359 40 0.	5 3.0% 2.0% 64 91 197	50 1,713 280 212 58 39 3 1 5 4 67.4 76.3 81.2 0.9 58.2 52.7 55.9 60.9 55.3 45.1 45.7 56.1 44.2 43.2 46.6 49.7 11 23 51 109 50 4,164 681 514 141 95 8 3 12 9 67.4 76.3 81.2 0.9 62.1 56.5 59.7 64.8 59.2 49.0 49.5 60.0 48.1 47.1 50.5 53.6 20 42 91 197
Princess Joann Road to Woodglen Vista Drive, Near Term + Pro Princess Joann Road to Woodglen Vista Drive, Near Term + 50% 4	15 8,514 40 0.	5 3.0% 2.0% 66 - 58 125 268	50 6,615 1,081 817 223 152 13 5 19 14 67.4 76.3 81.2 0.9 64.1 58.6 61.7 66.8 61.2 51.0 51.6 62.0 50.1 49.1 52.5 55.6 27 58 125 268 50 51.1 51.6 52 51.1 51 52.5 55.6 51 51.5 51.5 51.5 51.5 51.5 51.5
Magnolia Avenue Woodglen Vista Drive to El Nopal, Near Term 4 Woodglen Vista Drive to El Nopal, Near Term + 50% project 4	15 9,415 40 0. 15 12,570 40 0.	5 3.0% 2.0% 68 - 75 161 348	
Woodglen Vista Drive to El Nopal, Near Term + Project 4 Woodglen Vista Drive to El Nopal, Near Term + 50% project + cc 4		5 3.0% 2.0% 69 - 87 187 404	50 12,218 1,997 1,510 412 280 24 9 35 25 67.4 76.3 81.2 0.9 66.7 61.2 64.4 69.4 63.8 53.6 54.2 64.7 52.8 51.8 55.2 58.2 40 87 187 404 50 10,717 1,752 1,324 362 455 21 15 31 41 67.4 76.3 81.2 0.9 66.1 60.7 66.5 69.9 63.3 53.1 56.3 64.4 51.9 51.2 57.3 59.1 44 95 204 440
Magnolia Avenue 4 El Nopal to Mast Boulevard, Near Term 4 El Nopal to Mast Boulevard, Near Term + 50% project 4	15 14,291 40 0. 15 16,131 40 0.		
El Nopal to Mast Boulevard, Near Term + 50% project 4 El Nopal to Mast Boulevard, Near Term + 50% project + construc 4	15 17,971 40 0.	5 3.0% 2.0% 69 - 95 205 441	50 13,963 2,282 1,725 471 320 27 10 41 29 67.4 76.3 81.2 0.9 67.3 61.8 65.0 70.0 64.4 54.2 54.8 65.2 53.4 52.3 55.7 58.8 44 95 205 441

Appendix F. Roadway Construction Noise Model Results On Site

F_Fanita Onsite 03 27 2019.txt Roadway Construction Noise Model (RCNM),Version 1.1

Report date:03/29/2019Case Description:Fanita On Site

**** Receptor #1 ****

			Baseli	nes (dBA)
Description	Land Use	Daytime	Evening	Night
Residence	Commercial	65.0	60.0	55.0

Equipment

			Spec	Actual	Receptor
Estimated	Impact	Usage	Lmax	Lmax	Distance
Shielding	тырасс	USage	LIIIdX	LIIIdX	Distance
Description	Device	(%)	(dBA)	(dBA)	(feet)
(dBA)					
Dozer	No	40		81.7	50.0
0.0					
Scraper 0.0	No	40		83.6	50.0
Grader	No	40	85.0		50.0
0.0					
Excavator	No	40		80.7	50.0
0.0 Front End Loader	No	40		79.1	50.0
0.0					
Dump Truck	No	40		76.5	50.0
0.0 Sand Blasting (Single Nozzel)	No	20		95.7	50.0
0.0	NO	20		55.7	50.0
Sand Blasting (Single Nozzel)	No	20		95.7	50.0
0.0					

Results

(dBA)	Noise Limit Exceedance	(dBA)	Noise Limits
	Calculated (dBA)	Day	Evening

Night	F_Far	nita Onsi [.] Even						
Equipment	Lmax	l ea		-	Lmax	•	Lmax	Leq
		LCY						
Dozer			 81.7	 77.7	 N/A	 N/A	N/A	N/A
N/A N/A	N/A	N/A	N/A		N/A			
Scraper			83.6		N/A		N/A	N/A
N/A N/A	N/A	N/A	N/A	N/A	N/A	N/A		
Grader			85.0	81.0	N/A	N/A	N/A	N/A
N/A N/A	N/A	N/A	N/A	N/A	N/A	N/A		
Excavator			80.7	76.7	N/A	N/A	N/A	N/A
N/A N/A	N/A	N/A	N/A	N/A	N/A	N/A		
Front End Lo	bader		79.1	75.1	N/A	N/A	N/A	N/A
N/A N/A	N/A	N/A	N/A	N/A	N/A	N/A		
Dump Truck			76.5	72.5	N/A	N/A	N/A	N/A
N/A N/A	N/A	N/A	N/A	N/A	N/A	N/A		
Sand Blastir	ng (Single Noz	zel)	95.7	88.7	N/A	N/A	N/A	N/A
N/A N/A	N/A	N/A	N/A	N/A	N/A	N/A		
Sand Blastir	ng (Single Noz	zel)	95.7	88.7	N/A	N/A	N/A	N/A
N/A N/A	N/A	N/A	N/A	N/A	N/A	N/A		
	Tot	al	95.7	92.7	N/A	N/A	N/A	N/A
N/A N/A	N/A	N/A	N/A	N/A	N/A	N/A		

Appendix G. Roadway Construction Noise Model Results Off Site

G_Fanita offsite 03 27 2019.txt Roadway Construction Noise Model (RCNM),Version 1.1

Report date:	03/28/2019						
Case Description:	Fanita On Site						

**** Receptor #1 ****

			Baselines (dBA)				
Description	Land Use	Daytime	Evening	Night			
Residence	Commercial	65.0	60.0	55.0			

			Equipment										
Description	Impact Device	Usage (%)	Spec Lmax (dBA)	Actual Lmax (dBA)	Receptor Distance (feet)	Estimated Shielding (dBA)							
Dozer	No	40		81.7	50.0	0.0							
Scraper	No	40		83.6	50.0	0.0							
Grader	No	40	85.0		50.0	0.0							
Excavator	No	40		80.7	50.0	0.0							

Results

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Noise Limits (dBA)

Noise Limit Exceedance (dBA)

		(Calculate	d (dBA)	Da	iy	Eveni	ng	
Night		Day		Evening		light			
 Equipment			Lmax	Leq	Lmax	Leq	Lmax	Leq	Lmax
Leq	Lmax	Leq	Lmax	Leq	Lmax	Leq			
Dozer			81.7	77.7	N/A	N/A	N/A	N/A	N/A
N/A	N/A	N/A	N/A	N/A	N/A	N/A			
Scraper			83.6	79.6	N/A	N/A	N/A	N/A	N/A
N/A	N/A	N/A	N/A	N/A	N/A	N/A			
Grader			85.0	81.0	N/A	N/A	N/A	N/A	N/A
N/A	N/A	N/A	N/A	N/A	N/A	N/A			
Excavator			80.7	76.7	N/A	N/A	N/A	N/A	N/A
N/A	N/A	N/A	N/A	N/A	N/A	N/A			
	To	tal	85.0	85.1	N/A	N/A	N/A	N/A	N/A

			G_Fanita	offsite	03 27	2019.txt
N/A	N/A	N/A	N/A	N/A	N/A	N/A

Appendix H. Noise Barrier Height Estimates

SOUND BARRIER LOSS ESTIMATION*

Scenario: Fanita Parkway at Santee Lakes Campground

DATA Barrier Top Elevation, feet Source Ground Elevation, feet Height of Source above Ground, feet: Observer Elevation at ground or floor Distance from source to barrier, feet: Distance from barrier to observer, feet:	INPUT 429 425 3 413 35 80
BARRIER EFFECT RESULT	
Infinite Barrier Attenuation: Is Observer at Ground Level (yes or no): Adjustment for Loss of Ground Attenuation: Infinite Barrier Insertion Loss: Finite Barrier Adjustment Enter angle subtended by barrier :	-8.0 dBA yes 2.0 dBA -6.0 dBA 180 degrees
Enter Noise Level Without Barrier: Enter Reference Distance for Noise Level: Noise level including insertion loss of Barrier: Noise Level of barrier gaps:	70 dBA 50 feet 60.4 dBA 0.0 dBA
SUMMED AVERAGE LEVEL:	60.4 dBA

* Assumes a sound wavelength of 2 feet (about 550 Hz). Methodology Source: Harris, C.M. (1979), Handbook of Noise Control, 2nd. Ed.

SOUND BARRIER LOSS ESTIMATION*

Scenario: Fanita Parkway Section A-A (Project Site to Ganley)

DATA Barrier Top Elevation, feet Source Ground Elevation, feet Height of Source above Ground, feet: Observer Elevation at ground or floor Distance from source to barrier, feet: Distance from barrier to observer, feet:	INPUT 455 435 3 480 61 116
BARRIER EFFECT RESULT	
Infinite Barrier Attenuation: Is Observer at Ground Level (yes or no): Adjustment for Loss of Ground Attenuation: Infinite Barrier Insertion Loss: Finite Barrier Adjustment Enter angle subtended by barrier :	-4.9 dBA yes 1.0 dBA -3.9 dBA 180 degrees
Enter Noise Level Without Barrier: Enter Reference Distance for Noise Level: Noise level including insertion loss of Barrier: Noise Level of barrier gaps:	66 dBA 50 feet 56.6 dBA 0.0 dBA
SUMMED AVERAGE LEVEL:	56.6 dBA

* Assumes a sound wavelength of 2 feet (about 550 Hz). Methodology Source: Harris, C.M. (1979), Handbook of Noise Control, 2nd. Ed.

SOUND BARRIER LOSS ESTIMATION*

Scenario: Cuyamaca Section A-A (El Nopal to Beck Drive)

DATA	INPUT
Barrier Top Elevation, feet	508
Source Ground Elevation, feet	485
Height of Source above Ground, feet:	3
Observer Elevation at ground or floor	520
Distance from source to barrier, feet:	87
Distance from barrier to observer, feet:	75
BARRIER EFFECT RESULT	
Infinite Barrier Attenuation:	-4.8 dBA
Is Observer at Ground Level (yes or no):	yes
Adjustment for Loss of Ground Attenuation:	0.0 dBA
Infinite Barrier Insertion Loss:	-4.8 dBA
Finite Barrier Adjustment	
Enter angle subtended by barrier :	180 degrees
Enter Noise Level Without Barrier:	
	71 dBA
Enter Reference Distance for Noise Level:	50 feet
Noise level including insertion loss of Barrier:	61.1 dBA
Noise Level of barrier gaps:	0.0 dBA
SUMMED AVERAGE LEVEL:	61.1 dBA

* Assumes a sound wavelength of 2 feet (about 550 Hz). Methodology Source: Harris, C.M. (1979), Handbook of Noise Control, 2nd. Ed.

Appendix I. Use of Asphalt Rubber as CEQA Mitigation Memorandum



MEMORANDUM

To: Marni Borg, Principal Environmental Planner, City of Santee
From: Sharon Toland, Project Manager
RE: Use of Asphalt Rubber as CEQA Mitigation
Date: May 20, 2020

CC: Melanie Kush, Director of Planning, City of Santee

This memorandum documents the feasibility of asphalt rubber for mitigation of roadway noise impacts associated with the Fanita Ranch Project that are evaluated in the project-specific Noise Technical Report and Environmental Impact Report (EIR).

In early drafts of the Noise Technical Report that Harris prepared for the Fanita Ranch Project, Harris suggested the potential installation of asphalt rubber pavement to mitigate potential impacts to segments of Fanita Parkway, Cuyamaca Street, and Magnolia Avenue where installation of a noise barrier would not be feasible. Studies have demonstrated community noise level reductions in some instances of 5 A-weighted decibels (dBA), and up to 14 dBA, compared to traditional asphalt.^{1,2} Additional personal communication with the California Department of Transportation indicated that research from the University of California Pavement Research Center (UCPRC) would be most applicable for our analysis. The most recent study from UCPRC related to asphalt rubber demonstrated that use of asphalt rubber pavement could reduce on-board sound intensity (noise level where tire meets the pavement) by 3 dBA at the time of installation, although reduction in sound intensity varied based on material.³ Because a noticeable (3 dBA or more) reduction was demonstrated at the source (on-board sound intensity), and case studies demonstrated noticeable reductions in community noise level as a result of asphalt rubber installation, we identified asphalt rubber as a mitigation measure for the proposed project. However, because of the uncertainties in determining the potential reduction in community noise level from asphalt rubber over time, we concluded that with mitigation of asphalt rubber impacts resulting from project-generated traffic would not be reduced to below the significance threshold and would continue to be significant and unavoidable.

We have considered additional factors to asphalt rubber installation and longevity and received input from Harris and City of Santee (City) engineers, and project stakeholders at Padre Dam Municipal Water District. As a result of this additional consideration, we have concluded that asphalt rubber is not a feasible mitigation measure in the Noise Technical Report. Based on discussion with Harris engineers and review of UCPRC research, the noise reducing properties of asphalt rubber vary as a result of pavement type, as well as installation methods and experience of the construction contractor. The effectiveness of noise reductions could not be assessed prior to installation, and performance compared to existing asphalt could not be demonstrated without expensive, specialized equipment to measure on-board sound levels. Comparison of ambient community noise levels to future noise levels with asphalt rubber would not accurately isolate the effect of asphalt rubber, as traffic volumes would increase compared to existing, ambient conditions as a result of cumulative growth, as well as the proposed

¹ Putman, B.J., and S.N. Amirkhanian. 2005. "Rubberized Asphalt Mixtures: A Novel Approach to Pavement Noise Reduction." WIT Transactions on the Built Environment 77 (Urban Transport): 541–549.

² Sacramento County Department of Environmental Review and Assessment and Bollard & Brennan, Inc. 1999. Report of the Status of Rubberized Asphalt Traffic Noise Reduction in Sacramento County.

³ UCPRC (University of California Pavement Research Center). 2012. Investigation of Noise and Ride Quality Trends for Asphaltic Pavement Surface Types: Five-Year Results. Research Report: UCPRC-RR-2012-04. Prepared for the California Department of Transportation. August.

project. Additionally, the noise-reducing properties of asphalt rubber deteriorate over time.⁴ Similar to comparing future noise levels to existing noise levels, the City would not be able to accurately measure the deterioration in performance of asphalt rubber without measuring on-board sound levels because community noise level would be affected by changes in traffic volumes and asphalt rubber performance could not be isolated.

In addition to difficulties in determining whether the mitigation is effective, asphalt rubber would result in a maintenance burden compared to traditional asphalt. The UCPRC found that rubberized hot-mix asphalt open graded pavement, which is the pavement type that demonstrated a 3 dBA reduction compared to traditional pavement, provided noise reduction for several years after application, but noise benefit generally diminished noticeably after 7 to 9 years.⁵ Asphalt rubber did not provide a reduction of 3 dBA or more after 9 years. Results were similar for other case studies.⁶ Therefore, it is assumed that asphalt rubber would need to be replaced at least every 9 years to maintain noise benefits. This replacement schedule would result in additional impacts compared to regular pavement, which the City currently replaces at an average of every 15 years or more. Unlike traditional pavement, the entire length of asphalt rubber would need to be replaced rather than limiting maintenance to worn areas. More frequent replacement would cause nuisance impacts and disruption from more frequent road closures, additional exposure to construction noise, and additional criteria pollutant and greenhouse gas emissions.

Finally, Padre Dam Municipal Water District has major water and sewer facilities within affected roadways that require frequent maintenance. Padre Dam Municipal Water District emailed comments to the City on March 10, 2020,⁷ that expressed several concerns related to asphalt rubber:

- Increased roadway maintenance frequency and loss of effectiveness of asphalt rubber over time would result in nuisance noise to the Santee Lakes Recreation Preserve campground.
- The need to repair and replace the roadway with asphalt rubber pavement after each maintenance event would cause undue burden to its operations and budget.
- Due to temperature requirements for asphalt rubber installation, asphalt replacement would likely be limited to spring and summer, when potential nuisance noise exposure at the Santee Lakes Recreation Preserve campground would be at its peak.

Therefore, it was determined that the potential adverse impacts of asphalt rubber pavement outweigh the potential benefits. After careful consideration, in this circumstance, weighing all the factors for the proposed project, the use of asphalt rubber pavement as a mitigation measure to reduce traffic noise levels has been determined to be infeasible in the Noise Technical Report and EIR.

⁴ UCPRC 2012.

⁵ UCPRC 2012.

⁶ Freitas, Elisabete F. 2012. "The effect of time on the contribution of asphalt rubber mixtures to noise abatement." Noise Control Engineering Journal. January–February 2012.

⁷ Mael, Courtney. 2020. "Fanita Ranch (204020)." Email from Courtney Mael (Engineering Manager, Development and Construction, Padre Dam Municipal Water District) to Scott Johnson (Principal Civil Engineer, City of Santee). March 10.